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## Identification of the Parameters of $N$ aval A rtillery

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This book deals with the problems of reconstructing ballistic performance, based on eclectic source material. Included are some concrete examples of the identification of the parameters of naval artillery. Also included is a database of naval artillery from the Ironclad Era through W orld W ar 2.

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## CAVALLI, WAHRENDORFF AND THE MAKING OF KRUPP

The decade of the 1860s was a period of technical transition in naval warfare. Wood was giving way to iron for shipbuilding and armor protection. Smooth bore guns were giving way to rifles, both muzzle- and breech-loading. A nd the leading gun makers were graduating from cast iron to steel barrels. A nd the firm of W.G. A rmstrong in Britain was rapidly rising to prominence in the field. But there is another story; the story of two obscure inventors and an obscure Prussian company known as K rupp. This paper seeks to explore this other story, and shed some light on the beginnings of K rupp's rise to prominence.

1860-е годы стали периодом технической революции в военно-морском деле. Дерево уступило место железу, как в судостроении, так и в защите; гладкоствольные орудия - нарезным, как дульнозарядным, так и казнозарядным. А ведущие производители орудий начали выпуск стволов из чугуна и стали. Британская фирма WG Armstrong в этот период быстро пошла в гору и вскоре заняла видное место в этой области. Но есть и другая история, оставшаяся в тени исследователей. Это история двух непонятных изобретателей и не получившей тогда широкой известности компания Круппа из Пруссии. Эта статья направлена на изучение этой малоизвестной страницы, чтобы выявить роль Круппа и поставить его на видное место в истории этой эпохи.

The 1850s and 1860s were a time of transition in the development of artillery, characterized by the work of several individuals of extraordinary insight and determination. In Britain, the pioneering work of W. G. A rmstrong produced an array of breech loading guns in numerous calibers, suitable for the field artillery, the siege train and fortresses, and even the Royal Navy. Whitworth made advances in the production of steel for gun making, though his designs did not have the acceptance of A rmstrong's. Blakely designed muzzle loading rifles of great qual ity, with the same variety of applications as the Armstrong guns had, though not with the same wide acceptance. In the United States, Dahlgren and Rodman brought the smooth bore muzzle loader to its ultimate state of development. Parrott and Brooke produced rifled muzzle loaders of good performance.

There is, however, another line of development that has been virtually ignored. Almost all British and A merican historians mention the pioneering work of Cavalli and W ahrendorff, if they are mentioned at all, either as talented experimenters whose work led now here, or with degrees of inaccuracy that obscure their contributions ${ }^{1}$. And K rupp is mentioned as if its designs and products appeared fully developed and perfect, with a time distortion that condenses the fifty years prior to 1914 with passing comment. Y et much is made of how Armstrong grew and expanded as a successful commercial enterprise, in spite of the virtual boycott by the British armed services.

To be direct, there is another story in the development of modern artillery, one whose revelation is long overdue. It is sincerely hoped that this small effort will

[^0]encourage other more knowledgeable historians to fill in the gaps and correct any errors.

## I. Cavalli

Giovanni Cavalli was a Sardinian artillery officer of considerable talent and reputation. He had a successful career in the service of Piedmont-Sardinia and Iater of Italy, demonstrating considerable influence and foresight. In 1845, then Major Cavalli was involved with experimental firing against armored targets at Turin. In 1856, following the Crimean W ar, he advocated the construction of armored floating batteries of 1500 Tons, and larger ironclad warships of 1600 Tons and 24 guns or 2400 Tons and 36 guns, all with iron hulls and inclined armor, and fitted with rams. His case was sufficiently persuasive that they influenced Cavour to adopt such ships for the new Italian Navy.

He realized, as did many others, and perhaps as a result of the 1845 firings at armored targets, that the greater weight and explosive content of cylindrical conical shells would be advantageous for nearly all artillery applications. Y et the smooth bore guns of the time were hardly an effective delivery system, as the projectiles tended to tumble in flight, and the necessary windage combined with the greater projectile weight reduced gun performance.

What was needed was a system of rifling that would impart spin to the shells, thus restoring accuracy. So he examined the promising work of a Bavarian captain of artillery named $M$. Reichenbach. This talented officer experimented with a muzzle loading bronze rifled gun in 1816. By cutting seven grooves into the bore, he successfully fired conical projectiles, though deviation (deflection) in the trajectory was very great at first, but by reducing the angle of the rifling, the results were quite remarkable. But the work was curtailed in the face of lack of interest in military development so soon after the fall of N apoleon ${ }^{2}$.

In 1845, three experimental cannon were manufactured by the West Point Foundry, at the behest of the British government. They were highly unusual for the time, in that they were breech loading rifles. Hence, the detailed descriptions deserve to be quoted at length: "The chase of this gun does not differ essentially from the usual form of cannon; but at the breech the piece, instead of being round, has the four sides planed off so as to present from the rear an appearance of a square with the corners rounded off. It is bored throughout its length, and rifled with two flat grooves with rounded edges. The rear of the chamber is enlarged, and these grooves being continued through it, although shallower than in the chase, are deep enough to receive the wings or projections on the shop and hold it up till it reaches its seat in the gun.

Crossing the bore at right angles, with its front face perpendicular to the axis of the piece, a wedge-shaped opening with a rectangular cross-section is cut. It is

[^1]for a 32 -pdr. 24 cm deep, $13,7 \mathrm{~cm}$ wide at the large end, and $9,4 \mathrm{~cm}$ at the small. This opening receives the quoin or wedge destined to close the breech in rear of the charge. The wedge is made of hardened iron or steel, and of the same shape as the part of the opening which it is to fit. The wedge shape enables the bottom of the bore to be more perfectly closed, and prevents the escape of gas, whilst it also enables the breech-piece to be more easily moved after firing. The front face of the breech-piece is perpendicular to the axis of the piece, whilst the rear face makes with it an angle whose tangent is $18^{\text {th }}$ [sic. $1 / 8^{\text {th }}$ ], the co-efficient of friction of the hardened iron wedge against the cast iron of the piece. By means of this disposition and keeping the surfaces in contact well greased or moistened according as required, the breechpiece is found after firing to be more or less moved, at the same time that there is no danger of its being pushed too far or thrown out of place.

The breech-piece is provided with two handles, which serve to handle it in pushing in and withdrawing it from its position. The large handle placed on the right, is of such a size that, when the breech is open and ready for the charge, the projectile can be passed through it, the lower part of the handle part of the handle supporting the projectile, and guiding it through the breech opening into the chamber. To the large handle is attached a small chain and hook, the latter fitting into an eye screwed into the top of the opening on the right. This chain, when the breech is being opened, arrests the quoin when the opening in the large handle comes opposite the bore. When the charge is introduced, the cannoneer on the left pushes, and the one on the right pulls each by his handle, and the quoin comes back to the proper position for firing. In case any forcing is necessary, either for this or to move it after the piece is fired, a mortise is formed in the rear face of the quoin to receive the square end of a large iron handspike. It is not generally found necessary to use this lever except for the last-named purpose. In order to diminish the adhesion of the parts, three points are placed under the lower face of the quoin, which keep the quoin at the proper height in the cut.

To cut off the escape of gas, a ring of hammered copper is used, similar to the one in Armstrong's gun. The cross-section of this ring is about one inch square. A recess for it is cut out of the gun at the rear part of the bore, the inner diameter of it being greater than the outer one, in order to retain it in position. The ring projects about $6,4 \mathrm{~mm}$ behind the bore, and is pressed against by the quoin when in position. The interior diameter is the same as that of the chamber, and corresponding recesses are cut in it to allow the passage of the shot-flanges." ${ }^{3}$

Speaking of the same guns, General Sir Howard Douglas gives an even more contemporaneous description: "...In these guns the mechanical contrivances for securing the breech are very superior to the rude process of earlier times... The length of the Cavalli gun is 2,7 meters; it weighs 2,994 tones, and its caliber is $16,5 \mathrm{~cm}$. Two grooves are cut spirally along the bore, each of them making about half a turn in the length, which is 2,057 meters. The chamber, which is cylindrical, is 30 cm long and 18 cm diameter...

[^2]Immediately behind the chamber there is a rectangular perforation in a horizontal direction and perpendicular to the axis of the bore; its breadth vertically is 24 cm , while horizontally, it is $13,3 \mathrm{~cm}$ on the left side and $9,6 \mathrm{~cm}$ on the right side. This perforation is to receive a wrought-iron case-hardened quoin or wedge which, when in its place, covers the extremity of the chamber which is nearest the breech. The projectile... being introduced through the breech and chamber into the bore of the gun, and the cartridge placed behind it, a culot or false breech of cast iron is made to enter $6,35 \mathrm{~cm}$ into the bottom of the chamber behind the cartridge; and a copper ring, which also enters the chamber, is placed over it. The iron wedge is then drawn towards the right hand till it completely covers the chamber. After being fired, the gun can be reloaded without entirely taking out the wedge; for the latter, which is shorter than the rectangular cavity in which it moves, can be withdrawn far enough to allow the new load to be introduced." ${ }^{4}$


Cavalli's B reech M echanism


W edge of Cavalli B reech

The projectiles were especially interesting. As described by General Douglas, " ... the first [see below] is designated cylindro-conical, and the other cylindroconoidal; their entire lengths are 425 mm and 375 mm , respectively, and their greatest diameter is $16,5 \mathrm{~cm}$ : each has two projections, a b, directly opposite t one another, and $6,35 \mathrm{~mm}$ deep, which enter the grooves in the rifled bore. (These projections make an angle of 7 deg 8 min with the axis of the shot.) Each shot, if hollow, weighs about 31,3 kilos.; and if solid, about 46 kilos..." ${ }^{5}$ The ballistic shape of these projectiles is quite good, especially for that time! The blunter shape corresponds well with the more familiar 2 crh of the late $19^{\text {th }}$ and early $20^{\text {th }}$ centuries, while the Ionger resembles the 4 crh projectiles of the dreadnought era. The rounded base, however, would contribute to instability in flight.

In 1846, Cavalli was sent to Akers, Sweden, to oversee the production of some cannon being manufactured there for the Sardinia. This gave him an opportunity to meet and compare information with Baron M artin von W ahrendorff, the owner of the foundry and also an artillery designer of some repute. The Baron had been producing breech loading smooth bore guns since 1841.

A comparative trial was arranged for September of that year. The Cavalli gun produced interesting results, summarized in the Table below.

[^3]

Table 1.

| Shell, <br> kg | Charge, kg | Elevation | Muzzle velocity, <br> $\mathrm{m} / \mathrm{sec}$ | Range, m | Drift, m |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 31,3 | 3 | $14.75^{\circ}$ | 272 | 3044 | 77,7 |
| 31,3 | 4 | $13.00^{\circ}$ | 313 | 3354 | 91,4 |
| 46,0 | 3 | $14.50^{\circ}$ | 230 | 2370 | 25,6 |
| 31,7 | 4 | $13.00^{\circ}$ | 315 | 3491 | 90,5 |

The first two shots were using the nominal 2 crh shell, filled with black powder. The third was the same shell, but filled with lead, and the fourth was the nominal 4 crh shell, filled with black powder. The amount of drift/deflection in the trajectory was considered excessive, and the muzzle velocities were quite low.

Unfortunately, the gun was disabled after the fourth shot, when the breech blew off, a problem Cavalli attributed to weakness of the cast iron.

A nother of the three guns was tested at Shoebury Ness, in 1850. The results were very much the same as previously at A kers. Comments were that the deviations (deflection/drift) "were so variable in amount that no allowance could be made for them in laying the gun with respect to the" target ${ }^{6}$. A modern artillery expert, Edward Rudnicki, believes the excessive drift was the result of two factors: first, "The erratic nature of the drift with the splined shells could be a result of the projectile's balloting as it traveled down the tube, as two splines would not be enough to properly center and support the projectile," and second, that the rifling, one turn in 25 calibers, was excessive, as "... spin is a factor in M agnus Effect and thus drift. An excessive spin rate will over stabilize the projectile; as a result it will more greatly resist aerodynamic forces tending to cause it to nose over, with much resultant M agnus drift." ${ }^{7}$

[^4]

Representation of the C avalli breech loading system. (Holley, A Treatise on Naval Gunnery)

The last of the three guns was tested at Turin in 1854. But in the interim between the embarrassing failures at A kers and Shoebury Ness, Cavalli had made some changes. We know that during subsequent work in Belgium, he cut the splines to form two "buttons," which he found to be strong enough under the pressures of firing. From the data given in Table 2 below, it would also appear that he adjusted the pitch of the rifling, to avoid the over stabilization and drift demonstrated in the previous tests ${ }^{8}$.

The third gun, modified and firing a modified shell, was tested in 1854 in Turin. Unlike the previous tests, only one charge weight was used, 2,3 kilos, and only the long nosed shell was fired. The weight was reduced to about 31 kilos with the conversion of the two splines into four "buttons."

Table 2.

| Shell, <br> kg | Charge, kg | Elevation | Muzzle velocity, <br> $\mathrm{m} / \mathrm{sec}$ | Range, m | Drift, m |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 31 | 2,3 | $10^{\circ}$ | 305 | 2805 | 2,80 |
| 31 | 2,3 | $15^{\circ}$ | 305 | 3784 | 3,20 |
| 31 | 2,3 | $20^{\circ}$ | 305 | 4510 | 3,75 |
| 31 | 2,3 | $25^{\circ}$ | 305 | 5103 | 4,75 |

A new 8 -pdr gun tested at the same time was reported to have performed quite well, achieving a range of 2423 meters at 25 -deg elevation ${ }^{9}$.

Following the unsuccessful trials at Shoebury Ness, the Belgians became interested in Cavalli's work. They had an 18-pdr cast, with Cavalli's breech mechanism, but some modifications to the rifling. The two grooves were rounded with a width of $5,2 \mathrm{~cm}$ and a depth of $3,2 \mathrm{~cm}$. The two splines were replaced with two rounded buttons of virtually identical width, but allowing windage of 2 mm . But the shot moved freely in the bore, and so did not produce good results. A Captain GilIion of the Belgian artillery suggested that a pair of buttons/studs for each groove of the rifling would produce better results ${ }^{10}$.

W ith the successful trials in Turin, Col. Cavalli passes into history. His enduring legacy, however, is the wedge form of breech mechanism, which will appear again in this story.

[^5]One brief sideline remains to be examined. As Cavalli had used a form of "shunt" rifling first invented by Col. Treuille de Beaulieu, the highly capable French artillerist, in 1842, an examination of French developments is in order.

While the trials in Akers and Shoebury Ness were not completely successful, they did spur the French to begin serious development at the A rsenal at V incennes, in 1851. De B eaulieu used a 22 cm gun re-bored to a 30 -pdr. The first experiment was much the same as the Belgian gun already mentioned, or perhaps worse, save that they were testing a M uzzle Loading Rifle. Using the single stud/button allowed considerable "play" of the shell within the bore. Careful measurements demonstrated a variance of 1 deg 7 minutes in the angle of the shot leaving the muzzle ${ }^{11}$.

The French quickly adopted the two studs suggested by Cap't. Gillion, and the first serviceable gun, the M 1855, was quickly put into production. The gun tube would have been virtually the same as that of Cavalli, though a MLR. With a caliber of $16,5 \mathrm{~cm}$ ( 30 -pdr) it fired an oblong projectile weighing 26,4 kilos at a M V of $347 \mathrm{~m} / \mathrm{sec}$. Some of the first from the foundry were rushed to the Crimea, but arrived too late to see any service in that war. The gun did give good service in China and Cochin China (Indo-China), and were very effective against the A ustrians in the 1859 war.

Col. de Beaulieu, however regarded the M 1855 as a starting point only. Development continued, altering the rifling system from two grooves to three, at a varying pitch, and the introduction of a "gas check" attached to the rear of the projectile. This design was tested successfully, and became the M 1858/60 MLR, and comprised the original armament of Gloire M odified versions of this gun were also used to arm the first Italian ironclads, but that is beyond the scope of this tale.

With the M 1858/60 in production, de Beaulieu turned his attention to developing a breech loader, and began experimenting in 1859. He took the M 1858/60 as a starting point, but rejected the Cavalli wedge and the vent piece used by A rmstrong. He finally settled on the interrupted screw, which had been patented in the United States in 1853 by John P. Schenkl and A dolph S. Saroni. Test firing was successful, and the design entered production as the M 1860.

Performance of both the M 1858/60 and the M 1860 was the same. With the same 69 lb . projectile, MV was $317 \mathrm{~m} / \mathrm{sec}$. and a range of 6438 meters was achieved at an elevation of 40 deg. Deviation for range was 107,9 meters, and drift was 14,9 meters ${ }^{12}$.

## II. Wahrendorff

B aron M artin von W ahrendorff (1789-1861) was without a doubt one of the most talented gun designers of the $19^{\text {th }}$ century. He inherited the A kers styckebruk [foundry] and became one of its chief designers. He also sought to market the guns made from the high quality and plentiful iron ore available in his native Sweden.

[^6]Certainly A kers could and did manufacture the standard smooth bore muzzle loaders of the day. In 1836, they manufactured thirty 30 -pdr M /35 guns for foreign sale. A nd in 1844 they completed forty similar but lighter versions of the same gun for the Swedish Navy ${ }^{13}$.

The Baron, however, felt that such guns, and the standard carriage that was used to mount them, were really inefficient for the tasks, and wasted space in circumstances where space was at a premium. This included both on board ship, and in fortress casemates. In short, he saw breech loading as the solution ${ }^{14}$.

In 1837, Baron Wahrendorff obtained a patent for the design of his breech mechanism. General Sir Howard Douglas provides a description of the 30-pdr ( 6.37 inch) used for the A kers test in 1846, which deserves to be quoted at length:


Studded projectile with gas check from Shirokorad's Encyclopedia of Russian A rtillery


A s depicted in " $B$ aron $M$ artin von W ahrendorff"
"A rectangular wedge, 31 cm long, $20,5 \mathrm{~cm}$ broad, and $10,8 \mathrm{~cm}$ thick, is made to slide, towards the right or left hand, in a perforation, formed transversely through the breech, for the purpose of covering, after the gun is loaded, the aperture by which the charge is admitted into the bore. A notch $18,3 \mathrm{~cm}$ long and $1,8 \mathrm{~cm}$ broad is made longitudinally in the wedge, and through this passes the stem, or bar, of a cylindrical plug, by which the charge is kept in its place [a]. This plug is $18,8 \mathrm{~cm}$ diameter and 12 cm long, and it is provided with a stem or bar, 40 cm long, at the extremity of which is a screw nut having two handles [g]. The plug is introduced in a direction parallel to the axis of the gun, through an orifice in the breech; and its stem passes through a perforation made in an iron door which closes the orifice. When the gun is loaded the door is closed; the plug is pushed forward, to the rear of the charge, by means of its stem. [Then cylinder ' $b$ ' is inserted behind the plug, as the main source of strength to withstand the force of the propellant explosion] And the wedge is made to slide into its place: a turn of the screw nut at the end of the stem is then taken, when the whole is drawn tightly together and is ready for firing." ${ }^{15}$

The first gun, a 12 -pdr (about 12 cm ) was cast in 1840. It was an unchambered smooth bore, which was dubbed the $\mathrm{m} / 41$ after testing and adjustments.

[^7]It was submitted for trials at V axholm the next year. Further trials were conducted in 1845 aboard the ship-of-the-line M anligheten.

These trials were not entirely satisfactory, and development continued ${ }^{16}$.
The projectile used was the normal solid ball or hollow shell, all spherical. However, to avoid the problem of windage, Wahrendorff coated his projectiles with lead, which provided the seal. The effect was to increase the weight of the projectile on the one hand, and to take full advantage of the propellant gasses on the other ${ }^{17}$. Regrettably, no performance data is to hand for these breech loading smooth bores. But it seems reasonable to conclude that it would have been approximately equal to that of the usual smooth bore muzzle loaders of the time.

Even while the development of his smooth bore guns continued, the B aron began experimenting with a rifled gun tube. He did not, however, adopt the 'shunt' system of rifling that de Beaulieu had invented the previous year. Rather, he used the polygroove form first used by Reichenbach back in 1816, and used successfully in rifled muskets and small arms. But he retained the lead coated shot, as the coating would adhere to the rifle grooves and center the shot in the bore, while retaining the seal.

A s al ready mentioned, M ajor Cavalli arrived at A kers in 1846, to oversee the manufacture of some smooth bore guns for the Sardinian government. The meeting of two such talented and creative men was bound to produce many exchanges of ideas and lively discussions. In the absence of comments concerning any hostility between them, we can only assume their interaction was congenial. General Douglas hints at this by noting that the trials in that September were "experiments for the purpose of testing the merits of their shot... "

Cavalli seems to have convinced the Baron of the merits of conical projectiles, and even to test the same rifling scheme. W ahrendorff had a 30 -pdr prepared with the tube rifled according to Cavalli's specifications, and had some projectiles made for it, using the same splines to grip the grooves. General Douglas comments that the performance of the Wahrendorff guns was virtually identical to that of the Cavalli guns. But this is only to be expected, for by duplicating the conceptual flaws, he al so duplicated the less than successful results.

However, the Baron also lad some lead coated conical projectiles made for his poly-groove rifling. Douglas notes that fact, but without detailed comment. He merely states that, "It must be admitted that the W ahrendorff gun has considerable advantage, in respect to range, over the English 32-pounder at a high elevation... [and] stood well, the wedge [sic] resisting more effectually the force of the discharge than that of the Cavalli gun." ${ }^{19}$

[^8]

W ahrendorff B reech L oading Smooth B ore M. 1855 (compliments of L ars A hlberg)


Photo of $\mathrm{m} / 41$ gun from Hans $M$ ehl's N aval Guns, manufactured in 1845. N ote the naval truck carriage.


Douglas continues, probably more contemporaneously with the publication of his manuscript, and referring to the $\mathrm{m} / 54$, that: "Baron Wahrendorff has invented a 24 -pounder gun, which is also to be loaded at the breech. It is mounted on a castiron traversing carriage; and, taking little room, it appears to be very fit for casemates. The upper part of the carriage has, on each side, the form of an inclined plane, which rises towards the breech, and terminates near either extremity in a curve whose concavity is upwards. Previously to the gun being fired the trunnions rest near the lower extremity; and on the discharge taking place, the gun recoils on the trunnions, along the ascending plane, when its motion is presently stopped. After the recoil, the gun descends on the plane to its former position, where it rests after a few short vibrations. The axis of the gun constantly retains a parallel position, so that the pointing does not require readjustment after each round... The gun was worked easily by eight men, apparently without any strain on the carriage. With a charge of 3,63 kilos and with solid shot, the recoil was about one meter,
and the trunnions did not reach the upper extremity of the inclined plane, though the surface was greased. ${ }^{20}$

Trials In 1848, perhaps with the 12-pdr type in the photo above, and the sales of all types of Wahrendorff guns followed. Complete data is not available at this time, but below is listed what is known:

1845: part of an order given to Finspong for 108 82-pdrs standard smooth bores caliber 226.2 mm (c. $8.9^{\prime \prime}$ ). The entire order was manufactured in three installments: 1843 by Finspong, 1845 by A kers, and 1853-55 by Finspong. Thirty of these guns were aboard the Swedish warships Stockholm, Skandinavien, and Forsiktigheten.

1844-53: Nineteen 60-pdr m/44 for foreign sale.
1852: An unknown number of 24 -pdr $\mathrm{m} / 52$ ( 155 mm ) were manufactured for the C oast $D$ efence, These guns had a bore length of 11 calibers.


Courtesy of Lars A hlberg. Note the carriage.
1853: Seventy $30-\mathrm{pdr} \mathrm{m} / 53$ mounted aboard the Swedish warships F orsiktigheten (22), Stockholm (22) and Skandinavien (22). Some of this order was manufactured by Finspong in 1853, and Stafsjo in 1856.

1853: It appears that a lighter version of the $\mathrm{m} / 5330$-pdr was also manufactured, all by A kers. They were mounted on the Swedish warships Norrkoping (18) and Stockholm (20).

1854: Two versions of the $\mathrm{m} / 54$ 82-pdr were manufactured for Coast D efence. While the number is not known, the lighter version had a bore length of 9.5 calibers, and the heavier 11 calibers ${ }^{21}$.

Information on the sale of Wahrendorff rifled guns is even less precise, and perhaps even controversial. For example, one of the Swedish documents states that

[^9]no Wahrendorff guns were in Swedish service, while the documents from which the above list was taken disproves that in detail. Y et no reference is made in them to any of the $W$ ahrendorff rifled guns being in Swedish service. Indeed, the entry for the $16.7 \mathrm{~cm} \mathrm{~m} / 69$ ( $30-\mathrm{pdr}$ ) gun manufactured by Finspong specifically states that it was mounted on the screw frigate Vanadis, which was launched in 1862. Other sources, however, including Conway's, note that she carried eight 6.6" BL guns as part of her armament. So either we must believe that the ship sat idle for seven years, or the guns were W ahrendorff BLs. W hether rifled or smooth bore is difficult to say, but the timing argues in favor of rifled guns ${ }^{22}$.

Foreign sales are difficult to determine and quantify. But below is a list of what is known and suspected:

1843: The Prussian A rmy bought three of the smooth bore breech loaders for tests: 6-, 12-, and 24-pdrs.

1851: The Prussian Army bought a 12-pdr (12cm) BLR for tests. Over the next two years, guns of several other calibers were purchased for additional trials. And in 1854, the A PK (ArtilleriePrufungsK ommission) of the Prussian A rmy actually recommended that the 12 -pdr be adopted ${ }^{23}$.

A ustria-Hungary purchased W ahrendorff guns in large quantities. At the B attle of Heligoland in 1864, the frigate Schwarzenberg carried 6 smooth bore 60pdrs, 40 smooth bore 30 -pdrs, and 4 rifled $24-$ pdr BLs, while Radetzky mounted 4, 24 and 3 respectively. The rifled 24 -pdrs were definitely $W$ ahrendorff guns, m/61. How many of the smooth bores were also is a question.

B ut the most famous use occurred two years later, at the B attle of Lissa. The A ustrian fleet mounted at least 115 W ahrendorff 24-pdr ( 15 cm ) BLRs. There is also reference to a number of rifled 48-pdrs taken from fortresses to arm the Ferdinand Max and Habsburg. From the after action reports, the breech loaders fired faster and more accurately than the Italian rifled muzzle loaders.

In addition, guns were exported to B avaria, B razil, Egypt, B ritain, France, The Netherlands, N orway, Portugal, Spain, The Ottoman Empire, and the USA. The Danes also purchased a number of 4 -pdrs $(8.33 \mathrm{~cm})$ as both field guns and light guns for naval use. The barrel was 20 calibers, and fired a 4,7 kilo Common Shell with a 0,2 kilo black powder bursting charge, as a muzzle velocity of $370 \mathrm{~m} / \mathrm{sec}^{24}$.

1859: Russia ordered twenty 30-pdr BLs, which were delivered in 1862. However, these were 'blanks' so they could experiment with various systems of rifling. In one barrel, they tried the Armstrong system of small grooves and lead coated projectiles, but the shells broke up in the barrel and accuracy was bad. In another the shunt type developed by de Beaulieu, and in the third the "Prussian" [K rupp] system. All were tried at V olkov in September, and the decision was made to rifle all using the Prussian system. This work was done at the St. Petersburg Ar-

[^10]senal. Then the guns were used in the fortresses of $K$ ronstadt and around St . Pe tersburg. This rifling system was considered as the forerunners/prototype for their M 1867 family of guns ${ }^{25}$.

1858: The Prussian N avy ordered ninety guns for the Gefion, Arcona and Gazelle ${ }^{26}$. These were probably rifled breech loaders.

The W ahrendorff rifled breech loaders were very successful, and well designed, the larger calibers being chambered. The overall length of the 24-pdr was 21 calibers, and the bore was 18.4 calibers. The Russian 30 -pdrs were proportionately the same. The rifling was also very gentle, at the rate of one turn in 63.2 calibers.

There is little information on the performance of these guns. The Table below gives the information for the Austrian and Russian guns, and it may be assumed that the guns in other navies would be similar.

Table 3.

| Gun | Shell, kg | Charge, <br> kg, | Elevation | Muzzle velocity, <br> $\mathrm{m} / \mathrm{sec}$ | Range, m |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $24-\mathrm{pdr}$ | 27,7 | 2,15 | 14 | 310 | 3068 |
| $30-\mathrm{pdr}$ | 36,6 | 2,75 | 24 | 292 | 4867 |

For the 24-pdr, the data applies to the lighter Common explosive shell. A heavier armor piercing shell was available, as were so-called 'battering' charges. For the $30-\mathrm{pdr}$, the data applies to the armor piercing shell but with the 'light' charge. Common explosive shell was available ${ }^{27}$.

When M artin von Wahrendorff died on January 20, 1861, the A kers styckrbruk was taken over by A. von Stockenstrom and M.L. Berg, his illegitimate son. Gun production ceased in 1866, though the foundry continued to manufacture projectiles for some years. B ut the B aron had made several significant contributions to the field of artillery. He developed a workable breech mechanism, and an advanced traversing carriage. He proved the superiority of poly-groove rifling, and his lead coated projectiles demonstrated the importance of a good gas seal. Guns of his design and manufacture participated effectively in two naval battles. In short, he left a legacy of innovation and scientific development ${ }^{28}$.

But his greatest and lasting contribution occurred in 1859, when his latest models were tried by the Prussian War M inistry, and the design was selected for production! For the Prussians, however, the main question was of what material should the new guns be made: bronze, cast iron, or the very expensive cast steel ${ }^{29}$. A nd therein lies the rub...

[^11]

M odel of the 24-pdr from Hans M ehl's Naval Guns.

## III. Krupp

At the beginning of 1859, Alfred K rupp was not a happy man. Oh, his steel products were in great demand, for everything from railroads to fortresses to building material. But he had had almost no success in breaking into the lucrative market for artillery.

In 1841 the K rupp Werke had received some orders for 23 cm and 28 cm cannon for the Coast Defence. And they had participated in re-arming the Artillery with system C/42 smooth bore guns ${ }^{30}$.

Sometime around 1845 the French Army had purchased a single cannon for tests, which were duly conducted at the A rsenal at V incennes.

In 1855, the K hedive of Egypt purchased a number of guns. These were most likely the 30 -pdr smooth bores that were still in use in 1882 in the fortifications at A lexandria ${ }^{31}$.

But the Navy shunned his overtures. Their reasoning seems to have been that foreign sales bestowed a "legitimacy," or perhaps acceptability, to the gun maker, and Herr K rupp had few such sales and therefore little to recommend his product. So they purchased their ship borne artillery from foreign suppliers.

In J une of 1853, the newly commissioned Danzig had its armament of twelve guns shipped in Britain. Two years later, the Swedish firm of Finspong received an order for 48 guns, to be fitted in Thetis, Frauenlob, and Hela. A nd as previously mentioned, A kers received an order for 90 guns in 1858. Even small rifled guns for the new warships were ordered from Spandau ${ }^{32}$.

[^12]It would not be an understatement to claim that the decision facing the W ar Ministry following the trials of the Wahrendorff guns in 1859 was a "make or break" situation for K rupp. If the M inistry came down in favor of iron, then much of the work would go to Swedish foundries, probably A kers and Finspong. If they decided in favor of bronze, a traditional favorite of gunners, then K rupp would be unlikely to participate at all. Then the consequences could be a K rupp Werke on the fringes of the armaments industry, with the Prussian/German Army and Navy purchasing their artillery from foreign suppliers. So to understand the decision, it is first necessary to understand something of the materials involved.

Bronze suitable for cannon is composed of 90 parts copper and 10 parts tin. Increase the proportion of tin makes the bronze harder, but more brittle and hence liable to catastrophic failure. Decrease the proportion of tin, and the bronze is too soft for cannon, and loses some of its elasticity. But properly made, the Tensile Strength is about 45,500 pounds per square inch ${ }^{33}$.

The French Army went to war in 1859 with bronze 4 - and 12 -pdr guns. But this was just an expediency, as their order to K rupp for steel castings could not be filled in time. When hostilities ended, the French Emperor ordered all of the bronze guns melted down and the metal sold; the proceeds to be used to buy cast steel ${ }^{34}$.

As a material for cannon, bronze did have some critical disadvantages. It was subject to slight corrosion from general atmospheric causes, and more so from the gasses created by the burning of the black powder propellant. A nd the tin is liable to melt away at corners by the heat generated from rapid firing, in addition to that caused by the propellant. Being "soft" it is also liable to serious injury from the projectile bouncing around inside the bore; such impact also creating small corners ${ }^{35}$.

The characteristics of iron were well known, given that wrought iron was state of the art. Good wrought iron had a Tensile Strength of about 60,000 pounds per squire inch, about twice that of cast gun-iron. Iron had been the preferred material for heavy cannon for 300 years, popular with the gunners and the Generals ${ }^{36}$.

Steel was another matter entirely. There was a general suspicion on the part of gunners that it was likely to burst/fracture catastrophically and with no warning. Several steel guns had burst explosively during proof, causing causalities. This was because the margin between the elastic limit and rupture was very small.

The Tensile Strength of steel suitable for cannon is about 90,000 pounds per square inch. Bessemer, working at the W ool wich A rsenal, developed a process of hammering the steel to remove bubbles and imperfections, which would increase the Tensile Strength to about 145,000 pounds per square inch. But Friedrich K rupp believed that the Bessemer process was insufficient, and developed his own.

The K rupp guns were made of "crucible" steel. But the word "crucible" is not used in the original sense, but rather signifies that the ingredients are melted together in crucibles before being cast. The crucibles used were rather small, and each con-

[^13]tained a different recipe depending upon what portion of the gun was being poured; the material being tailored to give the most desirable characteristics for each portion. The goal was to create a large margin of safety betw een the elastic limit and the fracture limit. Early proof of his success was the trial at the A rsenal at Vincennes, when 3000 shot were fired from the smooth bore without degradation of the barrel. It has been claimed that K rupp steel had twice the strength of wrought-iron, without the bubbles or other imperfections that plagued other steels ${ }^{37}$.

The A PK had tested K rupp cast steel in 1855, so on their advice, the contracts were let to the K rupp Werke. It was also decided that the first priority should be the field artillery. Production commenced promptly, turning out guns of $6-, 12$ - and 24 -pdrs (roughly 9,12 and 15 cm$)^{38}$.

But from this point, the story becomes rather convoluted, and is best broken down into separate lines of development.


A ustrian 12cm (12-pdr) Cannon M 1861, shown with an old smooth bore 8-pdr.


C/61 A mmunition. Pictured are nose fuzed Common shell, Schrapnel, Timed fuze explosive, and Case shot.

[^14]

C/61 and M 1861 with A mmunition Carriage

## Prussian A rtillery

The order for the first 100 steel blank tubes was signed by the Prinzregent, Wilhelm I, who personally increased the amount to 300 tubes. K rupp was to cast the tube according to specifications, and then ship the blanks to the K onigliche Geschutzfabrik, the R oyal A rsenal, at Spandau, to be finished. From the point of view of the Prussian government, this arrangement made good financial sense. Steel was a very expensive commodity. Given that the Spandau A rsenal was already supported by the government, their work did not represent a great increase in expense beyond the monies paid to K rupp ${ }^{39}$.

This arrangement presents an important distinction. W hile K rupp was responsible for the steel gun tube, Spandau was responsible for the breech mechanism. So as often happens when dealing with a government agency under mandate to save money, Spandau tinkered with the design. M ost of the "improvements" over the original Wahrendorff design were harmless, but one deserves comment. Spandau replaced the brass obturator pad with one made from wood shavings! As wood tends to smolder, the seal weakened, allowing gases and soot to escape, to the dismay of the gunners ${ }^{40}$.

Complaints from the Artillery caused Spandau to provide an "improved" breech mechanism. K nown as the K reiner Breech after the designer, it proved an expensive failure! The resulting guns were known as the C/64.

Production of the C/61 and subsequent C/64 had been steady, but no doubt for financial reasons, at a moderate rate. Hence, fully one third of the artillery of the Prussian A rmy during the war against Austria in 1866 was the smooth bore C/42! These old short ranged guns were at the mercy of the more modern A ustrian artillery, composed mostly of the M 1861! But the performance of the C/64 was a repeat of the experience two years earlier during the D anish W ar!

Nathan Okun, perhaps the leading expert on the phenomenon of naval ferrous armor penetration, comments that "the two-piece design is somewhat weaker than

[^15]a single piece design... the reduction in strength is due to the inability of the two pieces to prevent each other from spreading sideways under the blast force near the crack between them, something that cannot happen in a single solid piece of steel. Thus, they can deform/crack separately in different directions, especially the front [inner] plate being hit directly by the powder blast, eventually resulting in the support from the back plate no longer being uniform or strong enough and the front plate will bend or break, allowing blast gasses to get around it and... making the gun unusable or... blowing the breech off." The result was that over time the K reiner wedge plates would bend, or the inner plate would break, under the stress of firing. A lso, the square breech opening, without any taper or rounding, offered a convenient corner for the concentration of forces, resulting in cracks in the breech block which could lead to structural failure ${ }^{41}$.

$K$ reiner Breech of the Prussian C/64
The reaction by the Prussian Ordnance Corps was to halt production of the $\mathrm{C} / 64$, and revert to the $\mathrm{C} / 61$. The existing $\mathrm{C} / 64$ guns were to be returned to Spandau, as convenient, to be repaired. These repairs amounted to drilling the square breech blocks, which they had forged onto the K rupp tube, for an insert suitable for the W ahrendorff cylinder and retainer pin; in other words, converting the $\mathrm{C} / 64$ into $\mathrm{C} / 61$. However, given the number of guns involved, the work was not completed in

[^16]time for the French War of 1870, though at least the old C/42 guns had been recycled ${ }^{42}$.

## K rupp's Own Production

At about the same time that K rupp was given the first order for the field artillery blanks that became the $\mathrm{C} / 61$, the War Ministry also ordered 24 -pdrs for the Coast Defence. But this was a low priority order, given that few suitable positions existed at the time. Great impetus was provided during the Danish War of 1864, when their ironclad Rolf Krake threatened to sail into Flensburg harbor. It took several $24-\mathrm{pdr} \mathrm{C} / 61$ guns from the siege train to drive her off ${ }^{43}$.

The Navy also ordered 24 -pdrs at about the same time. They had an immediate need to arm nineteen gunboats of the J ager and C hamaleon classes. Each carried one 24 -pdr and two 12 -pdrs of the C/61 type ${ }^{44}$.

These two orders seem to be the last of the W ahrendorff C/61 design manufactured for K rupp's own customers. The K rupp engineers had carefully and completely examined the strengths and weaknesses of both the Cavalli wedge and the W ahrendorff cylinder, and reached some conclusions. Cavalli's wedge was a good starting point. When combined with a B roadwell ring, it provided good obturation, but lacked strength to resist the pressure of large propellant charges, only being supported by the structure of the gun tube around the periphery. What was needed was the additional strength provided by the W ahrendorff cylinder, but without the complexity of his system of obturation. By removing a portion of the cylinder to provide a flat face, and attaching that to the Cavalli W edge, they retained the advantages of each component. The finished design resembled a rounded "D" and became known as the K rupp System., or cylindro-prismatic wedge ${ }^{45}$.


K rupp wedge. Compare with C/72 in the Conclusion.
A vailable evidence indicates that the K rupp System was in place in 1860-61. The 4-pdr Field guns ordered by the Saxon A rmy were so constructed. So too were the guns sold to foreign countries.

[^17]The orders from the Prussian government bestowed the "legitimacy" that Krupp has so long sought. As a result, foreign orders flowed into Essen, and K rupp's reputation increased accordingly.

Russia became one of K rupp's largest and best customers. Beginning in 1863, she ordered hundreds of guns and blanks of all sizes. The list below is a sample only:

18631004 -pdrs, 688 -inch and 308 -inch blanks, 24 -inch blanks, and at least one 11 -inch.

1865250 9-pdrs.
1866 an undetermined number of 9 -inch.
1867 411-inch.
1871 at least one 12 -inch ${ }^{46}$.
A ustria also began purchasing heavy guns from K rupp. Their first order was placed in 1864 or 1865 , for at least 288 -inch ( 68 -pdr) guns for the ironclads Erzherzog F erdinand Max and Habsburg, then under construction. Delivery of these guns was delayed at the behest of the Prussian government as war approached. They were finally delivered, probably in 1867, and they were definitely on board the intended ships by 1869. But over the next eight years, K rupp supplied 129 inch $(23.54 \mathrm{~cm})$ for the ironclad Lissa, 826 cm for the ironclad Custoza, 824 cm for the ironclad Erzherzog Albrecht, 109 -inch ( 23.54 cm ) for the converted ironclad Kaiser, 628 cm for the ironclad Tegetthoff, $3015 \mathrm{~cm} / 26$ for the frigates Radetzky and Laudon, and two 21 cm for the sloop $F$ asana ${ }^{47}$.

In around 1864, Spain purchased four 24-pdrs for the frigate Gerona, and around 1866, the Netherlands began purchasing 12 -pdrs for the light guns on their ironclads. A nd for an element of mystery, the Egyptian frigate M ehemet Ali was armed with a mixture of twenty Krupp 12-pdr and ten Armstrong 40-pdr BLRs. These were virtually the same caliber ( 12 cm and $12,1 \mathrm{~cm}$ )! The Ottoman Empire purchased ten 24 -pdrs and several 6 -pdrs for their frigate Selimieh ${ }^{48}$.

There are a series of minor mysteries involving foreign sales during the 1860s, mostly created by inaccurate primary information, and perhaps exacerbated by typographical errors. Below is a discussion of several samples.

In 1864, A. Hall of A berdeen launched a small ironclad sloop in speculation of selling her to the Confederate States of A merica. She was purchased in 1869 by Prince K umamoto and arrived at Nagasaki in January 1870. By the end of the year she had been presented to the Emperor as the Ryujo. But sources differ regarding her armament, and its origins. It appears that she mounted two 6.5 -inch and ten 5.5 -inch Breech Loaders. That the 6.5 -inch guns are breech loaders limits the potential manufacturers to the French ( 16.5 cm ) or K rupp ( $16.7 \mathrm{~cm} 30-\mathrm{pdr}$ ). A nd for the 5.5 -inch, the field includes the French ( 13.9 cm ), K rupp ( 18 -pdr, roughly

[^18]14 cm ), and A rmstrong ( $70-\mathrm{pdr}$ ). We can probably eliminate the French from consideration for reasons of quality and policy; to wit, French manufacturers were not allowed foreign sales for fear of giving away their "secrets." This implies that the 6.5 -inch gun came from K rupp. A nd by inference, the 5.5 -inch were probably also from K rupp.

An unknown shipbuilder (or agent?) in London provided three ships that eventually became part of the Imperial Japanese Navy. One was the Monshun,launched in 1865 as the British steamer Eugenie but sold to the Hizen Clan in February 1868. Sources agree that she carried a 7 -inch Forbes smooth bore, and that the second heavy gun was 5.5 -inch caliber. But one source, W atts and Gordon, state that it was an Armstrong muzzle loader, while another that it was a K rupp breech loader. The latter seems more likely, given the information below.

Launched in 1867 as the British steamer Hinda but sold to the Choshu Clan, Dai Ichi Teibo was armed only in M arch 1869. She received two guns, the larger given variously as a 6 -inch MLR, a 5.9 -inch MLR, and a 5.9 -inch BLR. There is agreement that the other gun was a $5.5-\mathrm{inch}(18-\mathrm{pdr}) \mathrm{K}$ rupp BLR. It therefore seems likely that the larger gun was al so a K rupp 24-pdr BLR.

The last ship, launched in 1866 as the B ritish steamer Assunta, was also sold to the Choshu Clan and became the Dai Ni Teibo. She was armed with two guns of the same caliber, given variously as 6.7 -inch A rmstrong BLR , or as 6.5 -inch K rupp BLR. While A rmstrong surely could have produced such an "unusual" caliber gun as a $6.7-\mathrm{inch}(17 \mathrm{~cm})$ gun, it seems quite unlikely. So it is more reasonable to believe that the guns were K rupp 30 -pdrs.
J.S. White of Cowes built a wooden paddle frigate in 1863, nominally for China as the Chiangtsu. Curiously, the Chinese government refused to ratify the purchase. Given the timing, it is quite possible the ship was originally ordered by the Confederacy who then could not pay, or that she was built on speculation for sale to the Confederacy, potentially as a blockade runner. The ship was sold to the Prefect of Satsuma in 1867, and became part of the Imperial Navy in 1869, as Kasuga. Sources agree that she carried one 7-inch Forbes smooth bore muzzle loader and two 30 -pdr smooth bore muzzle loaders. But there is no agreement about the other four heavy guns. One source states that they were 5.1 -inch BLRs, and another 4.5 -inch BLRs. B oth are odd and unlikely calibers! It therefore seems more reasonable to infer that the original manuscript documentation was virtually unreadable. So if the " 1 " and " 4 " were actually another number, then it is possible, or even likely, that the guns in question were really $5.5-\mathrm{inch}$, which would be in line with the armament of M onshun noted above, and by inference, that J.S. White may also have build that ship.

The firm of Denny in Glasgow built a composite screw corvette under the name Pampero as a commerce raider for the Confederacy. She was acquired by Chile, but captured by the Spanish during their 1864-66 W ar, while on the passage from the builders. Re-named Tornado in Spanish service, her reported armament was one 20 cm M LR, which was a Palliser conversion of their $20 \mathrm{~cm} \mathrm{No}$.1 modello smoothbore. Also listed are two 6.4 -inch BL and two 4.7-inch MLR. At that time, only France and K rupp manufactured $30-\mathrm{pdr}$ BLRs, and as mentioned above, the

French were not exporting their guns. So it is reasonable to infer that those two guns were from K rupp. The 4.7 -inch were most likely A rmstrong 40-pdrs.

Chile acquired a wooden screw frigate Chacabuco in 1866, from an unknown British source, which may have been built on speculation for sale to the Confederacy. Her reported armament was three 8.2 -inch, two 70 -pdrs, and four 40 -pdrs, supposed all Armstrong BLRs. But the three big guns were not a standard Armstrong caliber (21cm), though it was a standard K rupp caliber. While it is possible that A rmstrong could manufacture three non-standard guns to order, it is more likely they were purchased from K rupp.

A nd finally, there is the mystery of the Fujijama, also listed as the Fuji. Information about her is full of contradictions. She is listed as a wooden paddle frigate, though drawings do not show a paddle, unless it is internal, which is not mentioned. And at 1000 tons, she is really too small to be a frigate. Supposedly she was built in New Y ork for the Union Navy between 1863 and 1865, and strongly resembles the Resaca class. There are indications that she was ordered by the Shogun, who did acquire her in 1866, and so would not appear on the U.S. Navy lists. Her original planned armament was to have been 24 guns, but her hull was pierced for only five guns on each broadside, for unidentified smaller guns. Her heavy guns comprised one 6.3 -inch ( 30 -pdr) M LR, and two 5.9 -inch, type and manufacturer unknown. It is possible that the 5.9 -inch guns were K rupp 24 -pdrs, at the behest of the Shogun ${ }^{49}$.

## Naval Guns

The road to success with the Prussian Navy was still full of pot holes and obstacles. The War Ministry had observed that the 24 -pdr would be insufficient against armor, knowing the results of the French experiments in 1858 and 1861. They were aware that larger gun calibers would be necessary in the battle between armor and gun power.

In 1862 they ordered a few iron 17 cm guns from K rupp, probably motivated by parsimony. They were tried in 1864, and not surprisingly, found to be unsatisfactory ${ }^{50}$.

In the fall of 1864 , the $N$ avy decided to accept steel guns, and ordered 17 cm and 21 cm guns. But the Prussian Ordnance Corps had not yet lost faith in the K reiner breech, so K rupp was required to use it with the new guns.

In 1865, K rupp received a Contract with the navy for over 100 guns, to replace the various Swedish guns on the unarmored screw ships. Also, toward the end of the year, the eight ships of the Camaleon class were fitted with a rifled 68pdr in addition to their 24 - and 12 -pdrs. These guns were most likely the short $21 \mathrm{~cm} \mathrm{~L} / 12.25$ guns similar to those ordered by the A ustrian Navy.

[^19]Firing trials the next year, possibly using one of the 8-inch guns not delivered to A ustria, indicated that the 21 cm caliber was only marginally effective against the thicker armor being applied to ironclads, so 9 -inch ( $23,54 \mathrm{~cm}$ actual) guns were ordered, also with the K reiner Breech ${ }^{51}$.

1867 and 1868 were the absolutely critical period for K rupp and the Prussian Navy. Part was obviously technological, but the rest was pure politics. The Navy wanted the most modern and powerful guns for their new ironclads. K rupp desperately wanted that business. A nd the Prussian government did not want to be dependent upon a foreign supplier for the heavy guns needed by the Navy. To make everybody happy, K rupp guns must show well in a series of trials.

The second of these took place in May 1867, in two parts. The first involved one of the $21 \mathrm{~cm} \mathrm{L/19}$ guns ordered in 1864. A long side of it was a $21 \mathrm{~cm} \mathrm{L/19}$ gun provided by K rupp, with the cylindro-prismatic wedge. During the endurance test, the inner plate of the K reiner wedge split. A new wedge replaced the broken one, and the firing continued without interruption. But the incident did have serious consequences. First, the Ordnance Corps abandoned the K reiner wedge, and in July ordered 20 new 21 cm guns with the K rupp wedge. But they also refused to accept the guns with the K reiner wedge, now considering them unfit to meet the requirements of naval service. This action, correct though it may have been, caused a considerable delay in providing the armament for Kronprinz and Friedrich Karl, which had been delivered from the builders in August 1867, and forced to sit idle at K iel. The new guns could not be delivered before July $1869^{52}$.

The first trial pitted the new Krupp 9 -inch $(23,54 \mathrm{~cm})$ gun against an Armstrong 9 -inch [22,9cm] MLR. Three targets were prepared for the trial, representing the side of an armored ship. The first had a 6 -inch plate on 10 -inches of teak on a 1 -inch skin. The second was a 7 -inch plate on 30 -inches of backing. The third duplicated that of the Konig Wilhelm with 8-inches of armor with 10 inches backing and a 0,75 -inch skin. The guns were put in position 950 meters from No. 1, 750 meters from No. 2 and 500 meters from No. 3.

The Armstrong gun was fired four times at target No. 1, twice at No. 2 and once at $\mathrm{N} . \mathrm{B}^{3}$, but each shot pierced the target. The first shot from the K rupp gun at No. 3 pierced the 8 -inch plate but only 7,5-inches of the backing. The second shot at No. 2 pierced the target but the Gruson shot broke up passing through. The A rmstrong gun had produced an initial velocity of $400 \mathrm{~m} / \mathrm{s}$, while the K rupp gun only $348 \mathrm{~m} / \mathrm{s}$. This showed a clear superiority of the A rmstrong gun. K rupp argued that the shell was defective, and the gun had the K reiner wedge, which leaked gas and limited the size of the propellant charge, and asked for a new trial. For the above mentioned political reasons, the matter of selecting heavy guns for the Navy was tabled ${ }^{53}$.

[^20]The next trial was in $M$ arch 1868. K rupp brought a new gun with his cylindroprismatic wedge, and hooped for additional strength. Gruson had provided new chilled shell. The results were better than the previous M ay, but were still not satisfactory. The gun could not produce enough muzzle velocity. K rupp blamed the "corned powder" that had been mandated by the APK, pointing out that the A rmstrong gun was using prismatic black powder [sic. actually pebble], and asked for another postponement.

Politics being what they are, another delay was granted. But many of the officers in the navy could not understand why K rupp could not produce effective naval guns when Armstrong could. Some even felt that the Navy should buy guns from A rmstrong. Fortunately, both the Ordnance Corps and the War M inistry felt that muzzle loading rifles would be a technical leap backwards.

The next trial commenced on July $2^{\text {nd }}$, with K rupp bringing the same gun, and also a supply of Prismatic powder obtained from Russia. But again they were disappointed, though the results were better than in M arch. The Gruson chilled shell did penetrate into the plate, but not nearly as well as the chilled Palliser shot from the Armstrong gun. K rupp again asked for a postponement to study the results, which was granted.

The next month, K rupp returned, bringing new steed armor piercing shell. The first shot from his gun shattered the target plate!

A fter this success, both guns were subjected to the endurance test. The Armstrong gun developed a fissure after round 138, and was a ruin after the $300^{\text {th }}$ round. But the K rupp gun was still in working order after 676 rounds, even though one of the chilled AP shells had burst in and injured the bore after the $640^{\text {th }}$ shot! Following this success, a new model $21 \mathrm{~cm} L / 22$ was tried at the medium range with the prismatic black powder, which performed better than had the A rmstrong gun. ${ }^{54}$ It was readily apparent that the future of naval artillery was long barreled steel breech loading guns!

## Condusion and Disaussion

The lengthy delay in resolving the competitive trials between the K rupp 9inch $(23.54 \mathrm{~cm})$ and the A rmstrong 9 -inch MLR were not without cost. The guns intended for K onig Wilhelm were delayed, and not delivered until late 1869. Between 1867 and 1869, the A ustrian ironclads Drache, Salamander, Kaiser Max, Prinz Eugen, and Juan de Austria, which had fought so valiantly at Lissa, were all re-armed with 7-inch A rmstrong guns, and the old steam line-of-battle ship K aiser, re-constructed as an ironclad between 1871 and 1873, mounted the A rmstrong 9inch MLR, for a total of 66 guns. But this brief interlude was the only incursion Armstrong enjoyed with the A ustrians. In 1874, the Kaiser Max class were "reconstructed" [a political fiction for obtaining new construction under the guise of improving obsolescent/obsolete ships, The U.S. Navy used the same process on some Civil W ar vintage monitors at about the same time.] and their MLRs landed.

[^21]28 of these guns were used to re-arm the Erzherzog Ferdi nand Maxand Habsburg. The "re-built" ships, and all other new construction for the A ustrian Navy, were armed with K rupp guns, at least until the turn of the century ${ }^{55}$.

Proponents of Armstrong, both contemporary and modern, cast the 1867-68 competitive trials as primarily a political matter, only obliquely referring to the technology involved, and then mainly citing the "poor performance" of the K rupp guns. Their intention is to infer that the K rupp guns were inferior and undependable products. When the technical matters are mentioned, it is in the context of implying that much of it was acquired from others. For example, the process of shrinking hoops or rings around the breech and chamber for additional strength was invented by A rmstrong or Blakely, and the carriage used by K rupp by V avasseur ${ }^{56}$. Each should be examined in some detail.

In a sense, both contestants in the first competitive trial suffered from the same malady; government interference. In the case of Krupp, as already mentioned, it was the mandated K reiner B reech and the 'corned powder.' In the case of Armstrong, it was the short-sightedness of the British armed services which rejected his breech loading rifled guns. This denied Armstrong the opportunity for further devel opment of the concept by reverting to rifled muzzle loaders.


The Armstrong MLR probably represented the limit of the technology possible. The construction was a steel 'A' tube, with a number of wrought iron hoops or rings shrunk around it for strength. Designed for black powder, the barrel length was rather short. In other words, the interior ballistics was rather fixed, in that the physical structure could not be altered easily. The short barrel could not efficiently use any version of a slower burning propellant. While later versions did have a chamber, it could not be altered once the gun was completed. In short, the propellant charge weight and the projectile weight could be altered, but the gun itself could not. These same objections would cause the Royal Navy to recant their decision ten years later.

The original K rupp barrels were cast solid, then rifled and 'finished' for their breech mechanisms. Being of crucible steel, which as noted above allowed each section of the gun to be cast with a recipe tailored to provide the optimum qualities for that section, K rupp did not originally see the need for hoops or rings.

However, when the need was realized in 1867, K rupp did indeed shrink high sted rings around the low sted barrel. But it is disingenuous to claim that the con-

[^22]cept was taken from Armstrong. Indeed, it was already in the public domain! Brooke, Parrott, and Blakely (who also had a claim as the original inventor) all used hoops in their designs. The Italians spend some months prior to the 1866 W ar installing hoops on their cast iron 16 cm guns, most of which were purchased in Britain and France, both of whom used hoops for their guns ${ }^{57}$.


K rupp gun cast for a K reiner B reech
The comment that K rupp borrowed the gun carriage design from Vavaseur may indeed have some merit. On the other hand, Vavaseur may very well have borrowed the idea from W ahrendorff! The idea of using gravity and mass to absorb recoil was hardly new. In those days, there was no international protection of intellectual property. In consequence, inventions often had several inventors, and it is extremely difficult to determine whose came first. For example, V avasseur is credited with inventing the copper driving bands for projectiles in 1874. However, K rupp was using them in $1872^{58}$ !


L ater K rupp guns. A bove: hooped design C/68 B el ow: mantel design of C/72
With regard to the alleged poor performance of K rupp guns during the Fran-co-Prussian W ar, A Ifred K rupp's letter to Engineering published on June 18, 1875, adequately addresses the question. "With regard to the 200 guns stated to be disabled in the...war, I would offer the following remarks...There were three systems of breech-loading used in the war... my system, which was confined entirely to the 4 -pounder guns supplied to Saxony, while all the other 4 -pounders were upon Kreiner's double-wedge system, and the 6 -pounders were constructed upon the Wahrendorff plan. The 24 -pounders had all the double Kreiner wedge. They all

[^23]were, however, with the exception of some other guns supplied by another firm, made of steel taken from my Works... not one of the guns from here burst... and also that not one of the guns fitted on my system of breech-loading was disabled... That a large number of guns on the K reiner and Wahrendorff system were disabled (not burst), is quite true..."59

A nother analysis provides some interesting details. Prior to 1868, sixteen guns failed. Seven of these were Prussian field guns with K reiner breeches. The other nine were larger guns, many of which had K reiner breeches. Of the nine guns after 1868, two were damaged by premature ammunition explosions, and the other seven from the effects of overstraining due to overly large propellant charges, which blew the breech ${ }^{60}$. Note that disabled guns can be rather easily repaired, as evidenced by the 1867 trial with 21 cm guns noted above. The twenty five mentioned here were damaged so severely that they were returned to the foundry, and hence were out of service.

The 'poor performance' of the K rupp gun in the first two competitive trials was the result of the government mandates, in these cases, the Ordnance Corps. The other two were more directly related to the technology. In the third, the volume of the chamber was insufficient to get full advantage of the slower burning Prismatic powder. Hence, the length of the chamber was increased by 0.1 caliber, at the expense of the rifled portion of the barrel, from 16,9 to 16,8 calibers, and the charge weight increased. The Table below gives a reconstruction of the gun in its condition for Trial 3 and Trial 4. Subsequent tests in 1869 demonstrated that the gun could take the stress of an even larger charge, so its service performance is included for comparison ${ }^{61}$.

Table 4. A rmstrong vs K rupp 9-inch Guns

| Gun | Shell, kg | Charge, <br> kg | Muzzle <br> velocity, $\mathrm{m} / \mathrm{sec}$ | Note |
| :---: | :---: | :---: | :---: | :--- |
| Armstrong | 116,10 | 22,70 | 438,90 | Elswick designed |
| 9-in M LR | 116,00 | 23,00 | 454,15 | A ustrian service |
|  | 113,50 | 19,50 | 426,40 | Danish service |
| Krupp | 139,00 | 23,00 | 450,00 | Dutch service |
| 9-in BLR | 132,50 | 20,00 | 410,00 | Test 3 w/ Gruson shell |
|  | 139,00 | 30,50 | 435,00 | Test 4 w/ steel A P |
|  |  | 455,00 | Shell |  |
| Service as C/68 |  |  |  |  |

There is no question that politics were involved. W hat must be determined are the degree and the effect of such political intervention. To a great degree, both A rmstrong and K rupp were in the same position; to continue to be viable and profitable, both needed a large portion of the business from their respective governments. A rmstrong reverted to rifled muzzle loaders when his government left him with little market for his breech loaders, though fortunately his ship building busi-

[^24]ness more than made up the difference. K rupp had no ship building business at that time, and therefore imperatively needed the ordnance business from both the Prussian A rmy and Navy, small though the Navy was at that time. ${ }^{62}$

M any of the officer corps of the Navy did not care who supplied their guns, but that they needed guns promptly. The technical questions mattered less than having something to fire! The Ordnance Corps wanted a domestic provider, and at least rationalized that if the government could not afford to build their own facilities, K rupp would have to do. Likewise, the relative failure of the K reiner breech, and the success of Krupp's own system, had discredited the Royal Arsenal at Spandau, so there was probably an element of chagrin in their support for K rupp. They al so brought some technical expertise to the question, and felt that M LRs had little or no room for development, and were actually obsolescent. Hence, they were inclined to give breech loading technology a chance to develop. A nd in the background was the King, Wilhelm I, who was a personal friend of A Ifred K rupp. The King may or may not have understood the technical matters involved, but he did believe that steel breech loaders were the best for the future. In the event, the coalition who supported K rupp, or at least did not oppose his technology, could do no more than to give him as much latitude as possible to prove the performance of his guns. In effect, the four competitive trials forced K rupp to advance his technology. So he probably was given two more chances to perform than might be the norm in other circumstances. A fter all, even an order from the King would not change the results of the trials, which were physical and technical, not political.

The trial result vindicated K rupp, and he became the major supplier of Prussian, and later German, ordnance. But not the type to rest on his laurels, he promptly set about improving the C/68.

The result, known as the C/72, and including the C/73 field guns, was the direct ancestor of modern K rupp ordnance. The construction of the gun was changed. Instead of rings/hoops shrunk onto the barrel, the barrel was thinned and covered with a thick steel mantel where the strength was needed, though rings were still used in heavier guns for local strength. The chamber was designed for the slower burning Prismatic powder. The projectiles were no longer covered with lead, but now featured copper driving bands, and were made of steel. A nd the wedge was altered. Note in the figure below that it now featured two parts that lined up with the bore; the normal Broadwell Ring, and now also a tube through which the shell and charge can pass. The original design required that the wedge be moved far enough to expose the bore, and then moved back into position. The new model did not need to be withdrawn as far to allow loading. This simplified and accelerated the loading process, and allowed a higher rate of fire. A nd last, but not least, the barrels were longer! The slow burning Prismatic powder allowed the barrels to be lengthened, which increased propellant efficiency and produced higher muzzle velocities.

A nd finally, the old adage is that "Imitation is the sincerest form of flattery." "As late as 1880 a proposal was made to convert the [Armstrong] RBL 40 pr ( $4.75-\mathrm{in}$ ) and 7 -inch into 'side-closing' guns by rotating the piece 90 -deg within

[^25]the trunnion ring, thus making the vent piece a horizontal sliding block. As well as making handling more convenient the conversion saved much labour, as the vent piece no longer had to be completely removed for loading. Experimental guns were prepared, other systems of obturation tried, as well as projectiles with copper driving bands. The modified guns were said to have 'answered extremely well' but the expense involved, especially for new ammunition, ruled out further action." ${ }^{63}$


The K rupp 9-inch $(23,54 \mathrm{~cm})$ gun on a swivel carriage. (A ppleton's Cyclopedia of A pplied M echanics, 1880)

Every success story has a beginning, a point of origin. For Alfred K rupp, there were three essential factors, all of which contributed greatly and were indispensable. First, he developed high quality [by the standards of the time] steel suitable for gun making.

Second was the pioneering work of General of Artillery Giovanni Cavalli and B aron M artin von W ahrendorff. One could argue that W ahrendorff's contribution was greater, as his success enabled K rupp to begin breaking into the Prussian ordnance market, and there is some merit to that circumstance. However, exclusive of Prussian interest, both of those ingenious men focused attention on breech loading, and provided viable systems to prove breech loading was possible and practical.

[^26]


A n early Prussian lead coated shot, typical form of the Gruson Chilled Shot. (Holley, A Treatise on Naval Gunnery)


K rupp $30.5 \mathrm{~cm} / \mathrm{C} 80$
And third, K rupp realized that by combining the best features from both the Cavalli and Wahrendorff guns, a much more effective system could be developed. M odern K rupp artillery is the combination of K rupp steel, the Cavalli wedge, and the W ahrendorff cylinder. . And the rest, as they say, is history.

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## HITTING THE TARGET. NAVAL FIRE CONTROL 1860TO 1900

It is a common misconception that modern $N$ aval Fire Control and gunnery was a XX century development, solely beholding to Sir Percy Scott and William Sims and the 'Gunnery RevoIution' they launched, and that the 'art' of gunnery had changed little since the B attle of Trafalgar in 1805. Thus, the pioneering work of Bradley A. Fiske, A.P. D avydov and Sir George Elliot, amongst others, is discounted and ignored. This article seeks to look at the progress of the last 30 years of the XIX century to place the 'Gunnery Revolution' in its proper context.


#### Abstract

Существует распространенное заблуждение, что современные системы управления артиллерийским огнем появились лишь в XX веке и представляли собой развитие идей "Артиллерийской революции" сэра Перси Скотта и Уильяма Симса, а более раннее искусство стрельбы оставалось практически неизменным со времен Трафальгара в 1805 г. В результате вклад таких пионерских работ как работы Бредли Фиске, А.П. Давыдова и сэра Джорджа Элликота полностью игнорируется. Предлагаемая работа - попытка рассмотреть прогресс последних тридцати лет XIX века и рассмотрение "Артиллерийской революции" в контексте этих событий.


It is a common misconception, even among Naval Historians, that until Percy Scott and William Sims began the so-called Gunnery Revolution in the Royal and U.S Navies at the beginning of the twentieth century, the "art" of gunnery had changed little since the time of Trafalgar. This view overlooks the fact that Scott did not invent the Director, but resurrected the device and applied modern technology to the pre-existing concept and equipments ${ }^{\mathbf{1}}$ It also pre-supposes that such problems as deflection and roll were beyond comprehension, and completely discounts the scientific work of Bradley A. Fiske and A.P. Davydov, two of the prolific inventors of the age.

Nothing could be further from the truth. Hans Busk, writing in 1859, describes the gunnery problem as follows:
"... in firing at a moving object as at a steamer passing, we will suppose at twelve knots per hour, allowance must be made for her speed, and a point must be aimed at a-head of her, to be determined by her distance and rate of motion. But this is not all: an 8-inch shell takes two seconds to travel 450 yards, to that the gunner having in the first place made the closest approximate estimate of the distance of the vessel to be struck, has to calculate her rate and then to fix upon an imaginary point in her line of course at which she and the shell may arrive simultaneously, taking heed, moreover, if there be much sea on, to fire when the deck of his own vessel is horizontal, or at any rate with a falling in preference to a rising side" ${ }^{2}$

Indeed, "The first recorded system... is probably Philip Broke's 1807-13 method of laying the broadside guns to an ordered elevation... and... angle of training so that their fire could be directed on a target which the individual gun captains could not see." A Captain W. M oorsom, RN, had introduced a "director" in the early 1850 s to address the issues noted above. Located in a convenient position and manned by an officer, the target bearing, heel, and range were determined, and the guns laid accordingly. The officer gave the order to fire when the target came into
his sights. ${ }^{3}$ The entire process was verbal. One can imagine the designated officer asking the master Gunner for the range, estimated by eye and perhaps with the benefit of experience, then performing some quick calculations, after which instructions were shouted to the Lieutenants in charge of the batteries for the laying of the guns. A fter an appreciable interval, the shouted order to fire is given, and within seconds, each battery discharges. So far, so good, but can the process be repeated in the din of readying the guns for subsequent rounds? One suspects that, given the communications technology of the period, effectiveness of the system was limited to the first salvo/broadside only.

Poor communications was, however, only part of the problem. The guns themselves tended to be quite heavy and bulky. In broadside mounts, this mattered little as their traverse was limited, though this required the ship to maneuver to line up the guns with their target. For fire at other angles, pivot guns were common. Their carriages were mounted on a system of tracks or races, which enabled them to be moved from one side of the ship to the other, or cover the angles in between. But even in 1877, "... the crews of both [of Shah's] 9" guns had trouble moving their massive weapons from one broadside to the other over the races." ${ }^{4}$

M ounting guns in turrets or on turntables en barbette was less of a solution than commonly thought at the time. The early turrets were traversed by hand. In the case of the Huascar, for example, "it took sixteen men fifteen minutes to turn it through 360 degrees. ${ }^{15}$ Later, and larger, turrets and turntables were steam powered, though Inflexible's were powered by Rendel's hydraulic system, which had been experimentally used in the Thunderer, which allowed "a complete rotation ... in just over a minute." ${ }^{6}$

But the problem was one of tracking the target. Obviously, the hand operated turrets were much too slow, while the steam and hydraulic powered turrets and turntables lacked the necessary control, especially given their fixed loading position requirements. Like communications, the available technology was not sufficient for the task.

At any kind of range, gunnery was exceedingly bad, and the existing fire control system, such as it was, proved inadequate. In 1870, the ironclads Monarch, Captain, and Hercules took part in gunnery experiments off Vigo. Each ship was to fire for five minutes at a rock 600 feet long and 60 feet high, "or twice as long and four times as high as a ship." A t a range of about 1,000 yards, "Hercules fired seventeen shot, of which ten hit; Captain fired eleven shot, and made four hits; Monarch fired twelve shot, and made nine hits." But according to Captain Philip Colomb, had the rock been moving, none of the shots would have hit! ${ }^{7}$

New technologies, however, promised at least partial solutions. In the British Royal Navy, the implementation of electric ignition of the firing charge, around 1868 or so, provided a tactic that would enhance effectiveness. It required that the guns be laid on a pre-determined angle, and then the ship would maneuver to bring the guns in line. At that point, the firing circuit would be closed. Oscar Parkes described this gunnery tactic as used in conjunction with ramming:
"It was intended to withdraw the [gun crews] from these [broadside 9"] guns to the armoured forecastle [in Shannon] after they had been laid, and then fire them by electricity when passing the enemy if an attempt to ram failed.
"A s in the Shannon salvo firing was to be the special form of attack, the guns being loaded and laid under cover of the end bulkheads [of Northampton] and fired electrically without the crews being exposed in a close engagement. The broadside having been discharged, she was then to turn bows on, reload, and again maneuver for another broadside." ${ }^{8}$

It should be noted that Shannon was completed in 1877, and Northampton in 1878. There also may be some question as to how important ramming was as a viable tactic. M onarch's 12" 25 -Ton guns were sighted to 7,000 yards, through she had been completed in 1869. Alexandra, completed in 1877, had her 11" 25 -Ton guns sighted to 10,000 yards. ${ }^{9}$ At sea, this was at best wishful thinking, though it implies that gunnery action at ranges greater than 1,000 yards was considered reasonable. Indeed, in M ay, 1877, Shah's action with the monitor H uascar provides an example of the Royal Navy's capabilities, and A ndrew Smith's account deserves to be quoted at length:
"Shah's port guns opened fire at 1,900 yards... DeHorsey chose to use the Shah's speed to fight at long range, mainly 1,500 to 2,000 yards, although ranges (estimated by eye) varied from 300 to 3,000 yards. The Amethyst... kept at 1,500 to 2,500 yards, although A ble Seaman Patrick Riley records a minimum range of 1,000 yards in his memoirs... Fire control was extremely primitive. Ranges were estimated by officer's eye, shouted at the gunners through the noise of battle, sights set accordingly, and guns mostly laid and fired individually. However, the Shah also fired several broadsides from her 7" guns, including three by electric firing, mostly aimed by the director sight at H uascar's turret... The action had lasted about 2 hours 40 minutes. The Shah fired 32 rounds 9" (2 common shell, 11 Palliser shell, 19 Palliser shot), 149 rounds 7" (4 common shell, 145 Palliser shot), and 56 rounds 64 -pounder shell, total 237 rounds. The Amethyst fired 190 rounds 64pounder shell. Total... 427 rounds... We may safely conclude that the H uascar received at least 50 hits." ${ }^{10}$

From the above account, several points of some importance bear emphasis. There was a 'director sight' that could and was used for aiming at a specific target, the guns could be fired electrically when under 'director control', but information/instructions were still passed verbally. But the overall gunnery performance of the two British ships was rather good, considering the constantly changing range and bearing at which they were firing, the sea state, and that the monitor did not present much of a target above water; a minimum of $11.7 \%$ hits, though some sources claim sixty to seventy hits for 14.05 to $16.39 \%$.

In the mid 1870s, Admiral Sir George Elliot took advantage of another advance in technology to re-work the director system, which was subsequently fitted to most of the large warships in the Royal Navy. The 'director' was moved to the 'conning tower', or to a purpose-built 'Director tower' if no conning tower had been fitted, which was fitted with the new voice pipes to the various gun positions, as well as the existing electric firing circuits. ${ }^{11}$ The intent was obviously to solve
the communications problems, as well as further centralize gunnery control. But the test of combat brought mixed reviews.

An excerpt from the report of Captain H. Fairfax of the turret ironclad Monarch illustrates the chronic problems of fire control. Monarch was one of the ships participating in the bombardment of A lexandria, Egypt, in 1882:
"The sighting arrangements and methods of Iaying the guns for elevation are in this ship particularly bad. A fter the Captain of the turret has ascertained and communicated the heel to the number laying the gun the time necessary to work the elevating gear, lay the guns by means of the crude wooden scales, and make ready is so great that probably another gun or turret will have fired in the interim, and consequently the heel of the ship be so affected that a re-lay of the gun is necessary unless a bad or chance shot is purposely delivered... [the Elliot director gear] proved so untrustworthy that the turrets were fired independently. The voice pipes to the turrets proved useless in the din of action, and orders had to be passed verbally by specially stationed officers." ${ }^{12}$

Captain J ohn Fisher of the Inflexible, and A.K. W ilson, filed reports to the effect that the voice pipes were not an effective means of communications with the various guns, that the 'conning towers' restricted the vision of the gunnery officer considerably, and that some effective method of finding the correct range was needed. The Captain of Superb "... had noted that he had a clearer view of the action [from his conning tow er] than the individual gun captains stationed at each firing gun... [and]... suggested that an electric telegraph should be installed between the tower and the guns so that the bearing and elevation could be passed down... Other captains of ships not fitted with conning tow ers suggested that a similar connection should be made between the fighting tops and the guns... ${ }^{13}$

But only a few weeks later, on 18 August, the Elliot director gave sterling service during the landings at Port Said. Orion and Carysfort, in a slow bombardment of an Egyptian A rmy camp, fired effectively at a range of about 4,200 yards. A dmiral Hoskins, who commanded that area of operations, prai sed the action in his official dispatch: "I draw particular attention to the effective fire maintained by the Orion and Carysfort on a position which could only be seen from the masthead of the latter vessel at over 4,000 yards -- a fire by which a train standing on the rails at Nefiche station was twice hit and the carriages and trucks secured for our own use." ${ }^{14}$ In our modern parlance, the range and bearing were estimated from the masthead 'crows nest', and the information passed to the gunnery officer in the 'conning tower.' The correct bearing and the range was passed to the guns, which were then laid accordingly. The guns were then fired electrically, and corrections made upon spotting reports from the crows nest. In these circumstances, effective fire could have been accomplished at ranges of 7,000 or 10,000 yards, so long as direct observation of the fall of shot was practical.

In 1885, a Lt. R.H. Peirse took up the task of improving the 'director', and reportedly greatly improved the device and concept. A further set of modifications was made in the early 1890s, but within a few years the Director was overtaken by technology. The advent of a secondary battery of Quick Firing mounted in casemates on each broadside proved to be a complication, due to the different ballistics,
and so they were fired independently. ${ }^{15}$ AII-round loading of the heavy guns greatly increased their rate of fire, comparatively. A nd the new Barr \& Stroud rangefinders more than doubled the effective combat range. As the old style slow firing MLRs and BLRs fell out of use, so too did the Director system that enhanced their performance.

In the late 1870 s, about the same time that the RN was working with the Elliot Director, the Russian Navy deployed a fire control system of great interest. Designed by A. P. Davydov and accepted in 1876, it laid the guns at predetermined angles ahead or abaft the beam, and directly abeam. The choice of which line to use was made by the gunnery officer, who would anticipate what the relative positions of his own and the target ships would be. Once the guns had been laid, the gunnery officer had but to wait for own ship's motion to bring his sight on, at which point he could fire the guns electrically. ${ }^{16}$ This imminently practical system was probably deployed on the ironclad turret ship Petr Veliki and the armored cruisers of the General Admiral class, and subsequent ships, until replaced by the much superior Geisler system of 1894. ${ }^{17}$

The French Navy seems to have lagged well behind the British and Russian Navies. On 23 June 1884, the armored cruiser La Galissioniere, anchored at Chefoo, China, fired at targets up to 4,000 meters range, in an effort of over-awe Li Hung-chang. ${ }^{18}$ W hile this sounds impressive, it only required a rudimentary range table and a skilled gunner, even using the open sights of the time, to fire from an anchored ship at a stationary target clearly visible. Carysfort's feat two years before required a fire control system, crude by modern standards, to hit a target not even visible from the guns or the bridge, even though the range was similar. Theodore Ropp confirms, in his Development of a M odern Navy, that the French only became interest in fire control in 1891, on which more later.

On M arch 3, 1883, the bill that created the "N ew" U.S. Navy was signed into Iaw by President A rthur. This was a momentous event in the history of fire control because it unleashed the genius of Bradley A. Fiske upon the field of naval technology. So at this point, it seems germain to examine some of his inventions, as much as they influenced future developments as for their application within the context of this paper.

In 1883, Fiske designed electric primers to fire heavy guns, and suggested that the Plans for the Chicago be altered to include dynamo rooms to provide plenty of electric power. In December 1885, he suggested that heavy guns should be trained, elevated, and fired by electric motors, under the control of a single gun captain, and prepared a sketch of the necessary wiring. Two years later, he wrote a paper "detailing his plans for 'pointing and firing guns with automatic mechanisms."' This also detailed a device for automatically firing the guns at the proper point in the roll cycle of the ship. He proposed using a spirit level set at the same height as the guns, on the horizontal plane. When the bubble in the level was at the proper angle due to the roll, the liquid would drain away, which would break the electric circuit and fire the guns. ${ }^{19}$

One of the most significant of Fiske's inventions was a workable range-finder. Unlike the optical instruments with which we are familiar, this was a two-station two
observer device based on trigonometry, the principle being "to find the sum of two angles included between two observers and lines drawn from those two observers to the target." The two stations, one fore and the other aft, each equipped with a telescopic sight, formed the base of the triangle, a known distance from each other. Each observer would focus his sight at the same location of the target ship, such as the foremast. A wire was attached to each telescope. As the telescopes were moved onto the target, the wires moved. The distance these wires moved was proportionate to the range to the target, and a galvanometer dial, using the same principles as on the Wheatstone Bridge, then pointed an arrow along a scale calibrated in yards to indicate the range to the target. A nd the two stations were connected to the conning tower by electric telephones, the first such devices ever used at sea. ${ }^{20}$

W ithout a reliable range-finder, "firing at ranges greater than three thousand yards was considered useless because the errors of sighting were so great that ammunition would be wasted. In fact, in 1890 two thousand yards was considered to be about the limit of accurate range." The Navy was impressed with the device: "It is the opinion of the board that the experiments [with the range-finder] show that the instruments are in good order and the pointing accurate, that they will give reliable results within $3 \%$ in ranges less than 5,000 yards, or at greater ranges when adjusted skillfully." Two sets were to be placed aboard ship, one for each side. ${ }^{21}$

Several of the new warships for the U.S. Navy were fitted with the electric range-finder, as well as several other of his inventions, such as an electric range transmitter, electric range indicators, and telescopic sights. These included the battleships M aine, Texas, Indiana, and M assachusetts, as well as the cruisers Baltimore, San Francisco, Cincinnati and Minneapolis. ${ }^{22^{2}}$

In October 1890, Fiske began a year long trip to Europe to market his rangefinder. He was warmly received in Paris, and invited by the $M$ inister of $M$ arine to have his device installed aboard the ironclad battleship F ormidable at Toulon. The test was successful, and the French Navy accepted the instrument aboard F ormidable, and another for the coast defence battery at Cap Brun. It is unknown how widespread the use of the range-finder was in the French Navy, but there is no doubt that they had been very favorably impressed. It was also installed in the ChiIean battleship Capitan Prat, then building at La Seyne. ${ }^{23}$

But the two-observer range-finder came to a bad end. The A merican A siatic Squadron contained only one ship equipped with the device, the cruiser Baltimore. At M anila B ay, "... the ... electrical range finder ... failed after the first round was fired and because the topmasts of the Spanish ships were housed, it was very difficult to obtain masthead heights with either a sextant or stadimeter. Firing ranges therefore were set at the distance to the beach, with corrections made by spotting." Those units aboard the ships at Santiago fared no better. ${ }^{24}$ No matter how technically accurate the Fiske instruments were, and even after the U.S.N. accepted optical range-finders he expectantly awaited the $N$ avy changing its mind, they were too fragile for the rigors of combat. One is reminded of the Henderson Gyro and the Abferungs $G$ erat at Jutland in a later war, and cannot help but think that development was abandoned prematurely.


But the failure of Fiske's electrical two-observer system cleared the way for the major competitor, B arr \& Stroud. This Scottish firm was manufacturing optical single observer instruments that used the coincidence principle, to wit, prisms show the observer a split image, and adjusting screw to align each image into a single complete image by moving one prism. This was mounted on a calibrated scale, which translated the distance the prism moved into the range to the target. ${ }^{25}$

A fter trials and tests, the British A dmiralty ordered five models at the end of 1892, the first of which was mounted aboard the cruiser Blenheim on July 22, 1893. From then on, the Admiralty presented the firm with an increasing number of orders as the instruments were mounted on the ships of the Royal Navy. But foreign orders also made up a large portion of the company's business. Through their connection with A rmstrongs, the J apanese cruiser Yoshino received the eighth production model [which no doubt explains in part how the IJN's "Flying Squadron", of which she was the flagship, could so speedily overwhelm the Chinese cruisers Ch'ao Yung and Yang Wei at a range of 3,000 yards during the Battle of the Y alu the next year], while the Chilean Blanco Encalada and the A rgentine Buenos Aires received Iater production. In addition, the navies of Germany, Sweden, the Ottoman Empire, Italy, and Brazil all purchased instruments for trials. ${ }^{26}$

Perhaps B radley Fiske's most enduring contribution to the field of fire control was his invention of the telescopic sight., patented on September 5, 1893. Perfection of the instrument, however, was not accomplished without incident. In its first test, aboard the gunboat Yorktown during a voyage from Chile north in early 1892, the telescope had been attached to the gun! It promptly gave the ship's Executive Officer a black eye when the gun recoiled. But on September 22, when Yorktown held her required semi-annual target practice, the sight was given a second trial. "During the morning, eighteen shots were fired, using the regular open sights, with the customary dismal results." But in the afternoon, using the telescopic sight now attached to the gun shield, "... four shots hit the target, wrecking it... Several days later, a shot fired successfully at a moving target confirmed... " the importance of his invention. ${ }^{27}$

The above occurred a full five years before Percy Scott attached a telescope to one of the $4.7^{\prime \prime}$ guns aboard HMS Scylla. It should also be noted that Fiske's sight included fine cross-hairs, whilst Scott's initially did not. In M arch of 1897, the Secretary of the Navy directed that telescopic sights should be fitted to all of the 4-, 5-, and 6 -inch guns in the fleet, and the new M k. 5 mounting for 5 " guns to be installed in the new armored cruiser Brooklyn were so equipped from the outset. ${ }^{28}$

K arl Lautenschlager, in his article "A M ajestic Revolution", considers the telescopic sight to have been not merely important, but a revolutionary piece of technology, and his comments deserve to be quoted at length:
"U sing an open sight, the gunner had to line up a rear sight, front sight and the target. Since the human eye cannot focus on objects at different distances at one time, a compromise had to be made by focusing more or less on the front sight and attempting to keep target and rear sight in line. This meant that a target the size of a ship had to be inside 2000 yds . if it was to be hit consistently... The change from open sights to telescopic fire control gave pre-dreadnought battleships the capabili-
ty to shoot accurately out to about 7000 yards. The telescope's optics... and fine cross hairs, allowed accurate aiming and thus consistent hitting out to $7000 \mathrm{yds}$. . ${ }^{129}$

It is, perhaps, unfortunate that Mr. Lautenschlager over-looked the beneficial effects of range-finders to the increase in effective gun range. Still, his intent is valid; the telescopic sight was a milestone in the development of fire control.

Impossible as it may seem, the French Navy seems to have been absolutely quiescent in the fire control field. They had spent the thirty years since 1860 dealing with the technical issues involved with naval artillery and propellants, which resulted, with the nitrocellulose propellant for the long M .1887 guns, in first class artillery. But ranging was still accomplished using either sextants or Lugeol's Stadimeter, which dated to the late 1850s. It was a split image device with an attached Table for converting angles into ranges. In 1892 L V Fleuriai presented a much improved Statimeter, and C F Guyon provided a calculating circle for quick conversion to ranges That they did not adopt the Fiske rangefinder may be due to the 'not invented here' syndrome, which led to various proposals from French firms failing trials through the remainder of the decade.

However, the nature of warship armament had changed. A.P. Davydov foresaw this in 1881 and had designed a gun mount with greater training and possibly 'follow the pointer' gear for control. In 1884 V avasseur developed the first C entral Pivot type mounting, which greatly increased lateral training speed. A nd the development of Quick Firing guns created an inseparable divide between the heavy slow firing main guns and the secondary battery. Fiske foresaw this n 1893 and had changed his emphasis from Central/Director Control to the individual guns. The final Director in the British Royal Navy, installed in the Royal Soveriegn class, was intended only for the heavy main guns. A nd within a few years, 'all around' loading, introduced after the first two units of the Majestic class, so increased their rate of fire that the Director was no longer considered necessary or advantageous. The primary consideration became the best means of communicating target bearing, target range, deflection and firing orders to the guns... ${ }^{30}$

The system that developed in the French Navy over the next several years called for the observer [spotting officer] in the masthead obtaining a range and communicating it to the gunnery control center. The gunnery staff then estimated the target speed, calculated the deflection, and passed this information to the guns by the new Range and Order devices. The medium caliber guns then fired several broadsides, the first to a range less than that reported, and each subsequent one to a greater range until the target was hit or straddled. [Basically, this was a ladder-type system] O nce the range had been established, the main guns would open fire.

This method was tested in 1897 by the battleships Brennus, Neptune, and Marceau, but the results were mixed. The 'short-shot' method was considered too slow in finding the target. But once the range had been found, the results were favorable. The battleships scored $26 \%$ hits at ranges of 3,000 to 4,000 meters.

In 1898 the M inistry of M arine issued instructions for fire control methodology. The 'Iadder' system was discarded in favor of requiring the medium caliber guns to use the displayed range. The range figure was to be corrected by spotting.

Interestingly, salvo firing was not used, opinion being that as long as the guns were using the same range figure, their gunnery would be effective. ${ }^{31}$

But the Imperial Russian Navy may very well have been ahead of all other navies in the mid-1890s. Their Geisler 1894 system involved electronic indicators to not only transmit range data from the observer positions on the masts to the gunnery center, but also the sight settings, for both deflection and elevation, from the gunnery center to the gun positions. As soon as the guns had been laid, the gunnery officer could fire them electrically at the proper moment in the roll cycle. Since elevation and deflection were calculated values from the gunnery officer, the guns only needed to be kept on target by continuous aim in train. There were only two short-comings; the lack of a reliable and accurate range-finder, and the time lost to the manual processing of the elevation and deflection. The time and accuracy gained with the Geisler electronic indicators was to a considerable degree lost to the manual work involved. That being said, the Russians had the best system available before the 'gunnery revolution. ${ }^{32}$

Dr. Ropp made an interesting statement which deserves some attention. He stated that "in 1902 the state of gunnery in all the major navies was about the same [as the French Navy], except in the Italian, which used the British system of individual fire [but] without the sea-training of the gunners. The Russians and the Germans (the only navy on whose methods of fire the French had no information whatever and which may have discovered the principles of fire control independently) were using the French system. ${ }^{33}$ With regard to the two Imperial navies, one wonders to what he was referring, given that the Franco-Russian Entente was ten years old at that time, and the degree of technical exchange between the two was considerable, and that French yards were even building ships for the Russian Navy. A nd the Geisler 1894 system was well in advance of the French 'system' of 1898. However, one of the hallmarks of German gunnery in a later period was the use of the ladder system for rapid target acquisition. So with "reverse engineering" type reasoning, it would appear that the Germans picked up the latter from the French, and then refined it to tactical usefulness.

The young Imperial German Navy (Kaiserliche Marine) did, in part, advance well ahead of the major navies, this being in long range gunnery. Between October $11^{\text {th }}$ and $15^{\text {th }}, 1885$, the ironclad battleship Bayern fired at a target off the Courland coast, at ranges from 1500 to 5000 meters, scoring 33 hits out of 133 shots, an impressive $24.8 \%$. At a time when their normal practice firing range was only 2,500 meters, Bayern's long range shooting was sufficiently accurate to impress the naval leadership. As a result, it was decided to prepare range tables for every gun, so they could be fired to maximum range. A t this time, however, maximum ranges for the heavy guns were between 7,400 and 10,000 meters. ${ }^{33}$

But there is a considerable difference between firing at long range, and being able to control the fire in order to obtain hits. In 1890, A dmiral Thomsen, of the ordnance department, clarified the situation by pointing out that deflection would be a considerable problem at long range, and that target movement could be observed and measured with modern equipment. This led to two developments; the first of which, in 1892, was to commission Dr. August Raps to work with the firm
of Siemens-Halske to develop fire control equipment. Initially, this project was for the benefit of the Coast Defense artillery, but after the turn of the century, the Fleet began receiving the equipments. The second development was the issue of firing training regulations in 1893, using the new fire control known Gabelverfahren system, which allowed observation of changes in target movement in both range and bearing when compared to a scale. Once the target range had been determined, its movements could be tracked, and adjustments made for gun range and deflection, which could be communicated to the guns using the 'direct current 3-roller system,' one of the first range and order equipments. It is very possible that the Germans were the first to actively pursue accurate fire at long range. ${ }^{34}$

## Conclusions

## A. The test of combat

Unfortunately, there were few ship-to-ship actions in the period covered, that demonstrated fire control to any great extent. Discounting the Battle of Lissa, the field is limited to the Shah and the Huascar in 1877, the Sino-French W ar of 18845, the Sino-J apanese W ar of 1894-5, and the Spanish-A merican W ar of 1898. Of these, the first has been covered above, and the second offers little. The French squadron made short work of the vastly inferior Chinese ships, mostly in enclosed and calm waters of harbor and river.

The Battle of the Yalu, however, provides some points of interest, one of which has been cited above, to wit, the Barr \& Stoud range-finder aboard Yoshino encouraged effective fire at 3,000 yards. In addition, at ranges of 2,000 to 3,000 yards, the Chinese battleships were hit a hundred times, though the number of rounds fired is unknown. In the realm of the heavy guns, both Itsukushima and $M$ atsushima were hit by two 30.5 cm shells from the Chinese ironclads, but these may be attributable to the large number of European and A merican officers serving aboard. On the other hand, the J apanese fired only thirteen 32 cm rounds from their big guns, and obtained no hits for their efforts. Both the Chinese and Japanese heavy guns were mounted on turn-tables, so part of the different success rate may be attributable to the basic engineering; K rupp and A rmstrongs for the Chinese, and Canet for the J apanese. It is interesting, and perhaps indicative, that the Chinese ironclads opened fire at 6,000 yards, though they could hardly have been effective. ${ }^{34}$ They fired a total of 197 rounds from the 30.5 cm guns, and obtained a total of five hits $(2.54 \%)$, and 484 rounds from the guns from 30.5 cm down to 4.7inch, making 48 hits ( $9.92 \%$ ), though many of these had been on the old ironclads Hiei and Akagi, at ranges of only a few hundred yards. ${ }^{35}$

The Spanish-A merican War was the acid test for the "New Navy", the ships of which carried many of Fiske's inventions. W hile the failure of Fiske's range-finder has been noted above, as have the subsequent ranging problems, the gunnery statistics are illustrative. The A merican squadron fired 1578 -inch, 6356 -inch, and 6225 -inch shells, for a total of 77 hits $(5.45 \%)$, of which the largest portion belonged to the 8 inch guns. B ut it should be remembered that the targets were at anchor, and the range relatively short, so this performance was considered abysmal.

Of the ships that participated in the B attle of Santiago, the ones equipped with the Fiske range-finder, which should have given them a considerable advantage, also suffered the failure of the instrument. Fortunately, many of the ships in the fleet were al so equipped with Fiske's telescopic sight. But since the battle was in the nature of a stern chase at speed, the gunnery conditions were far from ideal anyway. A gain, the gunnery statistics paint an interesting picture. Of the forty seven 13 -inch shells fired by the Indiana class battleships, none hit. Iowa managed to get two hits from the 3912 -inch shells she fired ( $5.13 \%$ ). But taking the heavy gun performance as a whole, the hit percentage is only $2.33 \%$. Given the reasonably short ranges, the obvious conclusion is that the technology to track a target with those heavy turrets did not yet exist. Of the medium caliber guns, the USN fired 1,208 shells for 40 known hits ( $3.31 \%$ ). Though many hits could not be documented, making the actual percentage higher, the gunnery performance was still considered abysmal. ${ }^{36}$

## B. Effectiveness

So what does all of this mean? I believe the data supports several conclusions:

1) B ased on the performance of the ironclads off Vigo in 1870, 1,000 yards was too great a range for un-assisted fire, which explains why Hans Brusk considered 450 yards an example of long range in 1859. It seems safe to say that effective fire at 1,000 yards was unlikely.
2) B ased on Shah's performance, 'director' firing at targets Iarger than Huascar could be effective at a range of 3,000 yards. This would include the Russian Davydov system, and most probably the Elliot Director, mostly due to the lack of effective communications.
3) With big guns and no more technical assistance than a sextant-type rangefinder, effective gunnery was probably limited to 2,000 yards [meters], as maintained by Bradley Fiske, and detailed by K arl L autenschlager.
4) B ased on the U.S. Navy's appreciation of the Fiske range-finder, it seems reasonable to conclude that a viable range-finder could extend effective firing out to 5,000 yards. Add telescopic sights, and effective range could be extended to 7,000 yards. This presumes other technical support, such as electronic range indicators, and a central control to cal culate deflection.
5) B ased on the U.S. Navy's performance in the Spanish A merican W ar, viable range with only telescopic sights was probably not greater than 4,000 yards, and more likely 3,000 .
6) With a range-finder alone, based on the J apanese performance at the $Y$ alu, effective firing was limited to around 3,000 yards, with open sights.
7) A nd finally, with a viable technique, in spite of open sights and the lack of an effective range-finder, 3,000 meters could be a practical combat range, based on the French trials.

B ut the bottom line conclusion, how ever, is that the fire control developments were effective, and definitely increased the combat range of those navies that applied the technology.

## Notes

${ }^{\mathbf{1}}$ John Brooks, "Percy Scott and the Director," Warship 1996 (London: Conway M aritime Press, 1996), p. 150 \& 155. A nd Peter Padfield, Aim Straight: A Biography of Sir Percy Scott, the father of modern naval gunnery (London: Hodder and Stoughton Limited, 1966), pp. 189190. This is confirmed also by the "... stealing a master sight and other fittings from [old] ships in reserve... " on which more below.
${ }^{2}$ Hans Busk, The Navies of the W orld (London: Rutledge, Warnes, and Rutledge, 1859), p. 239.
${ }^{3}$ Brooks, op.cit., p. 155.
${ }^{4}$ Jack Greene and A lessandro M assignani, Ironclads at W ar (Philadelphia: Combined Publishing, 1998), p. 288.
${ }^{5}$ Ibid., pp.289-290.
${ }^{6}$ Oscar parkes, British Battleships (London: Seeley Service \& Co. Ltd., 1957), p. 254.
${ }^{7}$ Sir Thomas Brassey, The British Navy: Its Strength, Resources, and Administration, 5 V ols. (London: L ongman, Green, and Co., 1882), V ol. III, p. 418.
${ }^{8}$ Parkes, op.cit., pp. 236 \& 241.
${ }^{9}$ Ibid., pp. 132 \& 219.
${ }^{10} \mathrm{G}$ reene and M assignani, op.cit., pp. 287-291.
${ }^{11}$ Captain H. Garbett, R.N., Naval Gunnery ((London: George Bell and Sons, 1897), pp. 209-211. Gunnery in this period operated generally in one of two modes: independent firing or Director controlled sal vo firing. Of the two, independent fire was the more common.

Shooting still involved open sights mounted on the gun, though they had become rather sophisticated, allowing adjustments for both shell "drift" and target speed across [deflection]. Elevation was accomplished most likely using a scale graduated in 100 yard increments. Firing the guns was done electronically on the roll when the sight came on the target, and ranges were provided by the Gunnery Officer via voice pipe.

The Elliot Director system was built around a telescope fitted with cross hairs. This telescopic sight, one for each side of the conning tower, was fitted in a vertical frame, which was pivoted on a graduated arc matching the arcs provided for each gun. This frame moved over racers in the same manner as the guns, and allowed the tel escope to be elevated or depressed as necessary. It was also the mount for the electronic firing key, and several scales with verniers to display the ranges and corrections. M ounted on the bulkhead of the conning tower, in easy view, were various Tables that included, but not limited to, Range Tables for the guns, the 'speed across [deflection] based on target speed, the 'dip' correction for range, and the elevation/roll effect caused by the 'dip' correction.

The general procedure would be:

1) The Gunnery Officer decides the bearing in train to lay the guns, which was then passed to the guns via voice tube;
2) The range for firing was selected and passed to the guns;
3) The speed across correction is made and the sight set slightly in advance of the gun bearing;
4) The 'dip' correction - an allowance for the greater height of the Director above the guns, larger for close range or smaller for longer ranges - is identified from the appropriate Table and the tel escope is depressed from the horizontal accordingly, and then locked in place;
5) When the telescopic sight moved onto the target, the Gunnery Officer depressed the firing key which fired the guns electrically.

If the target should be at a slightly different range than anticipated, the system was sufficiently flexible to quickly compensate. By changing the scale and 'dip correction' for the correct range, and setting the 'dip correction' to the telescopic sight for the correct range, the sight would be on target at a slightly different point in the roll. The effect would be allowing the roll to alter the el evation from the horizontal of the guns at the time of firing, lower for a closer range or higher for a greater range.

The tactic previously described for Shannon and Northampton, as examples, was a variation of this broadside mode of Director firing, though the guns would be laid for the short range expected during a melee in connection with ramming, as occurred at the B attle of Lissa in 1866.

However, the main purpose of the Director, and no doubt the most common usage by the heavy ironclads, was to deliver converging fire on the target. To accomplish this, converging stops were fitted to the races of the guns so that each gun was aimed at the same point at a range of 600 yards. The stops were set up for three specific lines of bearing - bow, beam or quarter. The procedure was much the same, though instead of being given a specific bearing, the gun captains were told to prepare for "converged firing by director" and which of the three set lines was to be used.
[Special thanks to Dr. J ohn Brooks for his valuable assistance]
${ }^{12}$ Peter Padfield, Aim Straight, A Biography of Sir Percy Scott, (London: Hodder and Stoughton Limited, 1966), p. 55.
${ }^{13} \mathrm{I}$ bid. A nd Greene and M assignani, op.cit., p. 376.
${ }^{14}$ Lord Charles Beresford, Charlie B. A Biography of Admiral Lord Beresford of M etemmeh and Curraghmore (Boston: Little, B rown, \& Company, 1914), V ol. I, p. 182. A nd M arjorie E. M oore, Adventures in the Royal Navy: The Life and Letters of Admiral Sir Arthur William M oore (Liverpool: C. Tinling \& Co. Ltd., 1964), pp. 48 \& 49. And Lt. Colonel W. H. Green, "Tel-El-K abir, 1882," A rmy Quarterly and Defence Journal, V ol. 88, No. 2, 1964, p. 222.
${ }^{15}$ Garbett, op.cit., pp. 212 \& 213. This improvement, known as the "Collingwood" pattern after the battleship for which it was first mounted, represented a change in emphasis. First class battleships were now fitted with a secondary armament of 6 -inch BLRs which, due to the different ballistics, could not be grouped with the heavy guns of the main armament. So the modified Director was used for the main armament only, and the secondary guns fired independently.

The modifications consisted of:
> the trunnions of the telescope were moved to the outer end and mounted on a pivot. This reduced the required size of the sighting port and kept all movement inside the conning tower;
> the graduated arcs were eliminated, and replaced with graduated movable collars around the inner end of the telescope;
> the 'speed correction' was shown in knots, which eliminated two sets of reference tables, which increased the speed of operation;
> the convergence point for Director firing was increased to 800 yards.
The price for these improvements in operations, and especially the more efficient manner of handling the corrections, meant that each unit was specifically fitted and graduated for the ship in which it was mounted. In other words, there would be one set of tables and corrections for Collingwood and her 12 -inch guns, and a different set of tables for her half-sister Benbow, which carried 13.5-inch guns.

The final iteration in the $19^{\text {th }}$ C entury was known "double dial" gun director, developed in the early 1890s for the Royal Soveriegn class battleships. The modifications consisted of:
> a more powerful telescope with greater magnification and better focusing;
$>$ a graduated dial with a pointer was placed on each side of the telescope; on the right for the 'dip correction' and required elevation, and on the left for training and speed across corrections for the bow, beam or quarter convergence positions. The graduations of these dials was finer and more accurate than the scal es in the previous patterns.

The voice pipes were now equipped with electric bells and indicators to alert gunnery personnel of incoming messages.
${ }^{16}$ A leksei Pavelovich Dayvdov was a prodigious inventor, and single-handedly put Russia into the premier position in gunnery among the navies of the world, for a period of some ten years.

The first device, known as the 'galvanic [battery powered] electromagnetic lock,' was tested aboard Sevastopol in 1865. Basically, this used an electromagnet to initiate the hammer lock which fired the guns, and may be considered the first electric firing mechanism.

Other elements were tested in Pervenets in 1872, and the complete system was tried and accepted in 1876 and deployed the following year. By 1880 some 30 ironclads and large cruisers had been fitted with the system.

In brief, the revolved around a Director Sight arranged on a base with markers corresponding to the fixed angles to be used by the guns, and the galvanic firing key. From the bow, these angles were $45-\mathrm{deg}, 90-\mathrm{deg}$ and $135-\mathrm{deg}$. However, the firing circuit had to be closed in four distinct places to actually fire the guns.

The first step in the process was the Gunnery Officer selecting a target, fixing the Director Sight on the fixed angle most appropriate to the situation, and determining the range at which to fire. This information was communicated to the guns - choice of angle and range in 'cables' [200 yards each].

The gunners had two indicator status switches next to their gun. When set for 'aiming' the gun was not connected to the electrical circuit, and the gun was trained to the proper angle and the rear sight adjusted for the proper range. The status indicator was then changed to 'ready' and their portion of the circuit with the inclinometer was closed.

The next step was to maneuver the ship to bring the guns into line with the target. Near the helmsman was a 'steering apparatus/instrument' which showed the three fixed gun angles and a 'galvanic indicator' which was synchronized with the Director Sight. The helmsman's task was to steer the ship so that the indicator was aligned with the correct gun angle, thus closing another part of the firing circuit.

When the ship was properly aligned and all the guns reported 'ready,' and the Director Sight was aligned with the target, the Gunnery Officer closed his firing key, closing that portion of the firing circuit.

The final step was particularly ingenious. Davydov had developed a 'galvanic inclinometer' in which a pendulum swung along a graduated arc. In the 'zero' position of the roll cycle, the pendulum closed the final portion of the circuit, which initiated firing the guns.

Some thirty ships of the Baltic and Black Sea Fleets were equipped with the system by 1880, and it remained in service through the 1880s, when it was overtaken by advancing technology.

As a practical matter, the guns could certainly fire independent of the Director, on local control, with range and target bearing provided by the Gunnery Officer, but not using the galvanic firing system. In this mode of operation, they certainly would have performed as well as Shah, though there is an unfortunate lack of combat use to demonstrate the capabilities of the system.

A .V. K hramoi, History of A utomation in Russia B efore 1917 (English translation; J erusaIem: Israel Program for Scientific Translations,1969), pp. 87,134,135,179-181. And Captain Dr. A.V. Platonov, "Domestic Gear for Controlling A rtillery Fire," Tsitadel, No. 6 (no. 1, 1998), p.94, (translated by Steve McLaughlin). A nd Norman Friedman, Naval Firepower, Battleship Guns and Gunnery in the Dreadnought Era (A nnapolis: N aval Institute Press, 2008), p. 170.
${ }^{17}$ A.P. Davydov continued his work on fire control to at least 1890. While the information is very sketchy, and there is no certain if any of his subsequent inventions were actually accepted and deployed, an account of his work is indicative. It is extremely unfortunate that no drawings or specifications have survived.

1) It appears that an application of his 'steering indicator' was used with what we might call 'follow the pointer' instruments. "When the gun layer behind the gun aims at a moving target through the sights of a 'galvanic indicator,' an indicating device in front of the gun crew shows the same marks as do the sights, so that the crew, by traversing the gun mounting that carries both the gun and the layer, can al ways keep the gun aimed at the moving target." The wording is stilted and obscure, but 'galvanic indicator' is the term used for the Director Telescope. This seems to indicate that there was a pointer in the gun layer's sight and another in front of the mount, synchronized with the Director Telescope.
2) It also appears that in 1881 Davydov developed a means of electrical control of gun elevation. "... the gun elevating gear has special contacts connected with the range finder [sic] and so arranged that, when the elevating handwheel is turned, the gun elevation will be the correct one for the
range finder indication... the handwheel does not have to be turned continuously, but only for a few seconds." In a report to the Russian Engineering Society, Captain L.P. Semechkin commented on this proposed design on 5 J une 1991; "A s regards continuous setting of guns at elevation angles corresponding to the movement of the enemy, which is followed-up by a special observer, who determines the changing range, Davydov goes very far and offers the design of a gun mount that will set the gun at the required angles, this arrangement being the only one that ensures correct azimuth and elevation at the moment of firing." Unfortunately, there is no hard evidence what form of device this was, but the 'special [electrical] contacts' in the absence of powerful electric motors capable of elevating many tons of gun, and that the actual change in elevation was accomplished by the handwheel, implies something akin to a 'follow the pointer' set-up where a crew member turns the handwheel to match a pointer. Such an arrangement was within the technology already demonstrated by the 'steering indi cator' that was part of his Director system, though this is speculation.
3) Davydov also worked on gun stabilization to compensate for roll. The device "Iinked the indicator of the inclinometer with the el evating gear contacts in such a way that the gun elevation would be increased or decreased by an angle compensating for the ship's roll and pitch, so the gun could be fird at any time at the correct elevation." This would certainly be an ingenuous use of the inclinometer. One is reminded of the abferungs Gerat used by the Imperial German Navy after J utland which used a gyro device to stabilize the gun relative to the target, so the concept is certainly valid. It is unfortunate that the details of the design have not survived.
4) In 1877, Davydov devised a complete system for the indirect fire of coastal guns. The test shoot was done with 6 -inch mortars located behind a forest where it could not see either the target or the fire control post. A target was mounted on a boat with a beam of one meter, being towed at a speed of 9 knots. The fire control post could see the target, but not the guns. Davydov tested the system off $V$ yborg in 1879, and direct hits were achieved at a range of about 2150 meters.

The heart of the system was some form of calculator! As Davydov wrote at the time, "The lead does not depend on man's considerations but by the nature of things, ie., on the time taken by the shell and the speed of the enemy vessel. Prediction is done automatically and does not require any calculations or other combinational considerations by fire control personnel." He described the device/system to the Director of the M inistry of M arine on 28 February 1890 as folIows: "My automatic method of imparting the correct elevation to the guns requires that quadratic equations be solved immediately and automatically, that is, that, in accordance with the movement of the target, followed by the range finder, the guns be set immediately and automatically at the corresponding elevation angles, with an accuracy of 1 -deg/40 minutes or 1/14.4 of a circle, and this in addition to being simultaneously imparted both a vertical and a horizontal lead in accordance with the movement of the said target."

It should be noted that whatever this device was, it performed 23 years before the Dumaresq, and testifies to Davydov's genius. K hramoi, op.cit., pp. 134 \& 135, 181 \& 182.
${ }^{18}$ Richard N.J. W right, The Chinese Steam Navy, 1862-1945 (L ondon: Chatham Publishing, 2000), p. 60.
${ }^{19}$ Paolo E. Coletta, Admiral Bradley A. Fiske and the A merican Navy (Lawrence: The Regents Press of K ansas, 1979) pp. 19, 20, 21, 30.
${ }^{20}$ Ibid., pp. 28-28.
${ }^{21}$ Ibid., p. 29.
${ }^{22}$ Ibid., p. 38.
${ }^{23}$ Ibid., pp. 31, 32, 35.
All Range Finders, be they sextant-type, two observer or single observer instruments operate on the same principle; to wit, a trigonometric problem. They are all based on the following reasoning; if one knows the length of one side and two angles of a triangle, the length of the other sides and the third angle can be calculated easily. From there it is a simple process to determine the linear range from the firing ship to the target.

The earliest attempts to determine the range used sextant-type devices. In this case, the object being measured was the height of the main mast above the deck. Using this figure as the
'base line' combined with the two angles - the one at the deck assumed to be 90-deg. and the other determined by the sextant representing the angle from the top of the mast to the observer the calculations are rather simple. However, the error factor creeps into the situation in two forms; the height of the mast is not correctly known, and the roll of the observer's own ship tends to distort the results. The Russians developed an instrument to be used horizontally rather than vertically, using the length of the target ship, which produced much better results. The obvious problem was the angle of and/or the heading of the target ship, which would distort the 'base line' and produce inaccuracies.

The two observer system, as invented by Fiske and developed independently by the Imperial German Navy, was much more reliable. In this case, as described, the base line is the known distance between the two observer stations, each of which produces an angle to a prominent feature of the target, such as the fore mast or forward funnel. In this system, the base line is known and the two angles reliably acquired, It would produce accurate results from about any angle from which both observers could sight on the target.

The single observer equipment, in this period represented by Bar \& Stroud, provides the known base line, in this case the length of the instrument itself, and through a system of lenses and mirrors, allows the range to be determined. But its accurate range is limited by the length of its base line; longer instruments being much more accurate over longer ranges than short base line instruments.
${ }^{24}$ Ibid., p. 54.
${ }^{25}$ M ichael M oss and Iaian Russell, Range and Vision, The First Hundred Y ears of Barr \& Stroud (Edinburgh: M ai nstream Publishing Company Ltd., 1988), p. 20.
${ }^{26}$ Ibid, op.cit., pp. 30-33.
${ }^{27}$ Coletta, op.cit., p. 36 .
${ }^{28}$ Ibid, op.cit., p. 44.
${ }^{29}$ K arl Lautenschlager, "A M ajestic Revolution," Warship V olume VII (London: Conway M aritime Press, 1983), p. 111.
${ }^{30}$ John Spencer, "Conduite du Tir: the Birth of Centralized Fire Control," Warship 2010 (London: Conway Publishing, 2010), pp. 159, 165, 165.
${ }^{31}$ A very great technical problem was getting the information from the Gunnery Officer to the guns. As previously mentioned, the Elliot Director relied on the ew [in 1868] voice pipe technology. In 1880, Percy Scott joined HMS Inconstant as the Gunnery Lieutenant. This ship, the first of the I arge iron frigates, completed in 1869, and had neither boice pipes nor Elliot Director. Scott designed a range telegraph along the lines of the bridge to engine room telegraphs, and submitted it to the A dmi ralty in M ay 1881. Unfortunately it was not taken up until after the turn of the century.

B etween 1885 and 1893, Bradley Fiske had patented a number of devices which, taken in sum, would have constituted a Director system. However, he had changed his focus to the individual guns and had perfected an electric range transmitter and the range indicator receiving unit, coupled with his speed and direction indicator passed the necessary information to the guns or battery. With his range finder, these instruments were widely used in the New Navy.

The French Navy had not developed a Director, but in the early 1890s were keenly aware of the importance of Range and Order Transmitters to get the necessary information from the Gunnery Officer to the batteries of Quick Firing guns. The first proposal for such a system to warrant trials came from L V L oncelet in 1893. This was a system of cables and lamps to transmit bearing, range and deflection. Each turret/barbette would have eight cables for eight lamps. But the system could handle only five pre-set ranges between 400 and 2200 meters, and deflection was also restricted to five values. It was tried on the Neptune, but was ultimately considered insufficient.

A system from L V G, Eng was tried in 1895 in Amiral Duperre' successfully, and by November of 1897 was aboard Brennus, J ureguiberry, M arceau, Neptune and Amiral Charner. The equipment involved six dials to be read in pairs, from right to left. The right hand dial for range was graduated in 1000 meter increments, from 1000 to 4000. The left hand dial was graduated in 100 meter increments from 0 to 900 . The right hand Deflection dial was split into right and left scales, to distinguish between fore and aft direction of target movement. It showed target speed
in knots in 10 knot increments from 0 to 30 on each side. A nd the left hand dial was denoted in knots from 0 to 9 . Target bearing was handled much the same as deflection. Both sides of the Right hand dial had two increments, 0 and 100, while the left hand dial was graduated in 10 degree increments from 0 to 90 .

In early 1898 a competing system appeared, having previously been tried on the cruiser LatoucheTreville. This was the L V Germain hydraulic system using nanometers instead of electric voltmeters as in the Eng system. It had only four dials, including one for orders. Deflection, right and left, was in 2 knot increments between 0 and 30. Range was in 100 meter increments from 1000 to 5000 . A nd bearing was given on a single scale from 10 degrees to 180 degrees in 10 degree increments. Trials in 1899 proved so successful that it supplanted the Eng system for new construction.

Barr \& Stroud had offered to develop a 'Range and Order' system, and when the British A dmiralty affirmed interest in June 1892, development began in earnest. Prototypes were ready in 1894, and the device was ready for sale in July of 1898. B ut while the A dmiralty was deciding whether to buy, the J apanese N avy began placing orders for the new 'Range and Order Indicator' before the end of that month! By February 1901, 30 transmitters and over 200 receivers had been sold; one set to the A dmiralty for trials aboard Canopus, and another set for an A rgentine coastal fort, with the balance being bought by Japan. The device was entirely electric, using electromagnets to synchronize the pointers betw een the transmitter and the receivers.

Padfield, op.cit., p. 48. A nd Coletta, op.cit., p.38. A nd John Spencer, "C onduite du Tir: the Birth of Centralized Fire C ontrol," W arship 2010 (London: Conway Publishing, 2010), pp. 165 169. A nd M oss and Russel, op.cit., pp. 34 \& 34.
${ }^{32}$ The Russian Navy also abandoned Director Control for the reasons noted above. They al so saw salvo firing as too limiting, as the rate of fire was determined by the slowest gun. In the case of the slow firing heavy guns, this was an obvious conclusion. Early on, the Russian Navy had adopted a standard battery caliber of 6 -inch guns which, with their $M .1877$ family of guns, had a rate of fire substantially quicker than the heavier guns [if contemporary US naval guns are any measure]. This led to the change to decentralized shooting, with the role of the Gunnery Officer being to supply the relevant data for sight setting. However, this produced a practical limitation insofar as spotting the fire of an individual gun was left to the layer/gun captain of that gun. B eyond a range of 10 cables [2000 yards] such spotting became confused with the fire of other guns, reducing the ability to make corrections.

The solution came in 1893/94 with the system produced by the N.K. Geisler and Co. electromechanical works. This well conceived system integrated multiple functions in the following manner:

1) The range finder positions [Stadimeters; B \& S optical rangefinders for evaluation were only received in 1899], two of which were in the tops, were equipped with electric 'range transmitters;'
2) The Gunnery Officer in the conning tower had the receivers in the 'main range finder' display, and could evaluate the ranges received and enter the result in his own 'range transmitting dial' to the guns;
3) Target bearing was determined by use of a 'battle indicator' [an improved Davydov telescopic sight] and transmitted to the guns;
4) The manually calculated deflection was also transmitted to the guns in the same manner;
5) The 'battle transmitting dial' was used for basic orders: 'short alarm' [Ready for centralized salvo firing by electric firing circuit], 'Attack' [Fire! Independently], and 'Drumming' [C ease Fire].
6) With the 'shell transmitting dial' the Gunnery Officer could specify the type of ammunition to be used, be it armor piercing, Common high explosive, shrapnet [for defense against torpedo boats and destroyers] or practice [old cast iron projectiles].

N ote that during independent firing, range, target bearing and deflection would be updated continually, which included spotting corrections.

As with the French system mentioned above, the main weapon of attack was the QF battery, with the heavier guns joining as they were able.

W hile the Geisler system was conceptually very advanced, and shared many aspects of the later Director systems, it was limited in its efficacy by the lack of optical and more accurate range finders and telescopic sights for the guns, and any form of mechanical calculstion device for solving the Fire Control problem. Still, it was the best system produced in the late XIX century. N orman Friedman, U S Naval W eapons (A nnapolis: Naval Institute Press), p. 17. A nd Platonov, op.cit., pp. 94-96. A nd Stephen M cL aughlin, Russian \& Soviet Battleships (A nnapolis: N aval Institute Press, 2003), pp. 35, 63, 75, 81, 88, 112.
${ }^{33}$ Friedman, Naval Firepower, op.cit., p. 158. And Guy Hartcup, The War of Invetion (L ondon: Brassey's Defence Publishers, 1988), pp. 12 \& 14. A nd Paul Schmalenbach, Die Geschichte der Deutschen Schiffs-A rtillerie (Herford: K oehlers V erlagsgesellschaft mbH, 1968), pp. 57-62. And Paul Schmalenbach, "German Heavy Large Bore Guns Operational A shore During W orld W ar I," W arship International, No. 2, 1983, p. 148.
${ }^{34}$ The Gabelverfahren system had its crude origins in the Prussian A rmy Field Artillery in 1875. Their simple device consisted of two short poles connected by a known length of chain. On top of each pole was a graduaged plate with a sight bar. By aligning each sight bar with the same target, the two angles would be used with a pre-calculated Table to provide the range.

This concept was given to the Navy in 1880 for use in the coastal fortifications. O bviously the naval version would be scal ed up considerably, and the problem of communications between the now distant observer stations and the fire control center addressed. In the aftermath of the Bayern's shoot, in addition to ordering range tables for the guns in the fleet, von Thomsen initiated a test project to determine if the two station range finder and conversion tables could be adopted for naval use. Over the next few years, a test ship [possibly Oldenburg] was used for experiments in the Baltic. By 1890 the results were favorable, and von Thomsen authorized its formal development, and in 1893 the system was accepted for deployment. The first ships constructed with the equipment were the K urfurst F riedrich Wilhelm class, and the ironclad K aiser the first to receive it during her re-construction.

In these early installations, a special circular top wa fitted to the fore and aft masts, generally at the same height. They were sheltered from the elements but had 360 -degree traverse. On the inside rim was a finely graduated scale, and most likely races in the deck for movement of the sighting telescope. Each nearly identical top was connected to the conning tower by mechanical telegraph for reporting the angle of observation. The crows' nests, mounted still higher on the masts, were for spotting.

In the conning tower, calculations from successive range takes were used to calculate the rate of change of range, rate of horizontal deflection, target speed and course, and of course range. B earing and range were then communicated to the guns, likely by voice pipe or possibly by mechanical telegraph. There is no evidence to hand that either a Director or electrical firing was used, nor what means were used to deal with the roll cycle.

In 1897 the system was upgraded considerably. The mechanical telegraphs were replaced by electric telegraph units, and a new device was added, quite possibly as a result of Dr. Raps and Siemens Halske's work. It was known as the Stand Gerat [St.G] it was to measure target bearing and change of bearing rate. This was most likely a telescopic sight mounted on a stand with a graduated ring, located on or near the conning tower. Its use simplified the calculation process by eliminating a number of steps, and thereby enhanced the speed of the FC solutions. Dariusz M zurowski, e-mails to the author dated February 11 and 25, 2005, summarizing information from an article by K oop \& Schmolke.
${ }^{35}$ Wright, op.cit, pp 86 - 93. And H.W. Wilson, Ironclads in Action, V ol. II (London: Sampson Low, M arston and Company Limited, 1896), pp. 88 - 111. A nd Peter B rook, "The Battle of the Y alu, 17 September 1894, " Warship 1999-2000 (CL ondon: Conway M aritime Press, 1999), pp. 37-41.
${ }^{36}$ H.W. Wilson, The Downfall of Spain (London: Sampson Low, M arston and Company Limited, 1900) pp. 146 \& 146, 172 \& 173, 338 - 340. Peter Brook, "Spain's Farewell to Great-
ness: The Battle of Santiago, 3 July 1898," Warship 2001-2002 (London: Conway M aritime Press, 2001), p. 44. A nd Coletta, op.cit., pp. $54 \& 55$.

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## HELP SOLVE AN HISTORICAL MYSTERY!

In 1859 France completed the first ocean-going ironclad warship, «La Gloire», and changed the definition of naval power completely. Russia, as all the other Powers, found that her most powerful naval gun, the 60-pdr, was insufficient for modern warfare, and real ized the future naval armament relied on heavy rifled artillery. Both the A rmy and Navy began purchasing such cannon from foreign providers until a suitable domestic weapon could be produced. The relationship between the Russian military and K rupp is well known. But there was another provided, the Blakely Ordnance Company in England sold many guns to the Army and Navy, beginning with 8 -inch M LR in early 1863 to a large number of 9 - and 11 -inch guns. Deliveries began in November 1863 and continued until mid-1866. But no sources on the armament of Russian ships and fortresses mentions these guns. What happened to them is a mystery.

С постройкой во Франции в 1859 г. первого океанского броненосца «Ла Глуар», ситуация с ранжированием военно-морской силы кардинально поменялась. В России, как и в других державах, неожиданно обнаружили, что самые мощные 60 -фнт орудия стали недостаточными для современной войны, и стало понятно, что будущее военно-морских вооружений за тяжелой нарезной артиллерией. И армия, и флот начали искать зарубежных поставщиков, пока это оружие налаживалось в производстве на отечественных заводах. В настоящее время хорошо известны связи между русскими военными и Круппом. Но был и другой поставщик - компания Блекли из Англии, которая продала множество пушек для армии и флота, начиная с 8" дульнозарядных нарезных в начале 1863 г. и большим числом 9 " и 11". Поставки начались в ноябре 1863 г. и продолжались до середины 1866 г. Но до сих пор нет однозначного ответа - на вооружении каких кораблей и крепостей стояли эти орудия. Что произошло с ними - также остается загадкой.

In the process of researching an entirely different subject, I came across some information that bore directly on the history of the Russian Navy and Coastal Fortifications during the years from 1860 to 1867. The predominant view, especially in the W est, is that the revolutionary change to ocean-going ironclad warships and heavy rifled artillery left Russia with nothing but smooth bore guns until the M. 1867 guns began to be produced. This has always struck me as unlikely, and now there is evidence to refute that common view.

The story seems to be this; in 1862 Captain A lexander Blakely, late of the Royal A rtillery and one of the preimmenient artillery designers of the age, sent two heavy guns to St. Petersburg to be tested. These two guns were possibly an 8 -inch 200 pdr steel muzzle loading rifle, and an 11-inch cast iron reinforced with steel hoops, capable of firing a $400 \mathrm{lb}(181.4 \mathrm{~kg}$ ) bolt using a $35 \mathrm{lb}(15.88 \mathrm{~kg})$ charge of black powder. [see the illustrations] It appears the Russian Navy and Army were pleased, and there is indication that a number of 8 -inch, and perhaps 6 -inch 70 pdr , guns were ordered for the Fleet.

Early in 1863, Blakely was in St. Petersburg, and entered into a partnership with Francis Biard ('Bard' in Russian). Francis owned and operated a foundry, originally started by his father Charles in 1762, located in K olomenskaia on the mouth of the Neva River to the West of the city. Their efforts were rewarded in October of that year with C ontracts from the Navy for 9 -inch all steel guns for sea
service, and 11-inch all steel guns for the A rmy for K ronstadt and other fortresses protecting St. Petersburg. The total number of guns seems to have been 160.

The first of the 11 -inch guns for the order from Blakely's English facilities began in November 1863, and the planned rate of production was one gun per month for the following two years. Deliveries of the 9 -inch guns from England began in February 1864. By October 1864 some forty of the 11-inch guns had either already been delivered or were in various stages of construction; a rate faster than the one gun per month planned the previous year.

Unfortunately, production at the Bard foundry is not known...
It appears that the Russian Army and Navy were happy with the guns there were receiving, for in M arch 1865 they increased the quantity to 220 guns, specifying 8 -inch, 9 -inch and 11 -inch guns. There may have been a clause in the contract for the A rmy that encouraged Blakely to think in terms of larger and more powerful guns that the 11-inch, for in J une 1865 he had a 12.75-inch 900-pdr gun (similar to the guns sent to Charleston, see illustrations) under construction for them.

All of this activity did not go unnoticed. For one thing, large sums of money were involved. The 160 guns ordered in 1863, with carriages, amounted to 960,000 Pounds. Even a M ember of Parliament noted the "... immense orders for the Russian Government - 11-inch gund for the defence of Cronstadt [sic], and 8-inch guns for the Russian Fleet... the iron-clad fleet of Russia was now [1865] armed with Krupp's and Blakely's guns..." and speculated on the power of those guns against Britain's own ironclad warships.

The big question becomes what happened to all of those guns? From early 1863 to the time his business collapsed in 1866-67, Blakely's English facilities possibly delivered 200 guns to St. Petersburg, not including any production by B ard. $Y$ et there seems to be no record or evidence of their use.

I examined Shirokorad's wonderful tome on Russian Artillery. There seemed to be some hints, but nothing specific. Then I saw the drawing on page 127. It purports to be the K rupp 9-inch smooth bores that were "supposedly" mounted on the monitors in 1865-66. Y et it did not resemble any K rupp configuration I was familiar with. So I examined Holley's Treatise on Ordnance and Armour from 1865. In it I found a drawing of the 9-inch K rupp smooth bore and a drawing of a 9-inch Blakely rifle. The two were not similar, but the Blakely gun and the drawing on page 127 are strikingly similar! (see illustrations) We therefore have a modus ponens logic problem:

If the Holley drawings are accurate, and
If the drawing Shirokorad provided on p .127 is an accurate representation of the guns on the monitors,

Then the guns on the monitors were Blakely and not K rupp.
While this might be indicative, it is not conclusive. Nor is it conclusive that some of the projectiles for muzzle loading rifles strongly resemble the Blakely pattern, neither that of the French nor that of A rmstrong.

Rifled artillery was introduced into the Russian Fleet as early as 1860 aboard the wooden Gaidamak, in the form of four 3.4-inch $4-\mathrm{pdr}$ guns to supplement the smooth bores. The following year saw the 4.2-inch 8pdr gun carried in the wooden

Abrek. In 1862, the wooden Almaz and her three sisters carried three 6-inch rifled, two 4.2-inch rifled and two 3.4-inch rifled.


Image 1 B lakely 9-inch gun from Holley [1, p. 40]


Image 2 K rupp 9-inch smooth bore from Holley [1, p. 93]


Image 3 11-inch Blakely gun probably sent in 1862, cast iron with steel hoops.
A nd the 12.75 -inch gun from Charl eston. Blakely may have sent an improved version to St Petersburg. From Holley [1, p. 44]

The 4pdr and $8 p d r$ guns were developed in Russia who began experimenting in 1858 to copy the "French" system. But at that time, the French were using two or three grooves, whereas the Russians settled on six grooves. So what was called the "French" system may very well have originated in Britain, possibly with A rmstrong or Blakely.


Image 4 8-inch all steel gun of the type sent to St Petersburg, from Holley [1, p. 41]


Image 5 From page 127 of Shirokorod's tome [3, c. 127]
The origins of the 6 -in rifled are something of a mystery. We do not know if the guns were muzzle- or breech- Ioaders. If they were breech loaders, than K rupp is the most likely provider. If they were muzzle-loaders then the possible sources are very limited. At that time, 6 -in was an unlikely caliber. The only two potential suppliers were Dahlgren and Blakely. The former can probably be ruled out, as the 80-pdr had the disconcerting tendency to burst, so most likely Blakely's 70-pdr provided these guns.

In summary, if the Russian Navy saw fit to put some rifled guns - admittedly shell guns -- on several small wooden ships, does it stand to reason that the ironclads and steam warships, still the body of the Fleet, must make do with smooth bores, especially considering the tremendous sum of money the Government paid to Blakely and K rupp? I think not. I believe the story of the 1860 to 1867 period has yet to be told. The trick, of course, is to find the evidence.

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## THOUGHTSON THE NAVAL TECHNOLOGY USED IN THE BATTLE OF THE YALU


#### Abstract

Naval Combat is invariably a clash of technologies. The Battle of the $Y$ alu is unique in that it was the last battle in which ironclads participated, and the first battle influenced by the new technologies of Range Finders and Quick Firing guns, and represents the transition from Black Powder propellants to slow burning Brown Powder and nitrocellulose propellants. This article seeks to focus on the technologies involved as a partial explanation of its outcome.


Морской бой представляет собой войну технологий. В этом отношении битва на Ялу уникальна тем, что это был последний бой, в котором участвовали броненосцы, и первый бой в котором сказалось влияние новых технологий: дальномеров и скорострельных орудий, и переход от дымного черного пороха, для замедления горения на коричневый порох и порох на основе нитроцеллюлозы. Эта статья представляет попытку объяснения результатов сражения путем анализа этих технологий.

Naval combat invariably is a confrontation between technologies, influenced by the people involved. A detailed study of any naval battle, be it Salamis, Trafalgar, Lissa, T sushima, Jutland or Leyte Gulf, reveals men compensating for a technical inferiority or exploiting a technical superiority.

The Battle of the Y alu is no different. The Chinese fleet represented the best technology of the 1880s. The Japanese fleet represented a "mixed bag" of technologies, but were the clear victors. This brief paper is intended to examine the Fire Control/Gunnery technologies of both sides, hopefully to increase understanding of this brief period in history.

The engagement was fought at very close range. Compared to the well known actions at long range, such as the Run to the South at Jutland, or Bismarck and Hood, which have accustomed us to multiple thousands of meters range, the Battle of the $Y$ alu was fought at "spitting distance." The reason for this was primarily technical. These technical aspects also explain why gunnery practice and Battle Practice was made at short ranges, among all $N$ avies.

First, it is necessary to understand that the Breech Loading Rifles (BLRs or RBLs) fired very slowly. Compared to the combats in the First and Second W orld Wars, the Battle of the Yalu was naval action in slow motion. Tactics and combat capabilities were severely limited by this aspect.

Under ideal conditions, which of course did not exist in real life, the M uzzle Loading Rifles (MLRs or RMLs) could fire once every four minutes. The large BLRs of the 1860s and 1870s were not any better. This begs the question of Fire Control, defined as calculating where the target will be in terms of range, bearing angle, and estimated target course angle. In a five minute period, a ship steaming at 12 knots will travel a distance of 1852 meters ( 2160 meters at 14 knots), which is several ship lengths. Even if the target cooperates and maintains a straight course, the changes in the situation are considerable. Consequently, each shot must have a new solution.

These Fire Control solutions were entirely manual. Target range was either estimated by eye, or estimated with a sextant-like instrument which keyed off the waterline and the known height of some feature, such as mast or funnel height. Obviously accurate estimates were increasingly difficult as range increased. A n accurate and reliable rangefinder would do much to improve the situation.

The "state of the art" of gunnery may be described in the following eye witness accounts. A ccording to Admiral George Ballard, as a young man aboard the Resistance in 1876, the rear sight had ranges marked off up to 4,000 yards, but "... firing practices were very seldom carried out at more than 800. " A Petty Officer aboard Victoria in the 1890s noted that "the target was usually a spar with a red flag on it, at a distance of some two thousand yards or less... " A nd Admiral Ballard, while aboard Temeraire in 1884, described the A nnual Prize Firing as a target "stretched on a row of poles on a raft... and ranges of about 900 to 1,400 yards were marked by buoys instead of being left to guess work..." At the time of the Y alu battle, the Imperial German Navy, the most advanced in the development of long range gunnery, had only recently increased their practice range to 2,500 meters.

The only ship equipped with a viable rangefinder was the Japanese cruiser Yoshino, which carried the eighth production model of the Barr and Stroud optical coincidence instrument. But this single device allowed the "Flying Squadron" to engage effectively at the then unheard of range of 3,000 yards, and gave the J apanese a tremendous advantage.

While firing to the correct range is no doubt a great accomplishment, the guns still needed to be laid correctly. All of the guns in the Chinese and Japanese fleets had only open sights, attached to the guns! Like a modern hunting rifle, the rear sight must be lined by eye with the front sight and the target. For the hunter, this is a precision skill. But imagine attempting the same feat with a gun weighing many tons, in the absence of precision controls for both elevation and traverse. Now imagine performing the task on a rolling and pitching ship at sea.

The "state of the art" called for firing "on the roll" when the sights were on target. There were two problems with this method. First, the recoil of one of the big guns would affect the motion of the ship, providing a de facto delay to other guns. Either the gun captain waited for the roll before firing his gun, or the gun was fired anyway, producing questionable results. A nd second, firing "on the roll" required that the target be visible.

Guns using black powder as a propellant produce a lot of smoke! And the smoke tends to linger in the area, making hazy conditions if not outright impenetrable fog. And virtually all of the guns in the Chinese and Japanese fleets used black powder. The most common propellant was Prismatic Black; a compressed mold of powder intended for slower ignition than loose powder. However, the nature of black powder prohibits dependable regularity of burning. This also mitigated in favor of short ranges, as the irregular performance of the propellant equated to irregular and undependable ranging, so the greater the range, the less likelihood being able to consistently fire to that range.

By extension, the test of the 71 -ton ( 40 cm bore) at M eppen on 5 A ugust 1879 will serve as an example. Under ideal conditions, that is stable test platform and
every effort made to duplicate the same conditions for each shot, the gun was fired several times at a range of 2,500 meters. The results were described as "very accurate... excluding the first two regarded as trial shots, the vertical dispersion was only 17 3/4 inches and the lateral dispersion 71 inches..." By inference, these variations are primarily due to the irregular burning of the Prismatic Black powder used as the propellant. From a rolling and pitching deck of a ship, such irregularity decreased the possibility of accurate shooting as range increases.

In the mid 1880s, Brown Powder came into use. This had the advantage of producing about half the smoke as black powder. It also burned with much greater regularity than did black powder. This made it more suitable for the "Quick Firing" gun cartridges then being introduced, and as a secondary effect, promoted firing at longer ranges.

But Brown Powder was being eclipsed by the advent of "smokeless" (by comparison with Black and Brown powder) nitro-cellulose powders, such as the British Cordite, the French Poudre B, and Noble's B allistite. Of all the guns used at the Y alu, only the newer guns used Brown Powder, and only the Yoshino had Cordite for her Quick Firing guns. M ost of the Chinese guns used Prismatic Black powder, and the rest used Brown Powder.

The devices that would compensate for roll and provide simultaneous fire of the guns were already in existence. These were the Director Sight and electrical ignition circuits to the guns. The latter had been developed around 1868 in the British Royal Navy, and so was widely known. Y et even in the mid-1880s it was offered as an option by A rmstrongs, and presumably by K rupp.

The history of the Director is a subject still awaiting full investigation. It seems to have been invented in the early 1850s by a Captain M oorsom, RN. In the mid-1870s, Admiral Sir George Elliot developed a serviceable Director system, first used successfully by Shah in her bout with the Huascar in 1877. Its use at A lexandria, Egypt, in 1882 gave mixed reviews. The problem was a method of communication from the Gunnery Officer to the guns, as the voice tube seemed insufficient in the din of battle. Sir Percy Scott, when a young Lieutenant in 1881, invented an electronic device to visually transmit information to the guns; but it was still lying dormant in the Admiralty. Bradley Fiske also invented electronic range transmitters and indicators, but they were not available outside the U.S. Navy. A nd B arr and Stroud began development of electric range and order indicators only in 1894.

However, four of the ships built by Armstrongs were equipped with both the Director and electrical circuits for salvo firing, two on each side! These were the Japanese Naniwa and Takachiho, and the Chinese Chih Yuen and Ching Yuen. From a gunnery effectiveness view, it is interesting that both the Japanese ships were in the Flying Squadron with Yoshino. Even though both were armed with slow firing BLRs, their ability to shoot accurately would be greatly enhanced.

A nother side effect of the slow rate of fire of the BLRs was that a large ammunition supply was not required. There is not a great deal of specific information available, but what is widely known is probably indicative. By way of example, the official load-out of the Chinese Ch'ao Yung class, which includes the Japanese

Tsukushi, was 34 Common, 10 Shrapnel, 6 case shot, 36 chilled (Palliser) shells, and 14 chilled (Palliser) shot per ship. This is fifty rounds per 10 " gun. For the short 4.7" guns, the supply was 12 Common, 30 segmental, 30 shrapnel, and 10 case shell per gun. The Chen Yuen class battleships carried fifty rounds per 30.5 cm gun. The $M$ atsushima type had sixty rounds for the 32 cm guns, and one hundred for each 4.7-inch QF.

Bursters were most likely black powder. The British seemed loathe to experiment with high explosive fillers, only approving the use of Lyddite for medium caliber Common shell in the late 1890s, in time for Kitchener's march up the Nile. The Germans adopted gun-cotton in 1883 ( $G f / 83$ ), and the French shortly thereafter, but its use was short lived, being superseded by picric acid in the late 1880s ( $G f / 88$ for the Germans, M elinite for the French). If some of the German made shells were filled with gun-cotton, it would in part explain why there was a shortage of explosive shells in the Chinese fleet; the valuable gun-cotton was removed and sold for its industrial/commercial uses. Nor could the supply of domestically produced shells could not be trusted. A s Richard N.J. W right noted, "Ping Yuen scored a direct hit on $M$ atsushima at one point with her 10.2 -inch [ 26 cm ] gun. Unfortunately the shell was Tientsin-made and found to contain cement, not HE."


The late Peter Brook drew some conclusions in his treatment of the B attle of the $Y$ alu, which deserve some closer scrutiny. He noted that "The battle exploded the myth that small, fast unarmoured ships carrying a powerful big gun armament could, by means of superior speed, defeat a battleship by choosing their own decisive range. Ch'ao Yung, Yung Wei, Naniwa, Takachiho and the three big J apanese cruisers were all designed on this principle." This statement is misleading at best, and only partially valid.

In his Warships for Export, Dr. Brook gives the background of the so-called Elswick Cruisers at some length. The original memorandum was probably written by Stewart Randel in the late 1870s, and explained the specifications of the new cruiser type with its vitals protected by an armored deck only. Hence, they were the proto-types of the Protected Cruiser, and not completely unarmored or unprotected. The wording of the quote above is a little obscure, and seems to imply that a single such cruiser could overcome an ironclad battleship. Y et the specific memorandum says something quite different. "These larger [than gunboat] vessels from their great speed and artillery power combined, would be able to follow up and search out ironclads and to choose their own mode and time of attack... five of the new vessels could be built for the cost of one such ironclad. Collectively, they would offer greater power than the ironclad." From the use of plurals when referring to the small cruisers, and the singular "ironclad," it is logical that several such cruisers would combine against a single ironclad. It is equally obvious that this type of cruiser was never intended to be confined to a line of battle. In the context of when the memorandum was written, and bearing in mind the slow rate of fire which characterized the big guns of that time, it is entirely reasonable to envision a
division of four such cruisers harrying a single unescorted ironclad to death. So there was a valid justification for the Ch 'ao, Yang Wei, and their Japanese sister Tsukushi at that time, though singly or in pairs was obviously insufficient for the task. Nor were they ever intended to be exposed for long to the fire of opponents.

But it is questionable if Naniwa and Takachiho can be included as representatives of the same type of cruiser. The only point in which they comply with the original specifications is the heavy gun armament. But this is a characteristic they shared with many cruisers built for other navies, at that time and Iater. Otherwise, they had over twice the displacement, a much heavier armament, much better protection, and conform well to the other Second Class cruisers.

The three big Japanese cruisers, Itsukushima, Matsushima, and Hashidate have nothing in common with the origins of the Elswick Cruiser, and should not be considered with that type. Actually, Japan could not afford to build ironclads to compete the Chinese ironclads, and no Japanese ship at that time carried guns sufficiently powerful to penetrate their armor. So the Japanese Navy approached Emile Bertin, the famous French designer, with the problem of acquiring the largest and most powerful gun on the smallest possible hull. The resulting ships were almost complete failures, being outrageously unbalanced. The Japanese realized this after the French built pair were delivered and they had some experience with operations. So they altered the design of Akitsushima and Chiyoda to produce reasonable and viable cruisers. To re-apply an old adage, there is no form of criticism to which the Matsushima class do not offer themselves. The faults of the design and construction and armament, save for the Armstrong 4.7-inch ( 12 cm ) QuickFirers, combined with the losses of the French designed and built Unebi and Chishima, had a great negative effect on the reputation of F rench shipbuilders.

Dr. Brooks also presented the following statement, by way of a conclusion. "W hile the Chinese could have made a more effective showing with better officers and sufficient explosive shell for their 12 -inch guns, the most important factor in deciding the battle was that the J apanese had a more modern fleet, and in consequence mounted the quick-firers which proved so effective against the unarmoured Chinese ships." This is a very all-encompassing statement, and provides the basis for additional discussion.

The first point is that F uso and Hiei dated to 1878, while all of the Chinese ships involved were products of the 1880s, although the Kuang Yi class torpedo gunboats were completed in the early 1890s, and were armed with quick-firing guns. The Japanese M atsushima type were completed in the early 1890s, but to such a poor design that they did not represent an advance or improvement over the Chinese cruisers, save for their quick-firers. Both Chiyoda and Akistushima were serviceable cruisers, but of something of a hybrid design, in an effort to obtain useful ships from French designs. Akitsushima was originally to have been of the Matsushima type, and Chiyoda was also to have carried one of the huge 32 cm guns. By far the best Japanese cruisers were the Naniwa class and the new Yoshino. The former were contemporaries of the Chinese cruisers. So on the whole, the majority J apanese ships were not newer than their Chinese opponents.

As mentioned above, the 32 cm guns on the $M$ atsushima type were completely ineffective. The three ships managed to fire a total of thirteen rounds, but scored no hits. Not so the 30.5 cm guns on the Chinese ironclads. So it seems fair to say that the actual factors which determined the course of the battle come down to the quick-firing guns, and tactics.

Quick-firing guns were not a surprise to the Chinese. As mentioned, the Kuang Yi class was armed with them. But whereas the Japanese had added 3-inch QFs to Hiei, and up-dated Fuso by replacing her slow firing 17 cm BLRs with six 6 -inch QFs, the Chinese did not take similar action. The interesting question is, why not?

The answer is basically that Admiral Ting tried to keep his ships armed with the most modern pieces. Indeed, the constructors of the German-built ships felt that the ships were under-armed, and added two or four extra and unplanned 7.5 cm field guns on naval carriages, a point often overlooked in most reference books. A ndrzej M ach points out that Ting sought to strengthen the armament of the 6 best ships, and wanted 21 K rupp 12 cm QF guns. Due to the lack of money, the plan was reduced to twelve guns to be split between the two battleships. But the B oard of Revenue rejected the request as the Empress Dowager needed the money for her Diamond Jubilee the following year.

A nother possible source was the Kiangnan Arsenal, which was building quick-firers domestically. Richard W right notes that a "4.7-inch QF gun, firing a 45 lb . [20.41 kg.] shell had been test fired in Shanghai in June 1893. A dozen or more of these guns, replacing the Peiyang fleet's 6 -inch BL guns which had a rate of fire of just 1 rpm [round per minute], would have made a significant improvement to the fleet's gunnery performance. Unfortunately the Chinese administration was too ponderous to be capable of arranging such a scheme. The best that was achieved was the late delivery of a few of the 4.7-inch QF guns directed to the additional defence of W ei-Hai-W ei."

It seems that efforts to provide the most modern guns, and even explosive shells, fell victim to the endemic graft and corruption and bureaucratic inefficiency that characterized the final years of the $M$ anchu dynasty. Thus, the Chinese relinquished the advantage of quick-firing guns to the J apanese.

Still, naval history is replete with examples of inferior forces besting a superior enemy with masterful tactics. We will never know if A dmiral Ting and his foreign advisers could have handled his fleet effectively. He was rendered unconscious by the blast effect of the first ill-conceived shots from his flagship, the Ting Yuen, toward the Yoshino, at the impossible distance of 6,000 yards (around 5500 meters), and was unavailable for the rest of the battle. Lifting a page from his background in the cavalry, he approached in line abreast, a most dis-advantageous formation. Without the guidance of Ting and his staff, the formation remained unaltered, which allowed the Japanese Flying Squadron to fall on the weak flank, while their M ain B ody "crossed the ' $T$ '" of the Chinese line.

By way of a conclusion, it seems fair to say that the Battle of the $Y$ alu was decided as much by bad tactics, perhaps inadvertent, on the part of the Chinese, as
to the quick-firing gun and rangefinder advantages of the Japanese. All were required for the Chinese to lose so decisively.


A rmament layout of the Japanese ironclad cruisers Kongo and Hiei. (B rassey, The Naval A nnual)


A rmament layout of the J apanese ironclad Fuso. (Brassey, The Naval A nnual)


The C hinese ironclad battleship Chen Yuen after the B attle. N ote the few large holes but the large number of small holes; testimony to the 'rain of fire' from the Quick Firing guns on the J apanese ships. (Wilson, Ironclads in Action)


The Chinese cruiser Chih Yuen, lost during the Battle. (W ilson, Ironclads in Action)


The Chinese ironclad battleship Ting Yuen at anchor before the W ar. (Wilson, Ironclads in Action)


The Chinese ironclad battleship Chen Yuen in action. (W ilson, Ironclads in Action)


Drawing of the Japanese cruiser Naniwa. She and her sister were in the Flying Squadron that overw helmed the Chinese right flank. (W ilson, Ironclads in Action)


The J apanese cruiser Itsukushima, one of the three ships of the M atsushima type, carrying the monstrous 32 cm gun. A s a design, they were failures, though they remained in service until after the Battle of Tsushima in 1905. (W ilson, Ironclads in Action)


The most modern of the large warships present at the $Y$ alu, the Japanese cruiser Yoshino was the Flagship of the Flying Squadron and also was the only ship in the Battle to mount the new Barr \& Stroud rangefinder. (Wilson, Ironclads in A ction)

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## MATHMETICS AND THE ANALYSIS OF NAVAL GUN PERFORMANCE AND PROJECTILES

As the opening of the popular TV show "NUMBERS" says, we use math every day. But in the study of gun performance, this was not the case. Indeed, most historians, being rather non-mathematical, merely perpetuated the errors made by previous historians, who did not have good information in the first place. But now, thanks to the power and availability of computers, mathematics can be used to analyze data and even infer solutions where information was lacking.

My research is in the area of naval gun performance and the projectiles fired. What follows is a brief explanation of how mathematics has been used to obtain very interesting results.

## 1. Naval gun performance

The basic formula used determines the "efficiency" per unit weight of the propellant charge, and is rendered simply as:

$$
\mathrm{A}=\mathrm{V}^{2} / \mathrm{B} ; \mathrm{F}=\mathrm{MA} ; \mathrm{E}=\mathrm{F} / \mathrm{W},
$$

where A - acceleration; B - the length of bore traveled; V - velocity; F - "force"; $M$ - $M$ ass of the projectile; $W$ - the weight of the charge, and $E$ - the "efficiency" per unit weight of the charge.

Obviously, to find the performance of an unknown gun, the calculated "efficiency" is then used to back into the M uzzle V elocity:

$$
F=E \cdot W ; A=F / M ; V=\sqrt{2 A \cdot B} .
$$

The accuracy of this simple formula was tested against several instances of known data, such as the performance of the A rmstrong 8"/45 Pattern S gun used to arm several cruisers of the Japanese and several South American navies. Using a $55 \mathrm{lb} .(24,95 \mathrm{~kg}$.$) charge of cordite, the M uzzle V elocity firing a 210 \mathrm{lb} .(95,26$ kg .) projectile was $2817 \mathrm{ft} / \mathrm{sec}(858,6 \mathrm{~m} / \mathrm{sec})$. With a 250 lb . shell, the MV was $2582 \mathrm{ft} / \mathrm{sec}(787 \mathrm{~m} / \mathrm{sec})$. The formula exactly duplicated the known results using either projectile weight/M V combination as the "known."

There are, of course, some practical limitations to the application of this formula. For example, the propellant should be the same in both cases, and the bore length should also be the same or very close. In other words, the comparisons should be "like" to "like" to the greatest extent possible.

This formula proved especially helpful in a recent analysis of the gunnery performance of the Italian Navy during W orld War II. The historical record shows that the Italians rarely obtained hits on their British Royal Navy opponents. The reason given is an overly large dispersion of the shells, due to the high muzzle velocity, and in some cases interference caused by the guns being mounted too close together. However, this does not seem to be completely valid, as the problem per-
sisted even when the charge weight was reduced to produce a lower muzzle velocity, though to a lesser extent.

Jack Greene and Alessandro M assignani, in their recent book The Naval W ar in the M editerranean 1940-1943, comment on the overly large manufacturing tolerance and poor quality control in the production of their projectiles. It appears that there was a $\pm 2 \%$ variance in the weight of the projectiles, and of the propelI ant charges. Could this account for the dispersion?

The "R ange Table" performance of the Italian $381 \mathrm{~mm} / 50 \mathrm{M} 1934$ gun was an 885 kg . shell fired at $870 \mathrm{~m} / \mathrm{sec}$ using a charge of $271,7 \mathrm{~kg}$. which produced a range of 44,120 meters at 350 elevation. The Table below shows the variations in range resulting from varying the shell and charge weights by $2 \%$.

| SHELL WT. | CHARGE WT. | M V | RANGE* |
| :---: | :---: | :---: | :---: |
| 885,0 | 271,7 | 870 | 44120 |
| 902,7 | 277,1 | 870 | 44520 |
| 902,7 | 271,7 | 861 | 43660 |
| 902,7 | 266,3 | 853 | 42910 |
| 867,3 | 277,1 | 887 | 45330 |
| 867,3 | 271,7 | 879 | 44570 |
| 867,3 | 266,3 | 870 | 43720 |

* R anges computed using software designed by Dr. William Jurens.

These results are probably extreme, but demonstrate that the dispersion was due in large part to the lack of uniformity of the weights. Reducing the charge weight would have had a beneficial effect, but only by reducing the size of the variation and lowering the muzzle velocity threshold.

In the same manner, the formula may be used to calculate the gun performance in cases of different propellant charge weights and/or different shell weights. For example, the Ottoman ironclad Osmanieh mounted A rmstrong 8"9-ton M uzzle Loading Rifles. The Palliser and Common projectiles weighed $81,65 \mathrm{~kg}$. But the propellant charge for the Common shell was lighter. K nowing that the M uzzle V elocity of the Palliser shell, it was possible to calculate the muzzle velocity for the Common shell.

Likewise, the A rgentine coast defense ship Patagonia mounted Armstrong 10" 27,5 -ton BLRs. The Palliser shell weighed $204,11 \mathrm{~kg}$. while the Common Pointed shell weighed $181,44 \mathrm{~kg}$. In addition, the lighter shell was fired with a lighter propellant charge. Again, knowing the muzzle velocity of the heavy shell/heavy charge combination allowed for calculation of the light shell//ight charge.

A nother interesting case deals with the accuracy of some supposedly "known" data. V irtually every published source lists the performance of the German 38 cm SK L/45 C/13 gun as firing a 750 kg . Armor Piercing Shell at $800 \mathrm{~m} / \mathrm{sec}$. M ost agree that the propellant charge was 183 kg . of RP C/12. However, there are a few sources that list the shell weight as 760 kg . and with the heavier charge to produce a MV of $890 \mathrm{~m} / \mathrm{s}$.

If the "known" information is correct, it should be verifiable by mathematical means. So by using the $28 \mathrm{~cm} \mathrm{SK} \mathrm{L} / 45 \mathrm{C} / 07$ as the basis, a reasonably accurate performance could be derived for the 38 cm gun.

| SHELL WT. | CHARGE WT. | M V | Gun |
| :---: | :---: | :---: | :---: |
| 302 | 105 | 855 | $28 \mathrm{~cm} \mathrm{SK} \mathrm{L/45}$ |
| 750 | 183 | 830 | $38 \mathrm{~cm} \mathrm{SK} \mathrm{L/45}$ |
| 760 | 183 | 825 | " |

Due to a scaling effect, verified by a comparison of the 28 cm SK L/50 C/09 and the $30,5 \mathrm{~cm} \mathrm{SK} \mathrm{L} / 50 \mathrm{C} / 08$ guns, the results are deemed accurate within a $1 \%$ margin of error, which is not a material difference.

The writer suspects that the performance of the German 38 cm , and the 35 cm guns to have been mounted on the uncompleted Mackensen class battle cruisers, stems from the use of the barrels by the A rmy and in coast defenses. It seems likely that the mountings of the railroad carriages and coast defense installations were insufficiently strong to take the full recoil, so the charge weight was reduced to compensate.

Some of the most interesting work involved an analysis of American Civil W ar artillery, both smooth bore and rifled guns for both the Union and the Confederacy. This was intriguing as while there is a weal th of data available, there is little on the actual performance of the guns, and much of that is unreliable. A nd what reliable data there is may apply for only for the explosive shell, and omit for the ball or shot of greater weight.

Calculations of the propellant efficiency, in this case black powder, indicated some interesting results. First, there was a marked difference in the three types of guns; smooth bores, muzzle loading rifles, and rifled breechloaders. There was also a direct correlation of the results for each type with the length of the bore!

For example, for the smooth bores the point of maximum efficiency occurs with a bore length of 11,9 calibers, and a distance traveled of about 9,9 calibers, allowing two calibers for the charge, wadding and ball. John A dolphus Dahlgren, Iater an Admiral and Chief of the Bureau of Ordnance, had calculated this empirically, and his 11 -inch, 10 -inch and 9 -inch guns were of that length. The propellant efficiency for both models of the 15 -inch gun, at 9,7 and 8,7 calibers, was less. Likewise, the efficiency for guns with a longer bore was also less, and the longer the bore, the lower the efficiency. In other words, there was a point of diminishing returns. Thus, a simple graph of the bore lengths on one axis, and the efficiency values on the other, allows determining the efficiency for various bore lengths.

This phenomenon was well known, and explains the short barrel length of the MLRs and early RBLs that used black powder, and later brown powder. But in brief, the rationale is that black powder ignites almost instantly, producing a single release of expanding gases. If the distance traveled in the bore is less than 9,9 calibers, then some of the energy produced by the propellant is wasted. Beyond 9,9 calibers, other factors, such as friction and air pressure, retard the speed of the projectile.

It should be noted that while this methodology would apply equally well for all of the black powder guns, the values based on US black powder differ from those used by other nations. The US powder was "hotter" than that used by the British, and the contemporary Italian Fasano powder was reputed to be "hotter" still. Thus the entire research and analysis process must be duplicated for each of
the major Powers. It is very likely that the bore length for maximum efficiency would be different for each nation. At the present time, sufficient information has been obtained for an analysis of the Russian artillery during the same time period, and the work will commence in the near future.

## 2 Analysis of naval projectiles

Exterior ballistic calculations of the trajectory of a given projectile require a fairly complete knowledge of the of it's diameter, weight, length, and form or "pointiness." From about 1920, complete information is available for almost all projectiles. However, for the period from 1860 to 1919, information is much less complete.

By way of an example of the problem, most sources that the APC fired by the 28 cm guns of the dreadnoughts in the Imperial German Navy weighed 302 kg . M ore detailed information reveals the nomenclature of 28 cm Pzgr. L/3,2 m. Bdz. u K. This projectile dated to 1911. But ballistic analysis using the software created by Dr. William Jurens revealed that the projectile in use in 1914, and the one used in 1916, was not quite the same shell. There is a material difference in the ball istic Form Factor.

This difference is substantiated by comparing the technical drawings of the $\mathrm{L} / 3,2$ APC with photographic evidence from the Battle of Jutland in 1916, and from the unloading of shells following the A rmistice in 1918, prior to the internment of the German ships at Scapa Flow. The photographs do not show the same shell. Careful measurements of the photographed APC indicate a length of 3,4 to 3,5 calibers.

The writer believes that following test firings in October 1914 by K rupp, Ionger windscreens were fitted to German projectiles, including naval projectiles, to increase the maximum range. G.V. Bull provided much information about these experimental shoots in his Paris Kanonen - the Paris Guns (Wilhelmgeschutze) and Project HARP. Other substantiation can be found in D. Schmidt-Tapken's Deutsche A rtillerie- und M inenwerfer- M unition 1914-1918. Consequently, the improved ballistic performance of the 28 cm APC was likely caused by the simple expedient of adding a longer windscreen to the nose over the Armor Piercing cap.

However, the problem of unknown projectile specifics is substantially more difficult for the last forty years of the $19^{\text {th }}$ Century. There were a bewildering number of different projectiles for the various guns. But deductive reasoning can be beneficial for organizing the data.

Fortunately, the vast majority of the naval projectiles were struck with a Caliber Radius Head (crh) of around 2,0. This will tend to limit the peculiarities to national ity and manufacturers.

So the first step is to sort the data by nationality and/or gun manufacturer.
Second, the projectiles can be sorted by type: armor piercing shot, armor piercing shell, Common shell (nose fuzed explosive projectile), and Common Pointed (base fuzed Iarge cavity explosive projectile).

A nd third, the projectiles can be sorted by time, most easily by the date of the gun.
Hopefully, there will be a sufficient number of projectiles with known characteristics to allow for comparison. There are several formulas that allow mathematical analysis. The most common is to determine a "Constant" (K):

$$
K=\left(W / D^{3}\right) / L,
$$

where $W$ is the shell weight, $D$ is the diameter, and $L$ is the shell length in calibers.
Other helpful formulas are:

$$
\mathrm{V}=\pi \mathrm{R}^{2}(\mathrm{D} / 10) \mathrm{L},
$$

where V is V olume. This will give the volume of a cylinder, but given that the nose crh is a constant, there is no proportionate difference.

$$
\rho=W / V,
$$

where $\rho$ is the Density;

$$
\mathrm{A}=\pi \mathrm{R}^{2},
$$

where $A$ is the $A$ rea.

$$
\mathrm{V}_{2}=\mathrm{AL}\left(\mathrm{D}_{2} / 10\right),
$$

where $V_{2}$ is the $V$ olume of the unknown shell, and $D_{2}$ is the bore of the unknown gun.
The length of the unknown shell ( $\mathrm{L}_{2}$ ) can be derived by two calculations:

$$
\mathrm{L}_{2}=\frac{\mathrm{W}_{2}}{\mathrm{D}_{2}^{3} \cdot \mathrm{~K}},
$$

where $W_{2}$ is the weight of the unknown shell, and $D_{2}$ is the diameter of the unknown shell. Or

$$
L_{2}=\frac{W_{2}}{\rho A} / \frac{D_{2}}{10} .
$$

And finally, an exact proportionate match for the weight of a shell for the bore of the unknown gun, to the shell of the known gun, the formula is:

$$
P=\rho V_{2}
$$

where $P$ is the Proportionate equivalent.
The formulas would yield results based on the data for a known shell. For example, the iron Palliser shell fired by the British $16,25^{\prime \prime} / 30$ BL Mk I gun was known to be 2,68 calibers in length. It is reasonable to assume that the iron Palliser shells for the other contemporary Breech L oading guns would be very similar. The results of this comparison are summarized below:

| GUN | SHELLWT., kg | LENGTH | MATCH, kg |
| :---: | :---: | :---: | :---: |
| $16,25^{\prime \prime}$ | 816,47 | 2,68 | - |
| $13,5^{\prime \prime}$ | 567,00 | 3,25 | 468,15 |
| $12^{\prime \prime}$ | 323,87 | 2,64 | 328,79 |
| $10^{\prime \prime}$ | 204,11 | 2,87 | 190,27 |
| $10^{\prime \prime}$ | 181,44 | 2,56 | 190,27 |
| $9,2^{\prime \prime}$ | 172,37 | 3,12 | 148,20 |
| $8^{\prime \prime}$ | 95,26 | 2,62 | 97,42 |

Compared to the Proportionate M atch, the shells for the $13,5^{\prime \prime}$ and $9,2^{\prime \prime}$ are substantially heavier, while the shells for the $12^{\prime \prime}$ and $8^{\prime \prime}$ are slightly lighter. This assumes, of course, that the explosive cavity of all the unknown shells is propor-
tionately the same as for the known shell. But in the absence of information, this method provides a reasonable approximation.

Cavity size will indeed have an effect on the shell length. For example, the British 12 " AP M k. I had a cavity for a $5,68 \%$ charge of black powder. It was 3,16 calibers in length. But body of the 12" APC M k. VIa, without the AP Cap, had a length of 3,0 calibers, and a cavity for a 3,08\% charge of Lyddite (Picric Acid). Lyddite is about 1,62 times denser than black powder, so the cavity of the later shell was substantially smaller.

There are several other factors that must be considered, some of which are intangible exercises of judgement:

- The type of burster charge may have an effect on the data. For example, the German 24 cm Spgr L/2,5 m. Bdz., which dates to around 1888, originally had a cavity for a $2,5 \%$ charge of black powder. It was subsequently re-filled and refuzed, the new burster being 6,04\% of Picric A cid. This resulted in a 5 kg . increase in all-up weight, with no increase in length.
- Some nations that manufactured their own shells may follow the patterns and designs of one of the major projectile manufacturers. The Swedish firm of Bofors made extensive use of K rupp designs. The Spanish Navy received much technical and design assistance from the French concerns of Schneider and Canet. Several Italian shells originated with the Skoda W orks, and others are annotated that they are of German type. Such intangible information is beneficial for selecting the "known" shell from which the comparisons are made.
- M any of the armor piercing shot used from the 1860s had a small hollow cavity. This cavity may or may not have been filled with black powder, though there was no fuze; the charge being set off by the force of impact. However, this small filler was generally not included in the nominal projectile weight.


## 3. Conclusion

In the age of armored warships, how does one rate the effectiveness of any given ship? Historically, this has been by the power of the guns that it carried. But the late $19^{\text {th }}$ century is replete with claims for the power of one gun over another, yet there was little actual combat from which to draw conclusions. Historians are operating in a vacuum of data.

To judge whether the guns of the Chilean cruiser "Esmeralda" could indeed have overawed the iron armor of contemporary battleships, the historian must know the capabilities of that gun, to calculate the exterior ballistics and determine the results of hits. But to calculate the ballistic trajectory, the performance of the gun and the essential details of the shell must be known, or as the case may be, calculated.

This Paper has demonstrated how mathematics has become the essential tool needed to make reasoned inferences of the fundamental characteristics of gun and shell. With these results, the projectile form factor can be inferred, and ballistic performance calculated. M athematics is now as important to the modern historian as any other primary source.

## RECONSTRUCTING THE 120-MM GUNS FOR THE DESTROYER OQUENDO

In 1959, the Spanish Government decreed that the main caliber guns for the Oquendo class destroyers then under construction, to be $120-\mathrm{mm}$ guns in the new NG-53 mountings. In 1959-61 workshops in San Carlos produced 10 mountings of the specified type (three for each destroyer and one for coast testing), which proved not up to the specifications. So in 1962 they decided on the first great modification, to solve problems of the mounting. As a result, the Oquendo was fitted with only two mounting of this type, which were not used again in the Spanish Fleet. The other destroyers of the Oquendo class received six A merican mountings, Mk-32, derived from the well proven Mk-12 of WW 2.

During the research for the monograph about destroyers Oquendo Class, the author discovered that accurate information on the main caliber guns was extremely limited. For example, J.L. Coello's informative book, the main caliber of Oquendo armament is given as only a modification of the gun applied earlier on Canarias and Méndez Núñez, the $120-\mathrm{mm}$ guns of system V ickers-A rmstrong M k F. The basic difference made was to increase the length of a barrel from 45 to 50 calibers, which improved ballistic properties a little. In the same source it is stated that the Spaniards managed to obtain a muzzle velocity of $900 \mathrm{~m} / \mathrm{s}$ with a new charge. Changing to the old propellant and charge as used in the destroyers of Churruca class reduced the muzzle velocity to $875 \mathrm{~m} / \mathrm{s}$.

W ith the use of modern computer software, it is possible to estimate the data for the 50 caliber gun from the information which is given in such a veiled form. For the analysis, the program "Strelets", developed under direction of Dr. N.M. Rusanov of the "Rifle arms" faculty of Izhevsk State Technical Institute has been chosen. The baseline data on the ballistics of the Vickers-A rmstrong M k F is taken from the directory by Campbell:

| Length bore | 5399.5 mm |
| :--- | :--- |
| Chamber volume | $10.32 \mathrm{dm}^{3}$ |
| W eight projectile | 22.0 kg |
| Propellant charge | $6.5 \mathrm{~kg}\left(\mathrm{CSP}_{2}\right)$ |
| M uzzle velocity | $853 \mathrm{~m} / \mathrm{s}$ |
| W orking pressure | $3150 \mathrm{~kg} / \mathrm{cm}^{2}$ |

From this initial data, it is possible to achieve compatibility of data from Campbell, then the increase in length of the barrel by 5 calibers has been made, muzzle velocity thus has reached a value of $886 \mathrm{~m} / \mathrm{s}$.

On the one hand, the divergence with experimental data is only $1 \%$ (886 or $875 \mathrm{~m} / \mathrm{s}$ ), i.e. normal engineering accuracy, but on the other, an increase of velocity from lengthening the barrel, of 22 or $33 \mathrm{~m} / \mathrm{s}$, is essential enough. From here it is possible to draw the conclusion that, apparently the Spaniards were not limited to
simple increase in length of a barrel, and have undertaken serious enough modernization of the gun.

This conclusion was confirmed during the preparation of the monograph, owing to support of Spanish colleague, Capitán de Fragata (Ret) A ntonio G. Erce Lizarraga, who provided a detailed enough description of the given guns [Ref. 4].

As acknowledgement of our conclusions, the material was really and extensively redesigned. The most important difference consisted in application, for manufacturing a barrel, steel of higher durability. It has enabled at practically same thickness of the barrel to make replaceable (loose) liner. B efore, the exhausted barrel was subject to full replacement. A lso the static part underwent a modernization; primarily it concerned a semi-automatic breech mechanism. In a manual mode it functioned completely identical to the M k F.

The characteristics of the gun were: 36 grooves (the M k E, roughly contemporary to the Mk F, had 28 grooves), pitched for one rotation in 30 cal.; length of recoil - 500 mm , weight of liner 922 kg , weight of a shell of 22 kg , weight of complete round 36 kg , including weight of propellant charge -6.25 kg , muzzle velocity of $900 \mathrm{~m} / \mathrm{s}$, the maximal pressure of $3150 \mathrm{~kg} / \mathrm{sm}^{2}$, the maximum range of 21,240 meters. However, by order on the M inistry on January 8th, 1953, ammunition of the ships of the Spanish fleet unified was standardized. The standard propellant was to be $\mathrm{CSP}_{2}$ made in charges 6.5 kg , but because of its inferior ballistic properties, the muzzle velocity fell to $875 \mathrm{~m} / \mathrm{s}$.


Producing of Oquendo's guns


120 mm guns on cruiser $M$ endez $N$ unez

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## THE BRITISH - ITALIAN PERFORMANCE IN THE MEDITERRANEAN FROM THE ARTILLERY PERSPECTIVE

During the Second W orld W ar, the course of the naval conflict in the M editerranean can be reduced to battles between the British and Italian fleets. Three years of operations against the Royal Navy only produced one more or less significant victory for the Italians, who enjoyed a considerable numerical superiority in this, their main theatre of operations, while the priority for Britain was minor or even third-hand! A nd most of the engagements, as a rule, ended with the Italian forces retiring as fast as possible.

M arc A ntonio Bragadin's The Italian Navy in World War II is bewildering. Their 'greatest' victory was Pantellaria, in which a British destroyer and several transports were sunk. But given the correlation of the forces involved, the entire convoy should have been exterminated to the last vessel! A nd the 'super fast' Italian ships never could catch the much slower British vessels; Bartilomeo Colleoni, supposedly capable of 40 kts., was savaged by H.M .A.S. Sydney, which on her best day only made 32 kts .

How could it be that, having the larger fleet, magnificent artillery and welltrained crews, the Italian Fleet suffered one shattering defeat after another? Let us try to look at the problem through the prism of naval guns.

For the purposes of comparison, we shall select three artillery systems that were nearly analogous between the two navies: the $381-\mathrm{mm}\left(15^{\prime \prime}\right)$ main guns of the battleships, 203-mm ( $8^{\prime \prime}$ ) guns of the heavy cruisers, and the $152-\mathrm{mm}\left(6^{\prime \prime}\right)$ of the light cruisers. The performance of each is summarized below.

| Caliber | M odel | Shell's mass, <br> kg | M uzzle <br> velocity, $\mathrm{m} / \mathrm{s}$ | Form factor to <br> the low of <br> 1943 |
| :--- | :---: | :---: | :---: | :---: |
| $152 / 50$ | M k X X III | 50,8 | 841 | 1,08 |
| $203 / 50$ | M k V III | 116,1 | 855 | 1,03 |
| $381 / 42$ | M $~$ | 871,0 | 752 | 1,27 |
| $152 / 53$ | M odel 1926 | 47,5 | 1000 | 1,09 |
| $203 / 53$ | M odel 1927 | 125,3 | 955 | 1,09 |
| $381 / 50$ | M odel 1934 | 885,0 | 850 | 0,89 |

The technique and functions for ballistic calculations was presented in sufficient Detail in the pages of "Warship International" in an article by William Jurens. M any of the functions are of an empirical character, and so differ a little bit for each country. So in Russia the definitions of a standard atmosphere were set forth in the Russian State Standard 4401-78, which defined the character of temperature variations, density, viscosity, and air pressure at altitude functions. These are the functions used for this analysis. A nd for the laws of resistance the following were applied:

- Law resistance of Siacci (for shells of a form similar to the standard Type 1)
- The Law of 1930 (similar to a Type 8)
- The Law of 1943 (similar to a Type 7)

In this case for definition of the form factor of a shell, the Law of 1943 was selected. From the Table above, it is evident that the British and Italians have used shells with almost identical ballistic properties. However, here there is nothing exotic, as the British influence on Italian ordnance was very great. Up to the end of WW 1, the guns of the Italian fleet were made under license to designs from the firms of A rmstrong [EOC] and Vickers. A nd as a matter of fact, subsequent gun development were modern versions of those designs. This connection, by the way, shows rather exponential comparison of the form factors for shells of the main guns of the leading maritime states. For example, for guns of about $127-\mathrm{mm}$ ( 5 ") which were introduced into the inventories during the $1920-30$ s, as the main guns for destroyers, the values are as follows (using the Law of Siacci):

| System | State | M uzzle <br> velocity <br> m/s | Shell's <br> mass, <br> kg | Range for <br> angle, m | Form factor to <br> the Siacci's <br> low |
| :--- | :--- | :--- | :--- | :--- | :---: |
| $120 / 45$ M k I, M k II | England | 814 | 22,70 | $14450(30)$ | 0,82 |
| $130 / 40$ M odel 1924 | France | 725 | 34,85 | $18700(35)$ | 0,60 |
| $127 / 45$ SK C/34 | Germany | 830 | 28,00 | $17400(30)$ | 0,66 |
| $120 / 50$ M odel 1926 | Italy | 950 | 23,15 | $22000(45)$ | 0,62 |
| $120 / 45$ Type 3 | Japan | 825 | 20,41 | $16000(33)$ | 0,66 |
| $130 / 50$ B 13 | USSR | 870 | 33,40 | $25730(45)$ | 0,52 |
| $127 / 38$ M k 12 | USA | 762 | 25,04 | $15300(35)$ | 0,73 |

From the above table, taken from Tony DiGiulan's contributions to the W arships1 website (www.warships1.com), the ballistics of guns of the main European states and Japan were at approximately the same level. It is interesting to note, however, that the Soviet shell had the best ballistic form. But this should not be surprising, as the attention given to ballistics in the USSR, which resulted in the M. 1928 pattern projectiles, is well known now. Stalin even took a personal interest in the development program, which produced gun systems equal or superior to all foreign designs in all main parameters save one - barrel life. This unfortunately cancelled out all of their virtues, as the Effective Full Charge life of the gun was equal to the capacity of the magazine!

The A merican and British guns have the worst ballistics form, but this can not be the only criterion, since doctrine required the more universal application of both anti-surface and anti-air capabilities.

But to return to the Anglo-Italian conflict in the Mediterranean, it is well known that the hit probability is determined in Iarge part by the angle in descent of a shell, known as the Danger Space. Steve M cL aughlin defined this relationship as:

## Danger space $=$ Target width + Target height $/$ Tangent of A ngel of Descent

It follows, therefore, that the lower this angle of descent, the greater the hit probability, which is rationale behind the use of high velocity guns. Figure 1 re-
flects this parameter of the major British and Italian guns. Hereinafter the various graphs show 152 mm guns as circles, 203 mm guns as squares, and 381 mm guns as diamonds, with white designating the British and black the Italians.

As is depicted in Figure 1, at all battle ranges the angle of descent of the Italian shells is less than that of their British opposite number. Indeed, at ranges up to 16,000 meters, the angle of descent of the Italian 203 mm shell is less than that of the British 381mm!


Fig. 1. Comparison of angle of incidences of shells
If comparison were only limited to the size of the danger space, than the Italians should have enjoyed a considerable advantage. This makes the results of the gun battles quite paradoxical. Therefore, as a second step we must try to estimate the values of the ballistic corrections. A technique for obtaining such values would be to determine the effect of corrections in an elevation angle: the variation of an elevation angle is applied, which affects the range. Thus, for each degree of deviation either way, the shell either falls short or flies over by a certain number of meters. Other corrections produce a similar result. The unique exception is a variation of the atmospheric density and pressure, the values of which are generally included in the Range Tables. The given technique was approved by the authors on the basis of Range Tables for the 122 mm Soviet howitzer, model 1938, and has given satisfactory convergence.

1) Correction of elevation angle - sensitivity of the gun the roll of the ship (see Figure 2). Though Fire Control Suites were common before the W ar, the very sensitive instruments that appeared only afterwards had effect as if the ship were on an even keel, the consequences of roll being eliminated insofar as the guns were concerned. But in the absence of such systems, the divergence betw een the British and Italian guns is most obvious in the performance of the 381mm guns. Dispersion of the Italian shells was almost $1.5-2$ times greater! This means that in the
presence of virtually any wave activity at sea (which is almost always), the British would have on average twice as many hits as would the Italians!


Fig. 2. The correction on an elevation angle
2) Correction for the mass of the shell - sensitivity of the gun to the 'knowhow' of shells (see Figure 3). As is known, the more developed manufacturing processes warrant obtaining smaller tolerances. Thus, dispersion due to variation of the mass of the shell is lower, as the shells are more uniform. However, as Jack Greene and A lessandro M assignani have pointed out in their The Naval War in the M editerranean 1940-1943, manufacturing tolerances in the production of the Italian shells were overly large on the one hand, as was the weight control of the propellant used in bagged charges.

The Table below shows the changes in range caused by a mere $1 \%$ variance in shell weight and propellant charge weight.

| Condition | Shell Wt. (kg.) | M V (m/s) | Range @ 15-deg (meters) |
| :--- | :---: | :---: | :---: |
| Range Table | 885 | 870 | 26,420 |
| $1 \%$ increase in charge | 885 | 874.34 | 26,640 |
| $1 \%$ decrease in charge | 885 | 865.64 | 26,201 |
| 1\% increase in shell wt. | 893.85 | 865.68 | 26,289 |
| $1 \%$ decrease in shell wt. | 876.15 | 874.38 | 26,552 |
| $1 \%$ increase in both | 893.85 | 870 | 26,507 |
| $1 \%$ decrease in both | 876.15 | 870 | 26,332 |
|  <br> $1 \%$ decrease in shell wt. | 876.15 | 878.74 | 26,772 |
|  <br> $1 \%$ increase in shell wt. | 893.85 | 861.34 | 26,070 |

So even though it may have been possible for the Italians to have adjusted for the variations in shell weight, which were often labeled on the projectile and allowed for in the Range Tables, the variation in the propellant charges could not. Thus the Italians were laboring under an additional burden with regard to dispersion.
3) Correction for atmospheric pressure (see Figure 4). In this area, the change in condition would affect both sides, with neither obtaining a material advantage. Thus, the value of this correction is not so great, as atmospheric pressure varies rather slowly, which allows for its rather exact measure.


Fig. 3a. The correction on a mass for 152 -mm shells


Fig. 3b. The correction on a mass for $203-\mathrm{mm}$ shells


Fig. 3c. The correction on a mass for 381-mm shells


Fig. 4. The correction on atmospheric pressure
4) The correction for atmospheric density actually displays sensitivity of the gun to meteorological conditions, as the presence of rain or snow results in increased density of the air (see Figure 5). This correction, as opposed to atmospheric pressure, is rather difficult to take into account. Sudden rain or snow showers (the latter not common in the M editerranean), or fog, would have a detrimental effect on ballistic performance. B ut in this regard, the opponents approximately correspond to each other, with neither obtaining an advantage.
5) Corrections in initial [muzzle] velocity caused by variations in the condition of the charges (see Figure 6). These include charge temperature. Within a range of tolerance, accounted for in the Range Tables, a higher temperature would result in a higher initial velocity, and a lower temperature a lower velocity. Other factors are not so predictable. The very conditions of storage can negatively effect
the charges, and could result in a breakdown of the chemical components, while excess moisture would reduce burning efficiency. It is the opinion of the authors that the Italians had a slight advantage in this area.


Fig. 5. A correction for air density


Fig. 6. The correction on initial velocity


British ships under Italian fire
On the face of it, the British Royal Navy have an advantage over the Italians in only one area of correction, but it is the most important and significant. W hat does this mean? In the theoretical sense, the smaller danger space of the lower velocity British guns would imply that only the most careful preparations and calcuIations would counter the Italian advantage in hit probability. However, the ballistic effects of roll are less for the British than for the Italians, and therefore correspondingly easier to correct for. The worse the sea state, the greater the British advantage in this regard. It is interesting that, empirically, the Italian gunnery performance should have improved as a result of their reducing the muzzle velocity of their guns. The effect would have been to decrease the danger space on the one hand, but to enjoy a corresponding decrease in the dispersion caused by the roll of the ship on the other.

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## AN ESTIMATION OF THE PNEUMATIC GUN'S EFFECTIVENESS

At the end of 19th century, the armies and navies of several nations were experimenting with some systems of the pneumatic guns, which launched projectiles filled with dynamite. But the information about these guns contains many discrepancies, though the weapon's effectiveness was questioned. For example, Schroeder, writing in 1894 [see Bibliography], doubted the effectiveness for a number of subjective reasons. But $W$ atson, writing in 1991, cites objective reasons for the weapon's failure. In an effort to arrive at an objective scientific conclusion, a simulation model program was created.

## 1. Describing of the model

The model consists of two components: internal and external ballistics. The first part is the gas-dynamic task. Its calculation scheme is the interplay of two fundamental components; the volume of the compressed air tank, and the volume of the chamber of the gun. The latter will increase as the projectile is propelled down the gun tube towards the muzzle. A simple schematic of gun's pneumaticsystem is shown in the Fig.1.


Fig. 1. The principal gun's pneuma-schematic: 1 - collector; 2 - compressor's drive; 3 - compressor; 4 - return valve; 5 - gas-reservoir; 6 - main valve; 7 - gun tube

The gas's outflow $G$ from high-pressure balloon is over-critical only:

$$
G=p_{1} F_{k} \sqrt{\frac{k}{R T}\left(\frac{2}{k+1}\right)^{\frac{k+1}{k-1}}},
$$

where $p_{1}$ - gas pressure in tank; $F_{k}$ - the critical section of the main valve; $k$ - the adiabatic index of the air; RT - the "powder's power", on this case power of the compressed air.

The gas pressure gives the acceleration to projectile during the travel through the gun tube, which at the muzzle yields the initial, or muzzle, velocity. That movement in the tube is the parameter of the interior ballistics component..

The mathematical model of this first component is contained in two differential equation: the equations of the law of the impulse preservation for the projectile in gun tube, and the equation of indissoluble (Law of Lomonosov - Low of the matter preservation) for the gas in the tank.

$$
\begin{gathered}
\frac{d m_{b}}{d t}=-G \\
\frac{d v}{d t}=\frac{\left(p_{2}-p_{h}\right) F}{m}-g(\sin \alpha-f \cos \alpha) ;
\end{gathered}
$$

where $m_{b}$ - the mass of gas in the tank; $v$ - the projectile velocity; $m$ - the projectile mass; $p_{2}$ - the air pressure in gun tube; $p_{h}$ - the air pressure of the atmosphere; F - frontal area of projectile; g - gravity [9.81 m/s squared]; f - the index of friction (projectile and gun tube).

To this equation is added some algebraic equations:

$$
\begin{gathered}
\mathrm{p}_{1}=\frac{m_{b} R T}{V_{b}}, \\
\mathrm{p}_{2}=\frac{\left(m_{0}+\Delta m\right) R T}{V_{g}}, \\
V_{g}=F \int v d t .
\end{gathered}
$$

$V_{b}$ - the volume of the air tank; $V_{g}$ - the internal volume of the gun tube; $m_{0}$ the initial mass of the air in the gun tube; $\Delta \mathrm{m}$ - the mass of the air released from the tank.

The equations of the second component of the mathematical model are very trivial, and are in every manual of exterior ballistics. The A.A. Dmitrievsky edition, for example, presents four differential equations and some algebraic equations to solve the exterior ballistics problem.

So, the model is complete and mathematically valid, only needing initial data for calculations. A nd for this, Patrick M cSherry provided the research.

The initial pressure in the compressed air tank was about 70.5 atm . B ut the information about tank's volume is very interesting. Seaton Shroeder, the first commander of cruiser V esuvius, which mounted three 381-mm [15-in] pneumatic guns, wrote: the "volume of tank is 276 sq feet" $\left(7.83 \mathrm{~m}^{3}\right)$. B ut in his book, Shroeder wrote: "It's interesting, but the mass of the air in the tank is about three tons - this is result of displacement augmentation... before and after filling the tank".

If the condition of gas is normal (temperature about 300 K ), the equation of $M$ endeleev-K lapeiron gives the tank a volume of $48 \mathrm{~m}^{3}$. So, every gun had two tanks. It seems logical; one tank plumbed for the firing of the gun - the 'propellant charge' as it were -- and the second is connected to the compressor.

The interior ballistics component gave some interesting results (Fig. 2). Curves 1 and 2 show the normal changes of acceleration in the ordinary firing guns. If the velocity of combustion of the propellant is decreased, say by increasing the propellant powder grain size or form, the point of maximum acceleration occurs later and will be lower. Thus the difference between curve 1 and curve 2. B ut it turned out that the interior ballistics of pneumatic guns is very different!

Writing in 1993, M.C. W est asserts that the air pressure in gun tube remains constant, and as a result of this, the acceleration is increased constantly for the length of
the gun tube (curve 3b). But this is mistake! The assumption behind 3 b can only be valid for a very great tank volume, and a large aperture diameter of main valve, providing a continuous flow of compressed air, which is not the case. Really, this is asymptotic assumption, and the more valid assumption is better reflected by curve 3 a. It is similar to the curve for slow-burning powder. The maximum of pressure will be strongly pronounced, because the time the valve is open is small, anti-pressure is small too, and the consumption of compressed air is great. But with time, the antipressure will increase, and the compressed air consumption will decrease as the supply in the small tank used for 'firing' the gun is expended and the valve closed. So, if we have the extreme of pressure, then we also have the extreme of acceleration. From the point in time, represented by live $T_{3}$, the valve is closed and no more compressed air enters the gun tube, so the force continuing to push the projectile is from the expansion of compressed gasses that is similar adiabatic law.


Fig 2. Projectile acceleration in the gun
The form of projectiles is very difficult to quantify. Theoretical determination of resistance law is very hard, as it had a very non-standard shape and inordinate length, so the existing methods for the determination of the form factor seem inapplicable. But, according to Shroeder, the projectile had a form factor using the M ayevskiy law of about 5.646. For the air resistance for the external ballistic component of the model, the superior Siacci law was used. So the form factor using Siacci law is about 5.06. The atmospheric condition used was the "Standard Atmosphere" (See GOST 4401-81).

## 2. Thedisaussion of results

One of the complex criteria for estimating a projectile's ballistic characteristics can be served by the thickness of armour that a hypothetical AP shell can perforate. A s can be seen in the graph (fig. 3), the curve for a Zalinsky-type projectile is "non-standard." For traditional artillery, armour penetration decreases as the distance increase. But for the pneumatic gun penetration increases. The "sawtooth" character of the curve for the Zalinsky projectiles is due to the necessity of using lighter projectiles to obtain Ionger ranges, see Tables below. Vesuvius used tables to estimate the maximum range for each weight of shell. The fixed elevation, coupled with the necessity to use lighter shells for longer ranges, effectively limits attack on armour to a small zone at the maximum range for each weight of projec-
tile, reflected in Fig. 3 as the points in the "sawtooth" curve. Thus, unlike traditional artillery projectiles which would have an effect at any point along the trajectory, for the pneumatic shell, attack on armour would be limited to a few spots at range. At the usual combat range of about $2 \ldots . .3 \mathrm{kms}$, the effect on armour of a pneumatic shell is commensurable with shells M k III (102/40) and M k II (127/40) guns of the American fleet. Though this comparison, certainly, is speculative sense, as the high-explosive effect of the dynamite shell, in any case, would be more damaging than ordinary armour penetration.


Fig. 3. Comparative perforate armour of the $127-\mathrm{mm}$,
$102-\mathrm{mm}$ shells and hypothetical armour piercing shell of a pneumatic gun
The simulation model revealed a "draw-down" effect in the pneumatic system, caused by continuous use. Bearing in mind that the main compressed air storage tank had to service three of the pneumatic guns, a decline of air pressure was inevitable, with a negative effect on shooting to range. This is best illustrated by simplifying the process to a single gun, shooting 200-pound [weight of explosive; 500 lb projectile weight] shell. For the first shot (muzzle velocity $204 \mathrm{~m} / \mathrm{s}$, the range 1880 m ) pressure in the tank falls to 68.08 atm . So at the second shot and further these parameters are following:

| 2-nd | 68.02 atm | $198 \mathrm{~m} / \mathrm{s}$ | 1780 m |
| :--- | :--- | :--- | :--- |
| 3-rd | 65.73 atm | $194 \mathrm{~m} / \mathrm{s}$ | 1700 m |
| 4-th | 63.55 atm | $188 \mathrm{~m} / \mathrm{s}$ | 1600 m |
| 5-th | 61.50 atm | $185 \mathrm{~m} / \mathrm{s}$ | 1550 m |
| 6-th | 59.52 atm | $180 \mathrm{~m} / \mathrm{s}$ | 1470 m. |

Thus, without recharging, the sixth shot range falls about a quarter. By the way, Shroeder tried to estimate fall of pressure after the first shot, using the law

Boil-M ariott; increase of gas volume he has estimated as: $0.08 \mathrm{~m}^{3}$ - the volume of various internal cavities and $1.40 \mathrm{~m}^{3}-3 / 4$ volumes of the gun. Thus, there was the $59 \mathrm{~atm}[70.5-7.8 /(7.8+0.08+1.4)=59 \mathrm{~atm}]$ remaining.

The simulation model also allows an estimate of the tolerance in operation of the valve. As has shown testing, the time of valve open-shut operation is ideally 0.2 sec . It is interesting that if the tolerance of operation is off by 0.001 sec , the change of range is about 10 m , plus or minus. For engineering of that time such of the tolerance was very good, but for the grouping of shots it was obviously unsatisfactory. In this connection, the mediosquare deviation of shells was almost in some tens greater than traditional guns. By the results of M ay 1891 firing trials, intended to calibrate a single projectile weight, three shells were fired. The second landed about 50 yards short of the first, and the third about 50 yards over. So the probability of hitting a target was low.


Fig. 4. Dynamite gun of auxiliary cruiser Nicheroy
And finally, probably most essential shortcoming as a naval weapon, as mounted in Vesuvius, is its lack of range. In the literature there is no information on the maximum range, but most likely it was no more than 3 kms . The usual combat distance at the time was about a mile. Besides, because of its low velocity, the shell was rather a long time in flight. The simulation model gives the following interesting results for an estimation flying time:

Range, m. $\begin{array}{llll}700 & 1000 & 1400\end{array}$
$\begin{array}{llll}\text { Time, sec. } & 6.4 & 7.7 & 9.2\end{array}$

At such flight times, the target not only could to see a shell, but depart!
A unique way to radically increase muzzle velocity was to increase of pressure in entire system. A ccording to A. Y akimovich, in a folder there were items of information that there was design development of a pneumatic gun with pressure of compressed air about 350 atm . But if the tolerance of the valve operation of this gun also was 0.001 sec , than the change of range turns out 40 m ! From here it is clear why that the gun design was not pursued farther than the drawings.

A lso there is information that ostensibly "the experiments with 600-pound (272kg ) dynamite charges" were carried out. In this case the shell weighed 680 kg ( 1500 pound) and had length 2.1 m ( 7 feet). In the literature there is no information on its range, it is underlined only, that it was less than mile. The simulation model demonstrates why a shell of this type was not used. In a gun it could be launched only up to a velocity of about $100 \mathrm{~m} / \mathrm{s}$, and thus, the range would be hardly 500 m . At such range the firing ship itself could be damaged from the explosion of the shell!

The developed simulation model allows us to estimate the various factors of combat efficiency of pneumatic guns, that, for example, was made by the author in work for $267-\mathrm{mm}$ of the pneumatic gun of the B razilian cruiser Nictheroy. The basic data on this system are taken from A. Saks work, and applied to the 381-mm gun of the cruiser Vesuvius.

The comparative characteristics of the dynamite guns

| System | 203-mm | 267-mm |  | 381-mm of cruiser "V ezuvius" |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Length of tube, m/ feet | 18/60 | 16,47 / 54 |  | 16,47 / 54 |  |  |  |
| Pressure, ath. | 70.5 | 70.5 |  | 70.5 |  |  |  |
| M ass of explosive, kg pound | $\begin{array}{\|l} \hline 45.3 \\ 100 \\ \hline \end{array}$ | $\begin{array}{\|l} \hline 91 \\ 200 \\ \hline \end{array}$ | $\begin{array}{\|l\|l} \hline 22.6 \\ 50 \\ \hline \end{array}$ | $\begin{aligned} & 227 \\ & 500 \end{aligned}$ | $\begin{aligned} & 159 \\ & 350 \\ & \hline \end{aligned}$ | $\begin{array}{\|l\|} \hline 91 \\ 200 \end{array}$ | $\begin{array}{\|l\|} \hline 45 \\ 100 \\ \hline \end{array}$ |
| M ass of shell, kg pound | $\begin{array}{\|l\|} \hline 62 \\ 137 \\ \hline \end{array}$ | $\begin{aligned} & 158 \\ & 348 \\ & \hline \end{aligned}$ | $\begin{array}{\|l\|} \hline 91 \\ 200^{* *} \\ \hline \end{array}$ | $\begin{aligned} & \hline 445 \\ & 980^{* *} \end{aligned}$ | $\begin{array}{\|l\|} \hline 350 \\ 780^{* *} \\ \hline \end{array}$ | $\begin{aligned} & 227 \\ & 500 \\ & \hline \end{aligned}$ | $\begin{array}{\|l\|} \hline 130 \\ 285 * * \\ \hline \end{array}$ |
| Shell's kaliber, mm | 203 | 267 | 267 | 381 | 381 | 381 | 381 |
| M uzzle velocity, m/s | 230* | 160* | 230* | 130* | 150* | 200 | 290* |
| Range, m | 2100* | 1200* | 2100* | 760* | 1100* | 1900 | 3000* |


| System | 381-mm coastal gun |  |  |  |  | 381-mm |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Length of tube, m / feet | 15 / 50 |  |  |  |  | 15 / 50 |
| Pressure, ath. | 140 |  |  |  |  | 350 |
| M ass of explosive, kg pound | $\begin{array}{\|l\|} \hline 227 \\ 500 \\ \hline \end{array}$ | $\begin{array}{\|l\|} \hline 181 \\ 400 \\ \hline \end{array}$ | $\begin{aligned} & 136 \\ & 300 \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 91 \\ & 200 \\ & \hline \end{aligned}$ | $\begin{array}{\|l\|} \hline 45 \\ 100 \\ \hline \end{array}$ | $\begin{array}{\|l\|} \hline 91 \\ 200 \\ \hline \end{array}$ |
| M ass of shell, kg pound | $\begin{array}{\|l} \hline 448 \\ 990 \\ \hline \end{array}$ | $\begin{array}{\|l} 390 \\ 860 \\ \hline \end{array}$ | $\begin{array}{\|l\|} \hline 330 \\ 728 \\ \hline \end{array}$ | $\begin{aligned} & 252 \\ & 558 \\ & \hline \end{aligned}$ | $\begin{array}{\|l\|} \hline 195 \\ 430 \\ \hline \end{array}$ | $\begin{aligned} & 227 \\ & 500 \\ & \hline \end{aligned}$ |
| Shell's kaliber, mm | 381 | 381 | 381 | 381 | 381 | 381 |
| M uzzle velocity, m/s | 210* | 230* | 260* | 300* | 350* | 520* |
| Range, m | 1900* | 2100* | 2400* | 3000* | 3200* | 4500* |

Note: * - account; ;* - is chosen in a proportion to the nearest anal ogue. Pneumoautomatics for all guns is taken, as for guns Vezuvius. The eminence angle of guns in all cases is $18^{\circ}$.


Fig. 5. Shell for dynamite gun
A lso results of accounts for 381-mm of the coastal gun is interestingly. W ork by V.G. M alikov contains the information, that the $227-\mathrm{kg}$ shell flayed on range 1800 m (calculated data has given similar figure - see table), whereas the 51-kg shell on 5000 m . This last, however, appears exaggerated.

## Condusion

The history of creation and combat using of pneumatic artillery is very instructive. All its defects are objective, and caused by the low level of technical development of 19th century. But with our modern technology, the idea of pneumatic guns is very attractive. There are some advantages over traditional firing guns: noiseless, the ability to fire a shot in the every condition (even from under water!). A nd such a weapon would be useful in, say, anti-terrorists action.

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## TWO UNUSUAL WEAPONSIN EARLY SUBMARINES

During performance of scientific work "M odeling Gas-mechanical Systems" (RU State registration 0198002046) there was a question on the characteristics of large caliber pneumatic artillery systems created by Polish engineer Zalinsky for launching shells filled with dynamite. At the end of 19th century a number of these systems had been accepted to arm ships and coastal defense of the United States and Brazil, with the cruiser Nictheroy. A more detailed examination of their performance was considered in our earlier works [see Bibliography]. Subsequent research, how ever, revealed information on the acceptance of pneumatic artillery to arm submarines, specifically A merican U.S.S. Holland (SS-1) and Peruvian vessel built by F. Blum, the El Toro.

From the archival sources, the basic armament of John Holland's submarine consisted of a normal torpedo launching apparatus, and a 203 -mm dynamite gun! In the official reports concerning the early period of service confirm this, referring to the weapon as "the air torpedo." However, during the extensive period of trials and tests during 1898-99, "the apparatus for launching of air torpedoes" was dismantled. Unfortunately, no one kept any reports on its trials, so it is possible to judge the device only approximately. The "apparatus" was mounted in a "trainable" compartment, which was trained for shooting from below. And most likely, it represented an update of the pneumatic gun, intended to launch its projectiles into the bottom of a floating ship.

The pneumatic gun as designed by Holland represented a considerable modernization of Zalinsky's design. For this device, Holland received the patent No. 708552 [see fig. 1]. But as soon as it was tested submerged, the complete hopelessness of pneumatic artillery under water became clear. Nevertheless, Holland continued with the submarine a gun of his design. The government gave up all interest in the idea, now completely discredited, and for the entire term of service of SS-1, the gun was just unnecessary ballast!

The real caliber of the gun was $214 \mathrm{~mm}\left(8,4255^{\prime \prime}\right)$, and it was installed in the boat with a fixed el evation of 15 deg. Small changes in elevation could be made by changing the trim of a boat, but a more serious problem was the charge of compressed air for the gun. The projectile weighed $100 \mathrm{~kg}(222 \mathrm{lbs})$, with a pyroxiline charge of 23 to 36 kg ( 50 to 80 lbs ). Holland's estimates of performance were 900 m (1000 yards) from the surface position, but shooting submerged only about 25 m (30 yards). Magazines capacity was six shells, but if necessary additional shells could be located in the boat. It is necessary to note the important improvement of Holland's gun: it could shoot using either compressed air or a small charge of gunpowder!

In his official report to Captain Frederick Rogers, Lieutenant Nathan Sargent wrote on M arch, 28th 1899: "the forward pneumatic gun has been tested only on compressed air as powder charges have not arrived yet. The wooden shell charged in it in length of three feet and calibre eight and a half of inches was fired by pres-
sure $600 \mathrm{lbs} / \mathrm{sq}$ in (40 atm). The shell has fired to four hundred yards without any deviation in line of sight."

No. 708,552.
Patented Sept. 9, 1902.
J. P. HOLLAND.

SUBMARINE OR OTHER GUN.
(Ma Model.)


Fig. 1. The Plan from the Patent of Pneumatic Gun of Holland
For analyzing this found information, the author used the computer program "Pnevmobal" for the internal ballistics, which was structurally integrated into a
package of external ballistic calculation programs known as "A rtillery v 2.0." Earlier this package had been applied to the analysis of data on the pneumatic artillery of fleet and coastal defense.

The lead calculations have shown, that at pressure 40 atm . the $100-\mathrm{kg}$ shell can be launched from the tube at a velocity of $90 \mathrm{~m} / \mathrm{s}(295 \mathrm{ft} / \mathrm{sec})$, which really produces a range up to 360 m (393 yards), matching well with N. Sargent's official report. However, assuming that the pressure in cylinders was 136 atm, as intended by Holland, then the same shell would have an initial velocity of $170 \mathrm{~m} / \mathrm{s}(557$ $\mathrm{ft} / \mathrm{sec}$ ) and carry to a range of 1200 meters (1312 yards), a bit more than calculated by Holland. These results have incontestably cast doubt on the idea of the installation of pneumatic artillery on submarines as viable weapons.


Fig. 2. U.S.S. Holland (SS-1) and her dynamite gun
As for the El Toro, these results do not apply. She was constructed for operations against Chile in a mode of strict secrecy, which has severely limited the volume of the documentation. A nd even that little archival information about her has been irretrievably been lost. In this connection, for example, the majority of directories on submarines omit her entirely, while the others provide extremely inconsistent data.

Research with attention to the archival Peruvian sources, generalized in a previous article, has unequivocally shown that the basic armament of the boat was made up of four "torpedoes" of system Ley, each containing 10 pounds of dynamite. Possibly, this information on the explosive filler formed the basis of the claim that she had been armed with pneumatic/dynamite gun, almost two decades
prior to the submarine Holland. A ctually each of these "torpedoes" had a normal "timed fuze," so El Toro, having passed near the keel of the target ship, merely released the weapon [see Fig. 3].


Fig. 3. The plan of fastening of Ley's torpedos (F. Blum's sketch)
Having positive buoyancy, the torpedo - actually more of a floating mine surfaced, hopefully very near the hull of the target ship, and after a certain time of delay, exploded. Certainly such system was very far from perfect, but in the actual circumstances, single shot accuracy was not necessary for the Peruvians. In the plan of the inventor, the "torpedoes" should be used in two pairs, with each pair connected by a cable [similar to chain or dismantling shot] so on surfacing, one of the "torpedoes" should be on each side of the opponent's hull! In theory, the weapon would thus be effective against either moving or stationary targets, with the weight of the cable tending to draw the "torpedoes" toward the target hull.

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$\stackrel{5}{0}$
GERMAN
40 cm SKC/34
$38 \mathrm{~cm} \mathrm{SKC} / 34$
 28 cm SKC/34







|  | " | 149,10 | 44,80 | 840,00 | 65,00 | CPC | 4,50 | 8,50 | 4.8 |  |  |  | 22250 | $\begin{aligned} & \mathrm{Z}-46-\mathrm{Z} 50 \\ & \text { Z1-Z22, Z35- Z36, Z43 } \\ & -\mathrm{Z} 45 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Krupp | $12.8 \mathrm{~cm} \mathrm{KMC/40}$ | 128,00 | 28,00 | 867,00 | 85,00 | SAPBC | 4,41 | 8,60 | 6.5 |  |  |  | 20000 |  |
| Krupp | $12.7 \mathrm{~cm} \mathrm{SKC/34}$ | 128,00 | 28,00 | 830,00 | 30,00 | SAPBC | 4,41 | 8,60 | 4.4 |  |  |  | 17400 |  |
| Krupp | $10.5 \mathrm{~cm} \mathrm{SKC/33}$ | 105,00 | 15,80 | 880,00 | 80,00 | APCBC | 4,10 | 10,00 | 8.0 |  |  |  | 17070 | Standard HA gun |
| Krupp | 10.5 cm SKC/32 | 105,00 | 15,80 | 815,00 | 80,00 | APCBC | 4,10 | 10,00 | 3.5 |  |  |  | 15900 |  |
| Krupp | $8.8 \mathrm{~cm} \mathrm{SKC/30}$ | 88,00 | 10,20 | 740,00 | 80,00 | APCBC | 4,50 | 8,50 | 6.0 |  | 1,52\% | T | 15200 |  |
|  | " | 88,00 | 9,50 | 765,00 | 80,00 | APCBC | 2,91 | 8,50 | 6,0 |  | 1,63\% | T | 14350 |  |
| Krupp | $8.8 \mathrm{~cm} \mathrm{SKC/35}$ | 88,00 | 10,20 | 655,00 | 30,00 | APCBC | 4,50 | 8,50 | 3.5 |  | 1,52\% | T | 12800 |  |
|  | " | 88,00 | 9,50 | 680,00 | 30,00 | APCBC | 2,91 | 8,50 | 3,5 |  | 1,63\% | T | 12150 |  |
| Krupp | $8.8 \mathrm{~cm} \mathrm{SKC/32}$ | 88,00 | 10,20 | 890,00 | 80,00 | APCBC | 4,50 | 8,50 | 6,0 |  | 1,52\% | T | 18000 |  |
|  | IMPERIAL GERMANY |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Krupp | $42 \mathrm{~cm} \mathrm{SKL} 45 \mathrm{C} / 17$ | 420,00 | 1030,00 | 800,00 | 20,00 | APC | 3,28 | 4,00 | 6.5 |  |  | T | 24400 | 'L20ea' 'GK 4542' |
|  | " | 420,00 | 1030,00 | 800,00 | 20,00 | CPC | 4,00 | 4,00 | 6.5 | 9,71\% | 10,29\% | T | 24400 |  |
|  | hypothetical | 420,00 | 1030,00 | 800,00 | 30,00 | APCBC |  | 8,50 | 6,5 |  |  |  | 34000 |  |
| Krupp | 40 cm SKL 35 Gerat 11 | 400,00 | 885,00 | 735,00 | 16,00 | APC | 3,26 | 4,00 | 6.5 |  |  | T | 19300 | proposed Derfflinger \& Konig |
|  | " | 400,00 | 885,00 | 735,00 | 16,00 | SAP | 3,70 | 4,00 | 6.5 |  |  | T | 19300 |  |
| Krupp | 40 cm RK L/25 C/79 | 400,00 | 775,00 | 520,00 | 24,00 | AP | 2,80 | 2,00 | 6.5 |  | 1,29\% | BP | 12300 | Coast Defence |
|  | " | 400,00 | 640,00 | 540,00 | 24,00 | Common | 3,20 | 2,00 | 6.5 |  | 5,19\% | BP | 12050 |  |
| Krupp | $38 \mathrm{~cm} \mathrm{SKU45} \mathrm{C/13}$ | 380,00 | 750,00 | 805,00 | 20,00 | APC | 3,26 | 4,00 | 6.5 |  | 3,33\% | T | 23400 | Bayern, Ersatz Yorck |
|  | " | 380,00 | 750,00 | 805,00 | 20,00 | CPC | 3,84 | 4,00 | 6.5 |  | 8,31\% | T | 23400 |  |
|  | " | 380,00 | 750,00 | 805,00 | 20,00 | SAP | 4,08 | 4,00 | 6.5 |  | 8,93\% | T | 23400 |  |
|  | hypothetical | 380,00 | 760,00 | 800,00 | 30,00 | APCBC |  | 8,50 | 6.5 |  |  |  | 32500 |  |
| Krupp | $35 \mathrm{~cm} \mathrm{SKU45} \mathrm{C/14}$ | 350,00 | 600,00 | 820,00 | 20,00 | APC | 3,30 | 4,00 | 6.5 |  |  | T | 23400 | Mackensen |
|  | " | 350,00 | 600,00 | 820,00 | 20,00 | SAP | 3,73 | 4,00 | 6.5 |  |  | T | 23400 |  |
|  | hypothetical | 350,00 | 615,00 | 815,00 | 30,00 | APCBC |  | 8,50 | 6.5 |  |  |  | 32600 |  |
| Krupp | 34cm SKL/45 Gerat 10 | 337,00 | 535,00 | 835,00 | 16,00 | APC | 3,27 | 4,00 | 6.5 |  |  | T | 20800 | proposed Konig \& Derfflinger |
|  | " | 337,00 | 535,00 | 835,00 | 16,00 | SAP | 3,70 | 4,00 | 6.5 |  |  | T | 20800 |  |
|  | " | 337,00 | 535,00 | 835,00 | 20,00 | APC | 3,27 | 4,00 | 6.5 |  |  | T | 23550 |  |



|  | " | 283,00 | 302,00 | 855,00 | 20,00 | SAP | 3,57 | 4,00 | 7.5 | C/11 |  | 6,82\% | T | 21000 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | " | 283,00 | 285,00 | 855,00 | 37,00 | APC | 2,90 | 3,00 | 7.5 | C/07 | 6,53\% | 3,00\% | T | 24565 | Coast Defence |
|  | " | 283,00 | 302,00 | 855,00 | 45,00 | APC | 3,30 | 4,00 | 7.5 | C/11 | 5,20\% | 3,51\% | T | 29200 | Coast Defence |
|  | hypothetical | 283,00 | 315,00 | 845,00 | 30,00 | APCBC |  | 8,50 | 6.5 |  |  |  |  | 30600 |  |
| Krupp | $28 \mathrm{~cm} \mathrm{SKU40} \mathrm{C/01}$ | 283,00 | 240,00 | 820,00 | 30,00 | APC | 2,60 | 3,00 | 7.5 | C/01 | 3,54\% | 2,52\% | T | 18800 | Braunschweig, Deutschland |
|  | " | 283,00 | 240,00 | 820,00 | 30,00 | SAP | 2,90 | 3,00 | 7.5 | C/01 |  | 5,83\% | T | 18800 |  |
|  | " | 283,00 | 285,00 | 740,00 | 45,00 | APC | 2,90 | 3,00 | 7.5 | C/07 | 6,53\% | 3,00\% | T | 20770 | Coast Defence Kurfurst Friedrich |
| Krupp | 28 cm MRK L/40 C/90 | 283,00 | 255,00 | 700,00 | 25,00 | AP Shot | 2,63 | 2,00 | 5.0 | C/80 |  | 1,37\% | BP | 14635 | Wilhelm |
|  | " | 283,00 | 215,00 | 740,00 | 25,00 | Common | 2,60 | 2,00 | 5.0 | C/80 |  | 5,35\% | PA | 14200 |  |
|  | " | 283,00 | 240,00 | 720,00 | 25,00 | AP | 2,57 | 2,00 | 5.0 | C/95 |  | 2,52\% | PA | 14600 | [160 kg charge] |
|  | " | 283,00 | 240,00 | 700,00 | 25,00 | AP | 2,57 | 2,00 | 5.0 | C/95 |  | 2,52\% | PA | 14175 | [150 kg charge] |
|  | " | 283,00 | 240,00 | 700,00 | 25,00 | Common | 2,90 | 2,00 | 5.0 | C/95 |  | 4,81\% | PA | 14175 |  |
|  | " | 283,00 | 240,00 | 715,00 | 25,00 | APC | 2,60 | 3,00 | 5.0 | C/01 | 3,54\% | 2,52\% | T | 15100 | [1905 w/ RP C/00] |
|  | " | 283,00 | 240,00 | 715,00 | 25,00 | SAP | 2,90 | 3,00 | 5.0 | C/01 |  | 5,83\% | T | 15100 |  |
|  | " | 283,00 | 240,00 | 755,00 | 25,00 | APC | 2,60 | 3,00 | 5.0 | C/01 | 3,54\% | 2,52\% | T | 15900 | [1915 w/ RP C/12] |
|  | " | 283,00 | 240,00 | 755,00 | 25,00 | SAP | 2,90 | 3,00 | 5.0 | C/01 |  | 5,83\% | T | 15900 |  |
| Krupp | 28cm MRK L/35 C/86 | 283,00 | 255,00 | 650,00 | 25,00 | AP Shot | 2,63 | 2,00 | 5.0 | C/80 |  | 1,37\% | BP | 13530 | Kurfurst Friedrich Wilhelm |
|  | " | 283,00 | 215,00 | 720,00 | 25,00 | Common | 2,60 | 2,00 | 5.0 | C/80 |  | 5,35\% | PA | 13760 |  |
|  | " | 283,00 | 240,00 | 680,00 | 25,00 | AP | 2,57 | 2,00 | 5.0 | C/95 |  | 2,52\% | PA | 13755 |  |
|  | " | 283,00 | 240,00 | 680,00 | 25,00 | Common | 2,90 | 2,00 |  | C/95 |  | 4,81\% | PA | 13755 |  |
|  | " | 283,00 | 240,00 | 685,00 | 25,00 | APC | 2,60 | 3,00 | 5.0 | C/01 | 3,54\% | 2,52\% | T | 14450 | ]1905 w/ RP C/00] |
|  | " | 283,00 | 240,00 | 685,00 | 25,00 | SAP | 2,90 | 3,00 | 5.0 | C/01 |  | 5,83\% | T | 14450 |  |
|  | " | 283,00 | 240,00 | 700,00 | 25,00 | APC | 2,60 | 3,00 | 5.0 | C/01 | 3,54\% | 2,52\% | T | 14650 | [1915 w/ RP C/12] |
|  | " | 283,00 | 240,00 | 700,00 | 25,00 | SAP | 2,90 | 3,00 | 5.0 | C/01 |  | 5,83\% | T | 14650 |  |
| Krupp | $28 \mathrm{~cm} \mathrm{RK} \mathrm{L/35} \mathrm{C/80}$ | 283,00 | 345,00 | 525,00 | 17,25 | AP | 3,50 | 3,00 | 4.0 |  |  | 2,32\% | BP | 10175 | Coast Defence |
|  | " | 283,00 | 296,00 | 560,00 | 17,25 | Common | 3,50 | 3,00 | 4.0 |  |  | 3,38\% | BP | 10385 |  |
|  | " | 283,00 | 345,00 | 525,00 | 17,25 | SAP | 3,61 | 3,00 | 4.0 |  |  | 3,83\% | BP | 10175 |  |
| Krupp | $28 \mathrm{~cm} \mathrm{RKL/22} \mathrm{C/78}$ | 283,00 | 255,00 | 460,00 | 24,00 | AP | 2,60 | 2,00 | 4.0 | C/81 |  | 1,37\% | BP | 9500 | Coast Defence |
|  | " | 283,00 | 216,80 | 500,00 | 24,00 | Common | 2,60 | 2,00 | 4.0 | C/81 |  | 5,30\% | BP | 9700 | Coast Defence |
|  | " | 283,00 | 240,00 | 490,00 | 24,00 | AP | 2,45 | 2,00 | 4.0 | C/95 |  | 2,71\% | PA | 10000 | Coast Defence |


|  | " | 283,00 | 240,00 | 490,00 | 24,00 | Common | 2,96 | 2,00 | 4.0 | C/95 |  | 4,79\% | PA | 10000 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | " | 283,00 | 240,00 | 490,00 | 24,00 | APC | 2,60 | 3,00 | 4.0 | C/01 | 3,54\% | 2,52\% | T | 10500 |  |
|  | " | 283,00 | 240,00 | 490,00 | 24,00 | SAP | 2,90 | 3,00 | 4.0 | C/01 |  | 5,83\% | T | 10500 |  |
| Krupp | $26 \mathrm{~cm} \mathrm{RKL/22} \mathrm{C/76}$ | 263,00 | 187,00 | 430,00 | 11,00 | AP | 2,40 | 2,00 | 4.5 |  |  | 1,28\% | BP | 5000 | Preussen |
|  | " | 263,00 | 162,00 | 460,00 | 11,00 | Common | 2,50 | 2,00 | 4.5 |  |  | 4,81\% | BP | 5220 |  |
|  | " | 263,00 | 187,00 | 480,00 | 11,00 | AP | 2,40 | 2,00 | 4.5 |  |  | 1,28\% | BP | 5650 |  |
|  | " | 263,00 | 162,00 | 500,00 | 11,00 | Common | 2,50 | 2,00 | 4.5 |  |  | 4,85\% | BP | 5675 |  |
|  | " | 263,00 | 187,00 | 480,00 | 16,50 | AP | 2,40 | 2,00 | 4.5 |  |  | 1,28\% | BP | 7400 | Sachsen |
|  | " | 263,00 | 162,00 | 500,00 | 16,50 | Common | 2,50 | 2,00 | 4.5 |  |  | 4,81\% | BP | 7360 |  |
| Krupp | $26 \mathrm{~cm} \mathrm{RKL/20} \mathrm{C/74}$ | 263,00 | 187,00 | 445,00 | 11,00 | AP | 2,40 | 2,00 | 4.5 |  |  | 1,28\% | BP | 5200 | Kaiser |
|  | " | 263,00 | 162,00 | 460,00 | 11,00 | Common | 2,50 | 2,00 | 4.5 |  |  | 4,81\% | BP | 5440 |  |
|  | " | 263,00 | 187,00 | 480,00 | 11,00 | AP | 2,40 | 2,00 | 4.5 |  |  | 1,28\% | BP | 5650 |  |
|  | " | 263,00 | 162,00 | 500,00 | 11,00 | Common | 2,50 | 2,00 | 4.5 |  |  | 4,85\% | BP | 5675 |  |
| Krupp | $24 \mathrm{~cm} \mathrm{SK} \mathrm{L/50}$ | 238,00 | 148,50 | 900,00 | 30,00 | HE | 4,20 | 8,50 | 4.5 |  |  | 10,01\% | T | 26700 | Coast Defence |
|  | " | 238,00 | 150,50 | 900,00 | 30,00 | SAPBC | 4,10 | 8,50 | 4.5 |  |  | 5,51\% | T | 26700 | Coast Defence |
|  | " | 238,00 | 151,00 | 900,00 | 30,00 | CP | 4,10 | 8,50 | 4.5 |  |  | 9,87\% | T | 26700 | Coast Defence |
| Krupp | 24 cm SKL/40 C/97 \& $\mathrm{C} / 98$ | 238,00 | 215,00 | 700,00 | 30,00 | AP | 3,50 | 2,00 | 4.5 | C/80 |  | 1,74\% | PA | 16600 | Kaiser Friedrich III, Wittelsbach, Furst Bismarck, |
|  | " | 238,00 | 215,00 | 700,00 | 30,00 | Common | 4,50 | 2,00 | 4.5 | C/80 |  | 6,23\% | PA | 16600 |  |
|  |  | 238,00 | 215,00 | 800,00 | 30,00 | Common | 4,50 | 2,00 | 4.5 | C/80 |  | 6,23\% | PA | 16600 | Kaiser Friedrich III, Wittelsbach, Furst Bis- |
|  | " | 238,00 | 140,00 | 835,00 | 30,00 | AP | 2,83 | 2,00 | 4.5 | C/01 |  | 5,93\% | T | 16900 | marck, |
|  | " | 238,00 | 140,00 | 835,00 | 30,00 | SAP | 2,73 | 2,00 | 4.5 | C/01 |  | 6,14\% | T | 16900 | Prinz Heinrich |
|  | " | 238,00 | 140,00 | 835,00 | 30,00 | CP | 3,00 | 2,00 | 4.5 | C/01 |  | 9,93\% | PA | 16900 |  |
|  | " | 238,00 | 146,00 | 835,00 | 30,00 | APC | 3,10 | 4,00 | 4.5 | C/01/07 | 4,11\% | 5,68\% | T | 19700 |  |
|  | " | 238,00 | 146,00 | 835,00 | 30,00 | SAPC | 3,00 | 4,00 | 4.5 | C/01/07 | 4,11\% | 5,89\% | T | 19700 |  |
|  | " | 238,00 | 148,50 | 810,00 | 45,00 | HE | 4,20 | 8,50 | 4.5 |  |  | 10,01\% | T | 26600 | Coast Defence |
|  | " | 238,00 | 150,50 | 810,00 | 45,00 | SAPBC | 4,10 | 8,50 | 4.5 |  |  | 5,51\% | T | 26600 | Coast Defence |
|  | " | 238,00 | 151,00 | 810,00 | 45,00 | CP | 4,10 | 8,50 | 4.5 |  |  | 9,87\% | T | 26600 | Coast Defence |
| Krupp | 24cm MRKL/35 C/88 | 238,00 | 215,00 | 580,00 | 25,00 | AP | 3,50 | 2,00 | 5.0 | C/80 |  | 1,74\% | PA | 13030 | Siegfried, Odin |
|  | " | 238,00 | 215,00 | 580,00 | 25,00 | Common | 4,50 | 2,00 | 5.0 | C/80 |  | 7,67\% | PA | 13030 |  |
|  | " | 238,00 | 140,00 | 690,00 | 25,00 | AP | 2,40 | 2,00 | 5.0 | C/01 |  | 2,47\% | PA | 13000 |  |



|  | " | 209,30 | 108,00 | 780,00 | 30,00 | APC | 2,91 | 3,00 | 6.5 | C07 | 3,29\% | T | 16770 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | " | 209,30 | 108,00 | 780,00 | 30,00 | SAP | 3,10 | 3,00 | 6.5 | C/07 | 5,86\% | T | 16770 |  |
|  | " | 209,30 | 115,00 | 815,00 | 30,00 | CP | 4,20 | 8,50 | 6.5 |  | 7,08\% | T | 22600 | Coast Defence |
| Krupp | 21cm RKL/30 C/84 | 209,30 | 140,00 | 505,00 | 13,00 | AP | 3,50 | 2,00 | 4.0 |  | 1,79\% | BP | 7100 | Brummer |
|  | " | 209,30 | 140,00 | 505,00 | 13,00 | Common | 4,30 | 2,00 | 4.0 |  | 3,93\% | BP | 7100 |  |
| Krupp | 21cm RKL/22.5 C/68 | 209,30 | 98,50 | 446,00 | 14,00 | AP | 2,50 | 3,00 | 2.5 | Steel 1872 | 1,32\% | BP | 5900 | Kronprinz, Friedrich Carl, Konig Wilhelm |
|  | " | 209,30 | 79,00 | 425,00 | 14,00 | Common | 2,40 | 2,00 | 2.5 |  | 5,95\% | BP | 5280 | Kaiser |
| Krupp | 21cm RKL/20 C/68 | 209,30 | 98,50 | 433,00 | 14,00 | AP |  | 3,00 | 2.5 |  | 1,29\% | BP | 5700 | Hansa |
|  | " | 209,30 | 79,00 | 425,00 | 14,00 | Common |  | 2,00 | 2.5 |  | 5,95\% | BP | 5280 |  |
| Krupp | 21cm RKL/19 C/67 | 209,30 | 89,00 | 421,00 | 12,00 | AP | 2,50 | 2,00 | 2.5 | Gruson chilled | 1,35\% | BP | 4700 | Arminius, Prinz Adalbert |
|  | " | 209,30 | 78,00 | 391,00 | 12,00 | Common |  | 2,00 | 2.5 |  | 8,72\% | BP | 4230 |  |
|  | " | 209,30 | 89,00 | 421,00 | 14,00 | AP | 2,50 | 2,00 | 2.5 | Gruson chilled | 1,35\% | BP | 5200 | Friedrich Carl, Kronprinz |
|  | " | 209,30 | 78,00 | 391,00 | 14,00 | Common |  | 2,00 | 2.5 |  | 8,72\% | BP | 4690 |  |
|  | " | 209,30 | 98,50 | 401,00 | 14,50 | AP |  | 3,00 | 2.5 | Steel 1872 | 1,32\% | BP | 4700 | Friedrich Carl, Kronprinz |
|  | " | 209,30 | 79,00 | 389,00 | 14,50 | Common | 2,40 | 2,00 | 2.5 |  | 5,95\% | BP | 4970 |  |
|  | " | 209,30 | 98,50 | 437,00 | 14,50 | AP |  | 2,00 | 2.5 |  | 1,32\% | BP | 5900 |  |
|  | " | 209,30 | 79,00 | 425,00 | 14,50 | Common |  | 2,00 | 2.5 |  | 5,95\% | BP | 5410 |  |
| Krupp | $21 \mathrm{~cm} \mathrm{L/12.25} \mathrm{C/65}$ | 209,30 | 89,00 | 335,00 | 12,75 | AP | 2,50 | 2,00 | 2.5 | Gruson chilled | 1,35\% | BP | 3900 | Camaleon |
|  | " | 209,30 | 78,00 | 311,00 | 12,75 | Common | 2,40 | 2,00 | 2.5 |  | 6,03\% | BP | 3440 |  |
| Krupp | $17 \mathrm{~cm} \mathrm{SKL/40} \mathrm{C/01}$ | 172,60 | 64,00 | 850,00 | 22,00 | HE | 3,00 | 3,00 | 4.0 | M1901 | 5,47\% | PA | 14500 | Braunschweig, Deutschland |
|  | " | 172,60 | 64,00 | 850,00 | 22,00 | APC | 2,60 | 3,00 | 4.0 | M1901 |  | T | 14500 |  |
|  | " | 172,60 | 64,00 | 850,00 | 30,00 | HE | 3,00 | 3,00 | 4.0 | M1901 | 5,47\% | PA | 16900 | (turrets and coast defence) |
|  | " | 172,60 | 64,00 | 850,00 | 30,00 | APC | 2,60 | 3,00 | 4.0 | M1901 |  | T | 16900 |  |
|  | " | 172,60 | 62,80 | 815,00 | 45,00 | HE | 4,70 | 10,00 | 8,0 |  | 10,24\% | T | 24000 | Coast Defence |
| Krupp | 17cm RKL/24.6 C/72 | 172,60 | 55,90 | 472,00 | 11,00 | AP | 2,40 | 2,00 | 3.7 |  | 1,07\% | BP | 5000 | Preussen. Leipzig |
|  | " | 172,60 | 51,00 | 465,00 | 11,00 | Common | 2,80 | 2,00 | 3.7 |  | 8,24\% | BP | 5000 |  |
|  | " | 172,60 | 53,50 | 475,00 | 11,00 | AP | 2,41 | 2,00 | 3.7 |  | 1,12\% | BP | 5000 |  |
|  | " | 172,60 | 51,30 | 490,00 | 11,00 | Common | 2,79 | 2,00 | 3.7 |  | 4,48\% | BP | 5090 |  |
|  | " | 172,60 | 53,50 | 490,00 | 11,00 | AP | 2,41 | 2,00 | 3.7 |  | 1,12\% | BP | 5150 |  |



|  | " | 149,10 | 51,00 | 620,00 | 30,00 | CP | 4,31 | 2,00 | 4.4 |  | 7,85\% | PA | 12100 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | " | 149,10 | 40,00 | 680,00 | 30,00 | AP | 2,75 | 3,00 | 4.4 | C/01 | 2,50\% | PA | 12300 |  |
|  | " | 149,10 | 40,00 | 680,00 | 30,00 | SAP | 3,02 | 3,00 | 4.4 | C/07 | 4,05\% | PA | 12600 |  |
|  | " | 149,10 | 40,00 | 680,00 | 30,00 | CP | 3,38 | 3,00 | 4.4 | C/01 | 10,00\% | PA | 12300 |  |
|  | " | 149,10 | 40,00 | 680,00 | 30,00 | HE | 3,60 | 3,00 | 4.4 | C/07 | 11,00\% | PA | 12600 |  |
|  | " | 149,10 | 45,00 | 675,00 | 30,00 | SAPBC | 4,20 | 8,50 | 4.4 |  |  |  | 16585 |  |
| Krupp | $15 \mathrm{~cm} \mathrm{RKL/30} \mathrm{C/83}$ | 149,10 | 51,00 | 495,00 | 21,00 | AP | 3,35 | 2,00 | 4,0 |  | 1,33\% | BP | 8500 | Irene |
|  | " | 149,10 | 51,00 | 495,00 | 21,00 | Common | 4,00 | 2,00 | 4,0 |  | 3,82\% | BP | 8500 |  |
|  | " | 149,10 | 51,00 | 495,00 | 14,50 | AP | 3,35 | 2,00 | 4,0 |  | 1,33\% | BP | 6788 | Alexandrine, Arcona |
|  | " | 149,10 | 51,00 | 495,00 | 14,50 | Common | 4,00 | 2,00 | 4,0 |  | 3,82\% | BP | 6788 |  |
|  | RP C/88 QFC | 149,10 | 51,00 | 505,00 | 20,50 | AP | 3,35 | 2,00 | 4,0 |  | 1,33\% | BP | 8530 | Kaiser 1895 |
|  | " | 149,10 | 51,00 | 505,00 | 20,50 | Common | 4,00 | 2,00 | 4,0 |  | 3,82\% | BP | 8530 |  |
|  | " | 149,10 | 51,00 | 505,00 | 22,50 | AP | 3,35 | 2,00 | 4,0 |  | 1,33\% | BP | 8990 | Konig Wilhelm 1896 |
|  | " | 149,10 | 51,00 | 505,00 | 22,50 | Common | 4,00 | 2,00 | 4,0 |  | 3,82\% | BP | 8990 |  |
|  | " | 149,10 | 51,00 | 505,00 | 28,00 | AP | 3,35 | 2,00 | 4,0 |  | 2,94\% | PA | 10055 | Irene after 1902 |
|  | " | 149,10 | 51,00 | 505,00 | 28,00 | Common | 4,00 | 2,00 | 4,0 |  | 7,85\% | PA | 10055 |  |
| Krupp | $15 \mathrm{~cm} \mathrm{~K} \mathrm{L/22} \mathrm{C/65}$ | 149,10 | 35,50 | 414,00 | 13,00 | AP | 2,40 | 2,00 | 4,0 |  | 1,13\% | BP | 4600 | Arcona, Albatross |
|  | " | 149,10 | 27,70 | 441,00 | 13,00 | Common | 2,50 | 2,00 | 4,0 |  | 3,07\% | BP | 4480 | Thetis |
| Krupp | $15 \mathrm{~cm} \mathrm{~K} \mathrm{L/22} \mathrm{C/68}$ | 149,10 | 34,50 | 414,00 | 13,00 | AP | 2,41 | 2,00 | 4,0 |  | 1,04\% | BP | 4700 |  |
|  | " | 149,10 | 29,50 | 441,00 | 13,00 | Common | 2,49 | 2,00 | 4,0 |  | 6,44\% | BP | 4740 |  |
| Krupp | 15 cm RK L/22 C/72 | 149,10 | 34,50 | 450,00 | 13,00 | AP | 2,41 | 2,00 | 4,0 |  | 1,16\% | BP | 5000 | Arcona, Augusta, Ariadne, Carola |
|  | 15 cm RK L/22 C/65 | 149,10 | 29,50 | 485,00 | 13,00 | Common | 2,49 | 2,00 | 4,0 |  | 6,44\% | BP | 5010 |  |
|  | 15 cm RK L/22 C/68 | 149,10 | 34,50 | 446,00 | 14,60 | AP | 2,41 | 2,00 | 4,0 |  | 1,04\% | BP | 5400 | Habicht |
|  | 15 cm RK L/22 QFC | 149,10 | 29,50 | 474,00 | 14,60 | Common | 2,49 | 2,00 | 4,0 |  | 6,44\% | BP | 5390 |  |
|  |  | 149,10 | 34,50 | 446,00 | 15,00 | AP | 2,41 | 2,00 | 4,0 |  | 1,04\% | BP | 5500 | Charlotte, Bismarck |
|  |  | 149,10 | 29,50 | 474,00 | 15,00 | Common | 2,49 | 2,00 | 4,0 |  | 6,44\% | BP | 5490 |  |
| Wahrendorf | ${ }_{\mathrm{pdr})}^{15 \mathrm{~cm}} \mathrm{G.L/21}$ M. 61 (24- | 149,10 | 35,50 | 300,00 | 14,00 | AP | 2,40 | 2,00 | 3.0 |  | 1,13\% | BP | 3540 | Jager \& Caaleon |
|  | " | 149,10 | 27,70 | 310,00 | 14,00 | Common | 2,00 | 2,00 | 3.0 |  | 7,22\% | BP | 3540 |  |
| Krupp | $12.5 \mathrm{~cm} \mathrm{RKL} / 23 \mathrm{C} / 78$ | 125,00 | 18,20 | 471,00 | 14,00 | Common | 3,00 | 2,00 | 3,8 |  | 6,04\% | BP | 5000 | Arcona, Nixe |
|  | " | 125,00 | 18,20 | 471,00 | 15,00 | Common | 3,00 | 2,00 | 3,8 |  | 6,04\% | BP | 5200 | Grille, Wolf |


| 6,04\% | BP | 5600 | Habicht |
| :---: | :---: | :---: | :---: |
|  | BP | 2900 | Rhein |
|  |  |  | Habicht, Otter, Nymphe, |
| 7,53\% | BP | 5000 | Thetis, Falke |
| 7,53\% | BP | 5500 | Albatross, Cyclop |
|  |  |  | Augusta, Ariadne, |
| 7,53\% | BP | 5900 | Nymphe |
|  |  | 3890 | Jager \& Caaleon |
| 6,67\% | BP | 3520 |  |
| 10,00\% | T | 19500 | Coast Defence |
| 9,06\% | T | 19500 |  |
| 3,46\% | T | 16000 |  |
|  |  |  | Kolberg through |
| 5,40\% | T | 12700 | Regensberg |
| 9,64\% | T | 12700 |  |
| 4,56\% | T | 11880 |  |
| 5,40\% | T | 11810 | destroyers |
| 9,64\% | T | 11810 |  |
|  |  |  | Gazelle through |
| 3,46\% | PA | 12200 | Dresden |
| 10,00\% | T | 12200 |  |
| 5,40\% | T | 12450 |  |
| 9,64\% | T | 12450 |  |
| 4,56\% | T | 11500 |  |
| 3,46\% | PA | 11020 |  |
| 10,00\% | PA | 11020 |  |
| 5,40\% | T | 10820 |  |
| 9,64\% | $T$ | 10820 |  |
| 4,56\% | T | 10785 |  |
|  |  |  | Greif, Schwalbe, Wacht |
| 2,28\% | BP | 8200 | Alexandrine |
| 5,36\% | PA | 8200 |  |
|  | T |  | standard HA gun from c. |
|  | $T$ |  | 1913 |


|  | " | 125,00 | 18,20 | 471,00 | 17,00 | Common | 3,00 | 2,00 | 3,8 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Uchiatus | 12cm/19 C/65 (Bronze) | 120,00 | 12,00 | 350,00 | 13,00 | Common | 2,00 | 2,00 | 3.6 |  |
| Krupp | $12 \mathrm{~cm} \mathrm{RKL} / 23 \mathrm{C} / 69$ | 120,03 | 15,00 | 390,00 | 18,00 | Common | 2,30 | 2,00 | 3,0 |  |
|  | " | 120,03 | 15,00 | 390,00 | 21,50 | Common | 2,30 | 2,00 | 3,0 |  |
|  | "' ${ }^{\text {a }}$ | 120,03 | 15,00 | 390,00 | 25,00 | Common | 2,30 | 2,00 | 3,0 |  |
| Wahrendorff | $\underset{\mathrm{pdr})}{12 \mathrm{~cm}}$ G.L/23 M. 61 (12- | 121,92 | 20,00 | 332,00 | 14,00 | Shot | 2,80 | 2,00 | 3,0 |  |
|  | " | 121,92 | 15,00 | 321,00 | 14,00 | Common | 2,30 | 2,00 | 3,0 |  |
| Krupp | 10.5cm SK L/50 C/06 | 105,00 | 18,00 | 820,00 | 45,00 | HE | 4,76 | 8,50 | 8,0 |  |
|  | " | 105,00 | 16,00 | 850,00 | 45,00 | HE | 5,20 | 10,00 | 8,0 |  |
|  | 10.5 cm SKL $45 \mathrm{C} / 06$ | 105,00 | 18,20 | 820,00 | 45,00 | AP | 3,80 | 4,00 | 8,0 |  |
| Krupp | 10.5 cm SKL/45 C/06 \& C/12 | 105,00 | 17,40 | 710,00 | 30,00 | SAP |  | 4,00 | 4.4 | C/07 |
|  | " | 105,00 | 17,50 | 710,00 | 30,00 | HE | 3,60 | 4,00 | 4.4 | C/07 |
|  | " | 105,00 | 14,25 | 940,00 | 30,00 | APC | 2,77 | 2,00 | 4.4 | C/07 |
| Krupp | 10.5cm TKL/45 C/16 | 105,00 | 17,40 | 650,00 | 30,00 | SAP | 3,90 | 4,00 | 4.4 | C/07 |
|  | " | 105,00 | 17,50 | 650,00 | 30,00 | HE | 3,85 | 4,00 | 4.4 | C/07 |
| Krupp | 10.5cm SKL/40 C/97 | 105,00 | 18,20 | 715,00 | 30,00 | AP | 3,80 | 3,00 | 4.4 |  |
|  | " | 105,00 | 18,00 | 715,00 | 30,00 | HE | 3,89 | 3,00 | 4.4 |  |
|  | " | 105,00 | 17,40 | 690,00 | 30,00 | SAP | 3,90 | 3,00 | 4.4 | C/07 |
|  | " | 105,00 | 17,50 | 690,00 | 30,00 | HE | 3,85 | 3,00 | 4.4 | C/07 |
|  | " | 105,00 | 14,25 | 890,00 | 30,00 | APC | 2,77 | 2,00 | 4.4 | C/07 |
| Krupp | 10.5cm SKL/35 C/91 | 105,00 | 18,20 | 620,00 | 30,00 | AP | 3,80 | 3,00 | 3.1 |  |
|  | " | 105,00 | 18,00 | 620,00 | 30,00 | HE | 3,89 | 3,00 | 3.1 |  |
|  | " | 105,00 | 17,40 | 600,00 | 30,00 | SAP | 3,70 | 3,00 | 3.1 | C/07 |
|  | " | 105,00 | 17,50 | 600,00 | 30,00 | HE | 3,50 | 3,00 | 3.1 | C/07 |
|  | " | 105,00 | 14,25 | 800,00 | 30,00 | APC | 2,77 | 2,00 | 3.1 | C/07 |
| Krupp | $10.5 \mathrm{~cm} \mathrm{RKL} / 35 \mathrm{C} / 86$ | 105,00 | 18,00 | 465,00 | 27,00 | Common |  | 2,00 | 3,0 | C/80 |
|  | " | 105,00 | 18,00 | 465,00 | 27,00 | Common | 3,90 | 2,00 | 3,0 | C/92 |
| Krupp | $8.8 \mathrm{~cm} \mathrm{FLAKL/45} \mathrm{C/13}$ | 88,00 | 9,93 | 765,00 | 70,00 | SAP | 3,80 | 3,00 | 6.0 | C/07 |

standard anti-torpedo
boat gun till c. 1918
N
0.0
0.0
0
0
0
 old Torpedoboat
destroyers









 | 8 | 8 | 0 | 8 | 0 | 8 | 0 | 0 | 0 | 8 | 8 | 8 | 8 | 0 | 8 | 8 | 8 | 0 | 8 | 8 | 8 | 8 | 8 | 8 | 0 | 8 | 8 | 8 | 8 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |




| Krupp | $8.8 \mathrm{~cm} \mathrm{SKL} / 45 \mathrm{C} / 09$ |
| :---: | :---: |
|  | " |
|  | " |
| Krupp | $8.8 \mathrm{~cm} \mathrm{TKL} / 45 \mathrm{C} / 14$ |
|  | " |
|  | " |
| Krupp | $8.8 \mathrm{~cm} \mathrm{TKL} / 30 \mathrm{C} / 08$ |
|  | " |
|  | " |
|  | " |
|  | " |
|  | " |
|  | " |
|  | " |
|  | " |
| Krupp | $8.8 \mathrm{~cm} \mathrm{SKL} / 35 \mathrm{C} / 01$ |
|  | " |
|  | " |
|  | " |
|  | " |
|  | " |
|  | " |
| Krupp | $8.8 \mathrm{~cm} \mathrm{SKL} / 30 \mathrm{C} / 89$ |


|  |  |  | $\dot{ن}$ |  | Musquito，Pommerania | $\stackrel{\cong}{\overline{=心}}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  | $\begin{aligned} & =0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & \hline \end{aligned}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & 8 \\ & \hline 8 \\ & 0 \end{aligned}$ | $\begin{aligned} & \circ \\ & \hline 8 \\ & 0 \end{aligned}$ | $\begin{aligned} & \circ \\ & \hline \text { ᄋ } \\ & 6 \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \end{aligned}$ | $\begin{aligned} & \circ \\ & \text { O } \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \text { ó } \\ & \text { m } \end{aligned}$ | $\begin{aligned} & \circ \\ & \text { ob } \\ & \text { m } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \infty \\ & \mathrm{~m} \end{aligned}$ |  | $\begin{aligned} & \text { o } \\ & \text { o } \\ & \text { M } \end{aligned}$ | $\begin{aligned} & \text { O } \\ & \text { + } \\ & \text { M } \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{\circ}{+} \\ & \text { M } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text {-1 } \\ & \text { m } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text {-1 } \\ & \text { ल } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { I } \\ & \text { M } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{O} \\ & \stackrel{N}{\mathrm{~N}} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{O} \\ & \stackrel{N}{N} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { ㅇ } \\ & \text { i} \end{aligned}$ | $\begin{aligned} & \circ \\ & \hline \\ & \text { O } \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \circ \\ & \hline 8 \\ & \text { O } \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { N } \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { N } \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \text { O } \\ & \text { N } \\ & \text { N } \end{aligned}$ | O － N | O － N |
| 0 | ® | $\vdash$ | 0 | no | 0 | 呙 | － |  | $\vdash$ |  | $\vdash$ | $\vdash$ |  | $\vdash$ | $\vdash$ |  | $\vdash$ | $\vdash$ | $\vdash$ | $\vdash$ | $\vdash$ | $\vdash$ | $\vdash$ | $\vdash$ | $\vdash$ |
| $\underset{\sim}{\sim}$ | $\begin{gathered} \stackrel{\rightharpoonup}{4} \\ \underset{\sim}{-} \end{gathered}$ | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \stackrel{0}{\infty} \\ & \stackrel{\sim}{\circ} \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{0}{0} \\ & \text { ì } \end{aligned}$ | $\begin{aligned} & \circ 0 \\ & \stackrel{0}{1} \\ & \stackrel{1}{N} \end{aligned}$ | $\begin{gathered} \stackrel{\rightharpoonup}{\circ} \\ \stackrel{y}{0} \\ \text { é } \end{gathered}$ | $\begin{aligned} & \stackrel{\circ}{\stackrel{1}{4}} \\ & \text { é } \end{aligned}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{\circ} \\ & \stackrel{\rightharpoonup}{0} \\ & \text { en } \end{aligned}$ |  | $\begin{aligned} & \text { oे } \\ & \text { ì } \end{aligned}$ |  | $\begin{gathered} \stackrel{\circ}{\circ} \\ \stackrel{N}{N} \\ \hline \end{gathered}$ | $\begin{aligned} & \text { ò } \\ & \text { ì } \\ & \text { N } \end{aligned}$ |  | $\stackrel{0}{2}$ $\stackrel{0}{0}$ $\stackrel{y}{n}$ | $\begin{aligned} & \text { ò } \\ & \text { ì } \\ & \text { N } \end{aligned}$ |  | $\begin{aligned} & \text { ò } \\ & 0 \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \stackrel{\text { ®}}{+} \\ & \text { Ni } \end{aligned}$ | $\begin{aligned} & \text { oे } \\ & \text { î } \\ & \text { ஸi } \end{aligned}$ | $\begin{gathered} \text { N} \\ \stackrel{N}{N} \end{gathered}$ | $\begin{aligned} & \stackrel{y}{\circ} \\ & \vdots \\ & \text { Ni } \end{aligned}$ |  | $\begin{aligned} & \text { Ǹ } \\ & \stackrel{N}{\mathrm{~N}} \end{aligned}$ | $\stackrel{\circ}{\circ}$ | － |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \stackrel{\rightharpoonup}{0} \\ & \stackrel{0}{\circ} \\ & \stackrel{0}{2} \end{aligned}$ | คั | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \stackrel{0}{\circ} \\ & 0^{-} \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \stackrel{5}{\circ} \\ & 6 \end{aligned}$ | \％o |  |
| $\frac{\infty}{0}$ | $\begin{aligned} & \infty \\ & \stackrel{\infty}{M} \\ & \stackrel{\infty}{\omega} \end{aligned}$ | $\stackrel{-1}{O}$ |  |  |  |  |  |  | $\begin{aligned} & \text { O} \\ & \text { E } \\ & \text { E } \\ & \text { N } \\ & \text { N } \end{aligned}$ |  | 울 E N N | 오 ㅌ N N N | 오 E 흘 | 운 튼 N N | 운 E N N | $\begin{aligned} & \text { 오 } \\ & \text { E } \\ & \text { © } \\ & \hline 山 \end{aligned}$ |  | $\begin{aligned} & \stackrel{9}{9} \\ & \hline 8 \end{aligned}$ |  | $\begin{aligned} & \circ \\ & \hline 又 \end{aligned}$ | 오 E 옹 ㅂ |  |  | 오 ㅌ U U | ה |
| $\stackrel{-1}{ }$ | $\stackrel{-1}{\sim}$ | $\stackrel{-}{\text { m }}$ | $\stackrel{+}{*}$ | $\stackrel{\circ}{-}$ | $\stackrel{\bigcirc}{-}$ | $\stackrel{\circ}{\circ}$ | $\stackrel{\square}{-}$ |  | $\stackrel{\infty}{\bullet}$ |  | $\stackrel{\infty}{6}$ | $\stackrel{\bigcirc}{\sim}$ |  | $\stackrel{\bigcirc}{\sim}$ | $\stackrel{\infty}{\bullet}$ |  | $\stackrel{\infty}{\bullet}$ | $\stackrel{\text { ® }}{\text { ¢ }}$ | $\stackrel{\llcorner }{6}$ | $\stackrel{\sim}{6}$ | $\stackrel{\sim}{6}$ | $\stackrel{\sim}{6}$ | $\stackrel{\sim}{6}$ | $\stackrel{\sim}{6}$ | $\stackrel{\sim}{6}$ |
| $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { ले } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { ले } \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\begin{aligned} & \text { O } \\ & \text { in } \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { N } \end{aligned}$ | － |  | $\begin{aligned} & \text { O} \\ & \text { م } \\ & \text { N } \end{aligned}$ | $\begin{aligned} & 0 \\ & \mathrm{~L}^{\circ} \\ & \mathbf{N}^{\circ} \end{aligned}$ | $\begin{aligned} & 0 \\ & \mathbf{n}^{\circ} \\ & 0 \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{0}{\circ} \\ & \infty^{-} \end{aligned}$ | $\begin{aligned} & 0 \\ & 0_{0}^{\prime} \\ & 0^{\circ} \end{aligned}$ | $\begin{aligned} & 0 \\ & \mathrm{~B}^{\circ} \\ & \mathbf{N}^{-} \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{0}{\circ} \\ & \infty^{-} \end{aligned}$ | $\begin{aligned} & \circ \\ & \mathrm{C}^{\circ} \end{aligned}$ | $\begin{aligned} & 0 \\ & 0^{\circ} \\ & 0^{\circ} \end{aligned}$ | O | $\begin{aligned} & \mathrm{O} \\ & \text { ल } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { m} \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{\circ}{-} \end{aligned}$ | － | $\stackrel{8}{\circ}$ | ${ }_{0}^{\circ}$ | － |
| $\begin{aligned} & \mathrm{O} \\ & \stackrel{y}{4} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\stackrel{\circ}{\infty}$ | No | ৪ | $\stackrel{\text { N }}{\text { N }}$ | N | $\stackrel{N}{\sim}$ |  | $\begin{aligned} & \stackrel{\rightharpoonup}{\sim} \\ & \underset{\sim}{2} \end{aligned}$ | $\begin{aligned} & 0 \\ & \stackrel{0}{\circ} \\ & \end{aligned}$ | $\stackrel{\circ}{\circ}$ | $\begin{aligned} & \mathrm{8} \\ & \text { m } \end{aligned}$ | $\stackrel{\text { 악 }}{+}$ | $\stackrel{\circ}{\circ}$ | $\stackrel{\text { N }}{\underset{\sim}{2}}$ | ＋ | $\begin{aligned} & \mathrm{O} \\ & \underset{\sim}{\circ} \end{aligned}$ | － | $\stackrel{\sim}{\infty}$ | $\stackrel{8}{\circ}$ | $\begin{aligned} & \mathrm{O} \\ & \text { ले } \end{aligned}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{7} \\ & \underset{\sim}{n} \end{aligned}$ | $\stackrel{\text { 악 }}{+}$ | ¢ | $\xrightarrow{\circ}$ |
| ᄃ 0 0 0 | $\begin{aligned} & \text { ㄷ } \\ & \text { E } \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | $\frac{\stackrel{0}{6}}{6}$ |  |  | $\begin{aligned} & \text { ס } \\ & \stackrel{E}{E} \\ & 0 \\ & \hline 0 \end{aligned}$ | $$ | $\begin{aligned} & \bar{O} \\ & \check{E} \\ & 0 \\ & \hline 0 \end{aligned}$ |  | $\begin{aligned} & \text { U } \\ & 0 \\ & 0 \\ & \text { Qu } \end{aligned}$ | $\begin{aligned} & U \\ & 0 \\ & 0 \\ & \frac{1}{4} \\ & \text { in } \end{aligned}$ | $\begin{aligned} & U \\ & 0 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & U \\ & 0 \\ & U \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & u \\ & 0 \\ & 0 \\ & 0 \\ & \vdots \\ & \vdots \end{aligned}$ | $\begin{aligned} & U \\ & 0 \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \\ & 0 \\ & \text { Q } \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \\ & 0 \\ & 0 \\ & \frac{1}{6} \end{aligned}$ | $\begin{aligned} & U \\ & 0 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 0 \\ & \frac{0}{4} \end{aligned}$ | $$ | $\begin{aligned} & \text { U } \\ & \text { OU } \end{aligned}$ | $\begin{aligned} & 0 \\ & \text { Q } \\ & \hline \end{aligned}$ | $$ | U | $\begin{aligned} & \text { U } \\ & \text { O } \\ & \text { D } \\ & \text { ๗ } \end{aligned}$ | 0 |
| O- | $\begin{aligned} & \text { O } \\ & \text { N } \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\begin{aligned} & \text { B } \\ & \text { ì } \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{\rightharpoonup}{-} \\ & \underset{-}{2} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \underset{-}{\prime} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \underset{\sim}{\mathrm{H}} \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{\circ}{-} \\ & \text { - } \end{aligned}$ |  | $\begin{aligned} & \text { O} \\ & \text { ò } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { B- } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { O- } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { ò } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { B- } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text {-̀ } \end{aligned}$ | O- | $\begin{aligned} & \text { O- } \\ & \text { N- } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { D } \end{aligned}$ | O- | $\begin{aligned} & \mathrm{O} \\ & \text { Di } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{O} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { D } \end{aligned}$ | $\begin{aligned} & \text { O } \\ & \text { N } \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { N } \end{aligned}$ | O－ | O－ |
| $\begin{aligned} & 8 \\ & \stackrel{0}{6} \\ & \hline 1 \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{0}{0} \\ & \stackrel{\rightharpoonup}{6} \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{0}{6} \\ & \stackrel{7}{6} \end{aligned}$ | O － － | $\begin{aligned} & \text { O- } \\ & \text { ®్ల } \end{aligned}$ | $\begin{aligned} & \text { ৪ } \\ & \underset{-}{-} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { ò } \\ & \text { M } \end{aligned}$ | $\begin{aligned} & \text { O } \\ & \text { ণ } \end{aligned}$ |  | $\begin{aligned} & \text { O} \\ & \text { 읏 } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { O} \\ & \stackrel{0}{N} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { ó } \\ & \text { N } \end{aligned}$ | O | $\begin{aligned} & 8 \\ & 8 \\ & 0 \\ & \hline 0 \end{aligned}$ | $\begin{aligned} & \circ \\ & \hline 8 \\ & \hline 0 \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { O } \\ & \mathrm{N} \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{\circ}{\mathrm{N}} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { o } \\ & \mathrm{N} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \hline 0 \\ & \hline 0 \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 . \\ & 0 . \end{aligned}$ | O | $\begin{aligned} & \text { O } \\ & \text { O } \\ & 0 \end{aligned}$ | $\begin{aligned} & \circ \\ & \hline 0 \\ & 0 \\ & \hline 0 \end{aligned}$ | 8 | O | 8 |
| $\begin{aligned} & \circ \\ & 0 \\ & \hline- \end{aligned}$ | $\begin{aligned} & -1 \\ & 0_{0}^{\prime} \end{aligned}$ | $\underset{\sim}{\text { O}}$ | $\stackrel{\bullet}{\underset{6}{\circ}}$ | $\stackrel{\bullet}{\stackrel{\rightharpoonup}{m}}$ | $\stackrel{\stackrel{\rightharpoonup}{+}}{\underset{\sim}{+}}$ | $\stackrel{\ominus}{\underset{\sim}{\sim}}$ | $\begin{aligned} & \underset{\sim}{N} \\ & \underset{\sim}{n} \end{aligned}$ |  | $\begin{aligned} & \mathrm{O} \\ & \mathrm{O} \\ & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { O- } \\ & \text { N } \end{aligned}$ | O B － N + | $\begin{aligned} & \text { O } \\ & \text { N్ } \\ & \text { م } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { N } \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { N } \\ & \text { م } \end{aligned}$ | $\begin{aligned} & \text { O } \\ & \text { 8 } \end{aligned}$ | $\begin{aligned} & \circ \\ & \hline 0 \\ & \hline- \end{aligned}$ | $\begin{aligned} & \circ \\ & \hline 8 \\ & \text { O} \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { N07 } \\ & \text { Ĥ } \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{8}{n} \\ & \stackrel{0}{\circ} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \stackrel{1}{n} \\ & \stackrel{0}{\gamma} \end{aligned}$ | $\begin{aligned} & \mathrm{B} \\ & \stackrel{1}{n} \\ & \stackrel{0}{8} \end{aligned}$ | $\begin{aligned} & 8 \\ & 8 \\ & \stackrel{0}{8} \end{aligned}$ | $\begin{aligned} & \mathrm{B} \\ & \stackrel{\rightharpoonup}{n} \\ & \stackrel{0}{8} \end{aligned}$ | O | 8 |
| $\begin{aligned} & 8 \\ & \infty \\ & \infty \\ & \infty \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 \\ & \infty \\ & \infty \\ & \infty \end{aligned}$ | $\begin{aligned} & 8 \\ & \infty_{0}^{\prime} \\ & \infty \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{\text { ® }}{2} \end{aligned}$ | $\begin{aligned} & 8 \\ & \infty \\ & \infty \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{0}{\infty} \\ & \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { م } \\ & \end{aligned}$ | $\begin{aligned} & 0 \\ & \stackrel{0}{\infty} \\ & \end{aligned}$ |  | $\begin{aligned} & 8 \\ & \text { O } \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { O} \\ & \text { y } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { O } \\ & \text { Y } \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 . \\ & 0 . \\ & \hline 0 \end{aligned}$ | $\begin{aligned} & \text { O} \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & 0 \\ & 0 \\ & \hline 0 \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { O- } \\ & \text { Nem } \end{aligned}$ | $\begin{aligned} & \circ \\ & \text { oi } \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { ò } \\ & \text { M } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { ర్ల } \\ & \text { R } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { N్ల } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { Ю్ల } \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { O } \\ & \text { Ю్ల } \\ & \hline 1 \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { Ю్ల } \\ & \text { n } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { U్ల } \\ & \text { N } \end{aligned}$ | O－ | O－ |
| $=$ | $=$ | $=$ |  |  |  |  | $=$ |  |  | $=$ |  |  | $=$ |  |  | $=$ |  |  | $=$ | $=$ | $=$ | $=$ | $=$ | $=$ | $=$ |
|  |  |  | 을 | $\begin{aligned} & \text { 을 } \\ & \frac{2}{2} \end{aligned}$ | $\frac{0 ㅡ ㄹ}{2}$ | $\frac{0}{2}$ |  |  | $\begin{aligned} & \text { © } \\ & \text { O} \\ & \text { 认 } \end{aligned}$ |  |  | $\begin{aligned} & \frac{\pi}{0} \\ & \text { 弟 } \end{aligned}$ |  |  | © © © |  |  | $\begin{aligned} & \frac{\pi}{0} \\ & \text { 弟 } \end{aligned}$ |  |  |  |  |  |  |  |


|  |  |  |  |  | $\begin{aligned} & \ddot{U} \\ & \stackrel{0}{\omega} \\ & \stackrel{0}{\overleftarrow{0}} \\ & \stackrel{\tilde{0}}{0} \end{aligned}$ |  |  |  | $\begin{aligned} & \text { N్N } \\ & 0.0 \\ & 0 \\ & 0 \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | $\begin{aligned} & \text { ᄃ } \\ & \text { N } \\ & \text { N} \\ & \text { ¿ } \end{aligned}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \circ \\ & \hline 0 \\ & \hline \end{aligned}$ | $\begin{array}{ll} \circ & \circ \\ \hline & 0 \\ 0 & -1 \end{array}$ | $\begin{aligned} & 8 \\ & 0 \\ & -1 \end{aligned}$ | $\begin{aligned} & \text { O} \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { in } \\ & 7 \end{aligned}$ | $\begin{aligned} & \circ \\ & 0 \\ & \infty \\ & \text { 가 } \end{aligned}$ | $\begin{aligned} & \text { B } \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \text { 유 } \\ & \text { on } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { O} \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \stackrel{y}{2} \end{aligned}$ | － | $\begin{aligned} & \circ \\ & \hline \infty \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \text { oi } \\ & \stackrel{y}{+} \end{aligned}$ | ¢ <br>  | 앙 <br> － | $\begin{aligned} & \circ \\ & \hline 8 \\ & 0 \end{aligned}$ | $\begin{aligned} & \stackrel{\sim}{0} \\ & \stackrel{\sim}{\mathrm{O}} \\ & \end{aligned}$ | N | $\begin{aligned} & \stackrel{1}{0} \\ & \text { にٌ } \\ & \stackrel{\sim}{n} \end{aligned}$ | N | 8 <br>  | $\begin{aligned} & \text { O} \\ & \text { O } \\ & \hline \end{aligned}$ |  | N | $\begin{aligned} & \text { 음 } \\ & \text { N } \end{aligned}$ | －8 | N |
| ¢0 | ¢ 0 | 0 |  | ¢ | 0） | 0 | 0 | 0 | ¢0 | － | － | 0 | $\vdash$ | － | 0 | ¢ | ¢0 | － |  | $\vdash$ | 0 | 0 | － | 0 | 0 | ¢ | ¢0 |
| $\begin{aligned} & \text { oे } \\ & \stackrel{0}{\mathrm{O}} \end{aligned}$ | $\begin{array}{ll} \stackrel{\circ}{\circ} & \stackrel{\circ}{0} \\ \stackrel{0}{0} \\ \text { Ni } \end{array}$ | $\begin{aligned} & \text { oे } \\ & \stackrel{\circ}{0} \end{aligned}$ |  |  |  |  | $\begin{aligned} & \text { ò } \\ & \stackrel{R}{N} \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \stackrel{\infty}{\infty} \\ & \hline \end{aligned}$ | $\stackrel{\stackrel{\rightharpoonup}{N}}{\underset{N}{N}}$ | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \stackrel{\infty}{\infty} \end{aligned}$ | $\stackrel{\stackrel{\sim}{\mathrm{N}}}{\mathrm{~N}}$ | $\begin{aligned} & \circ 0 \\ & \text { oi } \\ & \stackrel{0}{\circ} \end{aligned}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{\wedge} \\ & \underset{\sim}{2} \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \stackrel{0}{0} \end{aligned}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{\mathrm{N}} \\ & \underset{\sim}{n} \end{aligned}$ | $\stackrel{\stackrel{\sim}{\mathrm{N}}}{\substack{0}}$ | $\begin{aligned} & \text { 仓े } \\ & \text { Ù } \end{aligned}$ | $\begin{aligned} & \text { ò } \\ & \text { io } \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{\stackrel{ }{2}} \\ & \underset{-}{2} \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \stackrel{y}{0} \end{aligned}$ | $\underset{\underset{N}{\mathrm{~N}}}{\substack{\mathrm{~N} \\ \hline}}$ | $\begin{gathered} \stackrel{\text { N}}{\sim} \\ \underset{6}{2} \end{gathered}$ | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \text { G- } \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{0} \\ & \infty \\ & \text { in } \end{aligned}$ | $\begin{gathered} \stackrel{\rightharpoonup}{\mathrm{N}} \\ \underset{\sim}{2} \end{gathered}$ |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  | $\begin{gathered} \stackrel{\circ}{\circ} \\ \stackrel{\rightharpoonup}{6} \end{gathered}$ | － |  |  | $\begin{aligned} & \text { ò } \\ & \text { © } \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \text { ò } \\ & \stackrel{\sim}{\infty} \\ & \stackrel{\infty}{\circ} \end{aligned}$ | $\begin{gathered} \stackrel{\rightharpoonup}{\mathrm{O}} \end{gathered}$ | $\begin{gathered} \stackrel{\rightharpoonup}{\circ} \\ \stackrel{\rightharpoonup}{6} \end{gathered}$ |  |  | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \text { © } \\ & \text { مin } \end{aligned}$ | － |  |  |  |
| $\sum_{\sum}^{\infty}$ | $\sum_{\sum}^{\infty} \sum_{\sum}^{\infty}$ | $\sum_{\sum}^{\infty}$ | $\stackrel{\infty}{\infty}$ | $\stackrel{\infty}{\dot{\Sigma}}$ | $\stackrel{\circ}{\sum}_{\infty}^{\infty}$ | $\sum_{\sum}^{\infty}$ | $\begin{aligned} & \vec{\infty} \\ & \stackrel{0}{0} \\ & \stackrel{y}{\otimes} \\ & \ddot{\omega} \end{aligned}$ |  | $\begin{aligned} & \bar{\otimes} \\ & \stackrel{\rightharpoonup}{\omega} \end{aligned}$ |  | $\begin{aligned} & \bar{\Phi} \\ & \stackrel{\sim}{\omega} \end{aligned}$ |  | $\stackrel{\infty}{\stackrel{\circ}{ \pm}}$ | $\stackrel{\infty}{\square}$ |  | $\stackrel{-1}{\stackrel{1}{2}}$ | $\begin{aligned} & \infty \\ & \stackrel{\infty}{+} \\ & \stackrel{-}{2} \end{aligned}$ | $\begin{aligned} & \infty \\ & \stackrel{0}{\mathrm{O}} \\ & \stackrel{1}{1} \end{aligned}$ | $\frac{\infty}{\otimes}$ | $\stackrel{\circ}{8}$ | $\stackrel{-1}{8}$ $\stackrel{y}{2}$ 0 0 | $\begin{aligned} & \text {-1 } \\ & \hline \mathbf{y} \end{aligned}$ | $\begin{aligned} & \infty \\ & \stackrel{\infty}{-1} \\ & \stackrel{\rightharpoonup}{\dot{1}} \end{aligned}$ | $\begin{aligned} & \infty \\ & \stackrel{\infty}{-1} \\ & \stackrel{\rightharpoonup}{2} \end{aligned}$ | $\begin{aligned} & -1 \\ & \vdots \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | -1 <br> 0 <br> 0 <br> 0 <br> 0 | －1 <br> $\stackrel{1}{2}$ <br> $\stackrel{0}{0}$ <br> 0 |
| $\underset{\substack{\mathrm{N}}}{\substack{0}}$ |  | $\underset{\substack{\mathrm{N}}}{\substack{n}}$ | $\underset{\substack{\mathrm{N} \\ \hline}}{ }$ | $\stackrel{\substack{\mathrm{N}}}{\substack{2}}$ | ${ }^{\circ}$ | $\infty_{\infty}$ | $\stackrel{m}{m}$ | $\stackrel{m}{m}$ | ल | $\stackrel{m}{\text { m }}$ | $\stackrel{m}{m}$ | $\stackrel{m}{m}$ | $\stackrel{\infty}{6}$ | $\stackrel{\infty}{\circ}$ | $\stackrel{\sim}{\sim}$ | $\stackrel{\sim}{\sim}$ | $\stackrel{\sim}{\sim}$ | $\stackrel{\sim}{\sim}$ | $\stackrel{\sim}{\sim}$ | $\stackrel{\sim}{\sim}$ | $\stackrel{\infty}{6}$ | $\stackrel{\infty}{\circ}$ | $\stackrel{\infty}{6}$ | $\stackrel{\infty}{\oplus}$ | $\stackrel{\circ}{1}$ | $\bigcirc$ | $\bigcirc$ |
| $\underset{\sim}{\text { N }}$ | $\begin{array}{ll} \stackrel{\circ}{\mathrm{N}} & \stackrel{\rightharpoonup}{\mathrm{~N}} \end{array}$ | $\stackrel{8}{\mathrm{~N}}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\stackrel{8}{\mathrm{~N}}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\stackrel{8}{\mathrm{~N}}$ | $\begin{aligned} & \mathrm{B} \\ & \mathrm{~N} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\begin{aligned} & \mathrm{O} \\ & \text { N } \end{aligned}$ | $\underset{\sim}{\mathrm{N}}$ | $\begin{aligned} & \circ \\ & \mathrm{N} \end{aligned}$ | $\stackrel{8}{\mathrm{~N}}$ | $\underset{\sim}{\mathrm{N}}$ | $\stackrel{\stackrel{\rightharpoonup}{N}}{\substack{2}}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\stackrel{8}{\mathrm{~N}}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\underset{\sim}{\mathrm{N}}$ | $\underset{\sim}{\underset{\sim}{i}}$ | O | $\stackrel{\mathrm{O}}{\mathrm{~N}}$ | $\underset{\sim}{\mathrm{N}}$ | $\underset{\sim}{\mathrm{N}}$ | $\stackrel{\circ}{\circ}$ | $\stackrel{8}{\text { N }}$ |
| 단 |  | $\stackrel{\circ}{寸}$ | $\underset{\sim}{\underset{\sim}{c}}$ | $\stackrel{\sim}{\sim}$ | $\begin{aligned} & 0 \\ & \stackrel{0}{0} \end{aligned}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{0} \\ & \stackrel{y}{2} \end{aligned}$ | $\stackrel{\ominus}{N}$ | $\stackrel{\stackrel{\circ}{N}}{\underset{\sim}{c}}$ | $\stackrel{\infty}{N}$ | $\stackrel{0}{\mathrm{~N}}$ | $\stackrel{\infty}{N}$ | $$ | $\underset{\sim}{\circ}$ | $\stackrel{8}{\text {－}}$ | $\underset{\sim}{\stackrel{L}{2}}$ | $\stackrel{N}{\mathrm{~N}}$ | $\stackrel{\leftrightarrow}{0}$ | $\stackrel{\infty}{\stackrel{\infty}{m}}$ | $\stackrel{\circ}{\mathrm{m}}$ | $\stackrel{\circ}{-}$ | $\stackrel{\text { ¢ }}{\text { ¢ }}$ | $\underset{\substack{n}}{\stackrel{N}{2}}$ | $\stackrel{\leftrightarrow}{\circ}$ | $\stackrel{\infty}{\infty}$ | $\stackrel{\circ}{\circ}$ | $\stackrel{\text { J }}{\text { J }}$ | － |








| 238,00 | 215,00 | 620,00 | 13,50 | AP | 3,50 | 2,00 | 6.0 | C/80 | 1,74\% | BP | 10020 | Kaiser Franz Josef |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 238,00 | 215,00 | 620,00 | 13,50 | CP | 4,47 | 2,00 | 6.0 | C/80 | 6,23\% | BP | 10020 |  |
| 238,00 | 215,00 | 640,00 | 20,00 | AP | 3,50 | 2,00 | 6.0 | C/80 | 1,74\% | BP | 12965 | Maria Theresia |
| 238,00 | 215,00 | 640,00 | 20,00 | CP | 4,47 | 2,00 | 6.0 | C/80 | 6,23\% | BP | 12965 |  |
| 235,40 | 132,50 | 600,00 | 10,00 | AP | 2,79 | 2,00 | 8,0 |  | 2,26\% | BP | 6700 | Tegetthoff (as re-armed) |
| 235,40 | 119,50 | 630,00 | 10,00 | Common | 2,30 | 2,00 | 8,0 |  | 5,69\% | BP | 6800 |  |
| 235,40 | 132,50 | 600,00 | 20,00 | HC | 2,90 | 2,00 | 8,0 | M. 98 | 2,26\% | BP | 10000 |  |
| 235,40 | 132,50 | 433,00 | 9,00 | AP | 2,26 | 2,00 | 3.5 |  | 2,26\% | BP | 4230 | Albrecht |
| 235,40 | 119,50 | 455,00 | 9,00 | Common | 2,30 | 2,00 | 3.5 |  | 5,69\% | BP | 4380 |  |
| 235,40 | 132,50 | 483,00 | 9,00 | AP | 2,26 | 2,00 | 3.5 |  | 2,26\% | BP | 4830 |  |
| 235,40 | 119,50 | 508,00 | 9,00 | Common | 2,30 | 2,00 | 3.5 |  | 5,69\% | BP | 4980 |  |
| 235,40 | 132,50 | 510,00 | 35,00 | AP | 2,26 | 2,00 | 8,0 |  | 2,26\% | BP | 11200 | Coast Defence |
| 235,40 | 132,50 | 510,00 | 35,00 | HC | 2,90 | 2,00 | 8,0 | M. 98 |  | PA | 11200 |  |
| 235,40 | 140,00 | 410,00 | 9,00 | AP | 2,26 | 2,00 | 3,5 | Gruson | 1,21\% | BP | 4070 | Lissa |
| 234,50 | 132,50 | 420,00 | 9,00 | AP | 2,26 | 2,00 | 3,5 | Steel | 2,26\% | BP | 4070 |  |
| 235,40 | 119,50 | 410,00 | 9,00 | Common | 2,30 | 2,00 | 3,5 |  | 5,69\% | BP | 3870 |  |
| 235,40 | 132,50 | 483,00 | 20,00 | AP | 2,26 | 2,00 | 8,0 |  | 2,26\% | BP | 10200 | Coast Defence |
| 235,40 | 132,50 | 483,00 | 20,00 | HC | 2,90 | 2,00 | 8,0 | M. 98 | 5,13\% | BP | 10200 |  |
| 228,60 | 116,12 | 432,82 | 12,00 | AP | 2,28 | 2,00 | 3.0 | Palliser |  |  | 5081 | Kaiser (rebuilt) |
| 228,60 | 113,40 |  | 12,00 | Common | 2,60 | 2,00 | 3.0 |  | 7,60\% | BP | 5042 |  |
| 228,60 | 115,98 |  | 12,00 | AP Shell |  | 2,00 | 3.0 | Palliser | 2,33\% | BP |  |  |
| 228,60 | 120,02 | 361,00 | 12,00 | Common |  | 2,00 | 3.0 |  | 6,99\% | BP |  |  |
| 209,30 | 94,00 | 463,00 | 12,00 | AP | 2,36 | 2,00 | 2.5 | Steel Gruson | 2,13\% | BP | 5600 | Kaiser Max (II), Fasana |
| 209,30 | 89,00 | 483,00 | 12,00 | AP | 2,50 | 2,00 | 2.5 | chilled | 1,35\% | BP | 5400 |  |
| 209,30 | 78,00 | 435,00 | 12,00 | Common | 2,38 | 2,00 | 2.5 |  | 6,03\% | BP | 4700 |  |
| 209,30 | 94,00 | 500,00 | 12,00 | CP | 2,93 | 2,00 | 4,0 | C/98 |  | PA | 5900 | Coast Defence |
| 209,30 | 78,00 | 545,00 | 12,00 | CP | 2,84 | 2,00 | 4,0 | $\begin{gathered} \text { C/99 } \\ \text { Gruson } \end{gathered}$ | 9,62\% | PA | 6000 |  |
| 209,30 | 89,00 | 335,00 | 12,75 | AP | 2,50 | 2,00 | 2.5 | chilled | 1,35\% | BP | 3900 |  |
| 209,30 | 78,00 | 311,00 | 12,75 | Common | 2,40 | 2,00 | 2.5 |  | 6,03\% | BP | 3440 |  |
| 190,00 | 97,00 | 850,00 | 30,00 | APCBC | 4,00 | 10,00 | 6.8 |  |  |  | 26500 | Cruiser Plan VII |




| $\stackrel{\infty}{\dot{\Sigma}}$ | $\sum_{\Sigma}^{\omega}$ | $\stackrel{\circ}{\dot{\Sigma}}$ | $\sum_{\sum}^{\infty}$ | $\stackrel{\infty}{\stackrel{\infty}{\Sigma}}$ | $\sum_{\Sigma}^{\infty}$ | $\underset{\sum}{\infty}$ | $\sum_{\sum}^{\infty}$ | $\sum_{\sum}^{\infty}$ | $\begin{aligned} & \bar{\Psi} \\ & \stackrel{\sim}{*} \end{aligned}$ | $\stackrel{\infty}{\sum}$ | $\sum_{\sum}^{\infty}$ | $\begin{aligned} & \bar{\otimes} \\ & \stackrel{\sim}{*} \end{aligned}$ | $\stackrel{\infty}{\stackrel{\infty}{\Sigma}}$ |  | $\begin{aligned} & \bar{凶} \\ & \stackrel{\oplus}{\omega} \end{aligned}$ |  |  | $\stackrel{\infty}{\stackrel{\infty}{\Sigma}}$ | $\dot{B}_{\dot{0}}^{0}$ |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\stackrel{\bigcirc}{+}$ | $\stackrel{\bigcirc}{+}$ | $\stackrel{\bigcirc}{\square}$ | คٌ | คึ่ | $\stackrel{\sim}{\circ}$ | คั่ | คั | $\stackrel{\sim}{\circ}$ | $\stackrel{\sim}{\text { ¢ }}$ | $\bigcirc$ | $\stackrel{\square}{1}$ | $\stackrel{\sim}{1}$ | $\stackrel{\circ}{1}$ | $\bigcirc$ | $\stackrel{\sim}{1}$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\stackrel{\text {－}}{ }$ | $\stackrel{\sim}{\text { ¢ }}$ | $\stackrel{\square}{0}$ | $\stackrel{\square}{\text { ¢ }}$ | $\stackrel{\square}{\text { M }}$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |
| $\stackrel{\stackrel{\rightharpoonup}{\mathrm{N}}}{ }$ | $\underset{\sim}{\mathrm{N}}$ | $\stackrel{8}{\mathrm{~N}}$ | $\underset{\sim}{\mathrm{N}}$ | $\underset{\sim}{\mathrm{N}}$ | $\underset{\sim}{\mathrm{N}}$ | $\underset{\sim}{\mathrm{N}}$ | $\stackrel{\text { ® }}{\sim}$ | $\underset{\sim}{\mathrm{N}}$ | $\underset{\sim}{\mathrm{N}}$ | $\underset{\sim}{\mathrm{N}}$ | $\underset{\sim}{\mathrm{N}}$ | $\underset{\sim}{\mathrm{N}}$ | $\underset{\sim}{\mathrm{N}}$ | $\stackrel{\stackrel{\rightharpoonup}{N}}{ }$ | $\underset{\mathrm{N}}{\mathrm{~N}}$ | $\underset{\sim}{\mathrm{N}}$ | $\stackrel{\mathrm{O}}{\mathrm{~N}}$ | $\stackrel{8}{\mathrm{~N}}$ | $\stackrel{\mathrm{O}}{\mathrm{~N}}$ | $\stackrel{\circ}{\circ}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ |  | $\underset{\sim}{\mathrm{O}}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\stackrel{8}{\mathrm{~N}}$ | － |
| $\underset{\sim}{\underset{j}{n}}$ | $\stackrel{\circ}{\sim}$ | $\stackrel{\sim}{\sim}$ | $\stackrel{\infty}{\infty}$ | $\stackrel{N}{N}$ | $\stackrel{\circ}{0}$ | $\stackrel{\stackrel{\rightharpoonup}{N}}{\underset{N}{2}}$ | $\stackrel{\circ}{\mathrm{O}}$ | $\stackrel{\underset{i}{i}}{ }$ |  | $\stackrel{\stackrel{N}{N}}{ }$ | ষ্ণ |  | $\stackrel{\circ}{N}$ |  | $\stackrel{8}{\mathrm{i}}$ | $\stackrel{\ominus}{i}$ | $\underset{\sim}{\underset{\sim}{i}}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\underset{\sim}{\sim}$ | $\begin{aligned} & \stackrel{\circ}{\infty} \\ & \stackrel{N}{+} \end{aligned}$ | $\stackrel{\mathrm{O}}{\underset{\sim}{2}}$ | $\stackrel{\infty}{\infty}$ | $\stackrel{\stackrel{\rightharpoonup}{\mathrm{N}}}{\mathrm{~m}}$ | $\stackrel{\curvearrowleft}{\sim}$ | $\stackrel{\circ}{\text { ® }}$ | $\stackrel{\circ}{\text { ก－}}$ |
| $\begin{aligned} & \text { ㄷ } \\ & \text { 的 } \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 0 \\ & \frac{0}{4} \end{aligned}$ | ㄴ | ¢ |  | $\begin{aligned} & 0 \\ & \frac{0}{4} \end{aligned}$ |  | $\begin{aligned} & 0 \\ & \frac{0}{4} \end{aligned}$ |  | ¢ |  |  | $\stackrel{\square}{8}$ |  | $\begin{aligned} & \text { O} \\ & \text { O} \\ & \text { E } \\ & 0 \end{aligned}$ | $\stackrel{\square}{4}$ | $\begin{aligned} & \text { O} \\ & \text { O} \\ & \text { EO } \\ & 0 \end{aligned}$ | ¢ | $\begin{aligned} & \text { Co } \\ & \text { E } \\ & \text { EO } \\ & 0 \end{aligned}$ |  | $\begin{aligned} & 0 \\ & 0 \\ & 0 \end{aligned}$ | $\frac{\square}{4}$ | 0 | $\stackrel{\square}{4}$ | 0 | 号 | 0 | ¢ 0 |
| $\begin{aligned} & \stackrel{8}{\circ} \\ & \stackrel{\rightharpoonup}{1} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \stackrel{-}{9} \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{8}{0} \\ & \text { - } \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { in } \\ & \text { 俍 } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \stackrel{1}{\text { N }} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \stackrel{\sim}{n} \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{8}{7} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { Nin } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { Ni } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \underset{\sim}{\sim} \end{aligned}$ | $\begin{aligned} & \text { Bn } \\ & \underset{\sim}{7} \end{aligned}$ | $\begin{aligned} & \text { Bn } \\ & \underset{\sim}{7} \end{aligned}$ | $$ | $\begin{aligned} & \circ \\ & \stackrel{0}{7} \end{aligned}$ | $\begin{aligned} & \text { Bn } \\ & \underset{\sim}{7} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \stackrel{\sim}{n} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \underset{\sim}{\prime} \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{8}{\mathrm{j}} \end{aligned}$ | $\begin{aligned} & 8 \\ & \underset{\sim}{\prime} \end{aligned}$ | $\begin{aligned} & 8 \\ & \hline \text { - } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { - } \end{aligned}$ | $\begin{aligned} & \text { O- } \\ & \text { o- } \end{aligned}$ | $\begin{aligned} & \text { O- } \\ & \text { o- } \end{aligned}$ |  | $\begin{aligned} & \text { O} \\ & \text { o- } \end{aligned}$ | $\begin{aligned} & \text { O- } \\ & \text { o- } \end{aligned}$ | $\begin{array}{ll} \mathrm{O} \\ \stackrel{\rightharpoonup}{N} & \stackrel{\rightharpoonup}{N} \\ \hline \end{array}$ |
| $\begin{aligned} & \circ \\ & \stackrel{0}{0} \\ & 0.0 \end{aligned}$ | $\begin{aligned} & \circ \\ & 0 . \\ & 0 . \\ & 0 \end{aligned}$ | $\begin{aligned} & 8 \\ & 0.0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 8 \\ & 8 . \\ & 8 \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{H}{0} \\ & \text { in } \end{aligned}$ | $\begin{aligned} & 8 \\ & 8 \\ & 8 \\ & \hline \end{aligned}$ | $\begin{aligned} & 8 \\ & 8 \\ & \hline 0 \end{aligned}$ | $\begin{aligned} & 8 \\ & 8 \\ & \hline 0 \end{aligned}$ | $\begin{aligned} & 8 \\ & 8 \\ & 8 \\ & \hline \end{aligned}$ | $\begin{aligned} & \stackrel{8}{0} \\ & \stackrel{0}{f} \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{8}{\circ} \\ & \text { gin } \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{\rightharpoonup}{N} \\ & \text { in } \end{aligned}$ | $\begin{aligned} & 8 \\ & \hline-8 \\ & \hline 0 \end{aligned}$ | $\begin{aligned} & \text { B } \\ & \text { N్N } \\ & \text { in } \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{-}{N} \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{0}{\circ} \\ & \stackrel{y}{2} \end{aligned}$ | $\begin{gathered} 8 \\ \underset{\sim}{N} \end{gathered}$ | $\begin{aligned} & 8 \\ & \hline \text { B } \\ & \text { B } \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { B. } \\ & \text { - } \end{aligned}$ | $\begin{aligned} & \mathrm{B} \\ & \text { - } \\ & \text {. } \end{aligned}$ | $\begin{aligned} & \circ \\ & \hline- \\ & 0 . \\ & \hline \infty \end{aligned}$ | $\begin{aligned} & \circ \\ & \hline- \\ & \hline \end{aligned}$ | $\begin{aligned} & 8 \\ & 8 \\ & \hline \end{aligned}$ | $\underset{\underset{6}{\circ}}{\substack{\mathrm{O} \\ \hline}}$ | $\underset{\substack{\mathrm{N} \\ \hline \\ \hline}}{ }$ | $\begin{aligned} & 8 \\ & \hline 0 \\ & \hline 8 \end{aligned}$ | $\begin{aligned} & 8 \\ & 0.0 \\ & 0 \end{aligned}$ | $\begin{array}{ll} \hline 8 & 8 \\ \hline-0 \\ \hline 0 \\ \hline 0 \\ \hline 0 \end{array}$ |
| $\begin{aligned} & \text { On} \\ & \text { in } \\ & \text { Lis } \end{aligned}$ | $\begin{aligned} & \text { in } \\ & \text { ig } \end{aligned}$ | $\begin{aligned} & \text { ion } \\ & \text { in } \\ & \text { 号 } \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{-j} \\ & \text { in } \end{aligned}$ | $\begin{gathered} \mathrm{p} \\ \stackrel{-}{\mathrm{N}} \end{gathered}$ | $\stackrel{\otimes}{-0}$ | $\stackrel{\circ}{\circ}$ | $\stackrel{\otimes}{\mathbf{\circ}}$ | $\stackrel{\otimes}{\circ}$ | $\begin{aligned} & \text { in } \\ & \infty \\ & \infty \\ & \hline 0 \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{0} \\ & \stackrel{N}{\sim} \end{aligned}$ | $\begin{gathered} \stackrel{\circ}{2} \\ \stackrel{y}{m} \end{gathered}$ | ৪ | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \stackrel{N}{N} \end{aligned}$ | $\begin{aligned} & \text { م우 } \\ & \stackrel{0}{2} \end{aligned}$ | $\begin{aligned} & \text { On } \\ & \text { مip } \end{aligned}$ | $\begin{aligned} & \text { م } \\ & \stackrel{0}{7} \end{aligned}$ | $\begin{aligned} & \text { مిN } \\ & \text { Non } \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{0} \\ & \stackrel{N}{\mathrm{~N}} \end{aligned}$ | $\stackrel{\circ}{\stackrel{\circ}{N}}$ | $\stackrel{\otimes}{\infty}$ | $\begin{aligned} & \infty \\ & \underset{\sim}{\circ} \end{aligned}$ | $\begin{aligned} & \infty \\ & \underset{\sim}{\infty} \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{\infty} \\ & \stackrel{N}{N} \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{\infty} \\ & \underset{\sim}{2} \end{aligned}$ | $\stackrel{\circ}{\sim}$ | $\begin{aligned} & \infty \\ & \stackrel{\sim}{\sim} \end{aligned}$ | $\begin{array}{ll} \hline \stackrel{O}{\mathrm{O}} \\ \stackrel{\sim}{\mathrm{~N}} \end{array}$ |
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| Krupp | $15 \mathrm{~cm} \mathrm{G}. \mathrm{U/35} \mathrm{K/80}$ |
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| Krupp | $15 \mathrm{~cm} \mathrm{G}. \mathrm{L/26} \mathrm{C/72}$ |
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| Krupp | $15 \mathrm{~cm} \mathrm{G}. \mathrm{L/26} \mathrm{C/78}$ |
|  | ＂ |
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| Uchatius | 15cm G．L／25 M． 80 |
|  | ＂ |
| Wahrendorf | $\begin{aligned} & 15 \mathrm{~cm} \text { G.L/21 M. } 61 \text { (24- } \\ & \mathrm{pdr}) \end{aligned}$ |
|  | ＂ |
|  | ＂ |
| Skoda | $12 \mathrm{~cm} \mathrm{G}. \mathrm{L/45} \mathrm{K/14}$ |
| Skoda | $12 \mathrm{~cm} \mathrm{G} \mathrm{ப} 40 \mathrm{~K} /$. |
|  | ， |
| Skoda | 12cm G．L／35 K／04 |
|  | ＂ |
| Krupp | 12cm G．L／35 C／93 |
|  | ＂ |
| Krupp | 12cm G．L／35 C／87 |
|  | ． |

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|  | ＂ | 120，00 | 23，80 | 650，00 | 25，00 | AP | 2，85 | 2，00 | 3.0 |
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|  | ＂ | 120，00 | 23，80 | 650，00 | 25，00 | CP | 3，10 | 2，00 | 3.0 |
| Krupp | $12 \mathrm{~cm} \mathrm{G} \mathrm{~L} 35 \mathrm{C} /$. | 120，00 | 26，00 | 530，00 | 25，00 | AP | 3，48 | 2，00 | 3.0 |
|  | ＂ | 120，00 | 26，00 | 530，00 | 25，00 | Common | 4，21 | 2，00 | 3.0 |
| Uchatius | 12cm G．L／36．5 M． 87 | 120，00 | 26，00 | 535，00 | 25，00 | AP | 3，48 | 2，00 | 3.0 |
|  | ＂ | 120，00 | 26，00 | 535，00 | 25，00 | Common | 4，21 | 2，00 | 3.0 |
| Uchatius | 12cm G．L／35 M． 87 | 120，00 | 26，00 | 535，00 | 25，00 | AP | 3，48 | 2，00 | 3.0 |
|  | 12cm G．L／23 M． 61 （12－ | 120，00 | 26，00 | 535，00 | 25，00 | Common | 4，21 | 2，00 | 3.0 |
| Wahrendorff | pdr） | 121，92 | 20，00 | 332，00 | 14，00 | AP | 2，80 | 2，00 | 3.0 |
|  |  | 121，92 | 15，00 | 321，00 | 14，00 | Common | 2，30 | 2，00 | 3.0 |
|  | $10 \mathrm{~cm} \mathrm{L/19.4} \mathrm{M.63} \mathrm{(8-}$ pdr） | 106，10 | 11，00 | 305，00 | 9，50 | Common |  | 2，00 | 3.0 |
| Skoda | $10 \mathrm{~cm} \mathrm{~L} / 50 \mathrm{~K} / 11$ <br> 10 cm L／50 K／07 \＆ | 100，00 | 13，75 | 900，00 | 18，00 | CP | 4，20 | 4，00 | 3.9 |
| Skoda | $\begin{aligned} & \mathrm{K} / 10 \\ & 9 \mathrm{~cm} \text { G. L/45 K/13 } \end{aligned}$ | 100，00 | 13，75 | 880，00 | 14，00 | CP | 4，20 | 4，00 | 3.7 |
| Skoda | BAG | 90，00 | 10，20 | 780，00 | 70，00 | CP | 4，20 | 3，00 | 5.0 |
| Skoda | $9 \mathrm{~cm} \mathrm{G}. \mathrm{L/45} \mathrm{K/12} \mathrm{TAG}$ | 90，00 | 10，20 | 840，00 | 30，00 | CP | 4，20 | 3，00 | 5.3 |
| Uchatius | 9 cm G．L／24 M． 75 $8 \mathrm{~cm} \mathrm{L/19.5} \mathrm{M}$.63 （4－ | 87，00 | 6，45 | 448，00 | 15，00 | CP | 2，74 | 2，00 | 4.4 |
| Finspong <br> Wahrendorff | pdr） <br> 8 cm G．L／20．1 M． 61 （3－ | 87，00 | 5，75 | 284，00 | 19，00 | Common | 2，87 | 2，00 |  |
|  | pdr） | 83，30 | 4，70 | 370，00 | 14，00 | Common | 2，00 | 2，00 |  |
| Wahrendorff | GREAT BRITAIN |  |  |  |  |  |  |  |  |
|  | 18＂／40 Mk． 1 | 457，20 | 1505，94 | 737，62 | 30，00 | APC | 3，74 | 4，00 | 8.08 |
|  | ＂ | 457，20 | 1505，94 | 737，62 | 30，00 | CPC | 4，21 | 4，00 | 8.08 |
|  | ＂ | 457，20 | 1505，94 | 737，62 | 30，00 | APCBC | 4，43 | 8，00 | 8.08 |
|  | ＂ | 457，20 | 1322,69 | 787，06 | 30，00 | APCBC | 4，14 | 6，00 | 8.08 |
|  | 18＂／45 Mk．II | 457，20 | 1322,69 | 807，72 | 40，00 | APCBC | 4，14 | 6，00 | 8.84 |
|  | ＂ | 457，20 | 1505，94 | 757，00 | 40，00 | APCBC | 4，43 | 8，00 | 8.84 |
|  | 16＂／45 Mk．I | 406，40 | 928，97 | 788，21 | 40，00 | APCBC | 4，14 | 6，00 | 8.84 |


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|  | " | 342,90 | 639,57 | 756,52 | 20,00 | APC | 3,64 | 4,00 | 7.01 | Mk. II a | 11,30\% | 2,34\% | S | 21589 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vickers | 13.5"/45 Mk. VI | 342,90 | 635,04 | 745,24 | 20,00 | APC | 3,88 | 4,00 | 6.7 |  |  |  | L | 21132 | Erin |
|  | " | 342,90 | 635,04 | 745,24 | 20,00 | CPC | 4,86 | 4,00 | 6.7 |  |  |  | L | 21132 |  |
|  | " | 342,90 | 639,57 | 742,59 | 20,00 | APC | 3,64 | 4,00 | 6.7 | Mk. II a | 11,50\% | 2,34\% | S | 21029 |  |
|  | 12"/35.5 Mk. VIII | 304,80 | 385,56 | 736,70 | 13,50 | AP | 3,16 | 2,00 | 7.01 | Mk. 1 |  | 5,68\% | BP | 12993 | Majestic, Canopus |
|  | " Cordite | 304,80 | 385,56 | 736,70 | 13,50 | CP | 3,80 | 2,00 | 7.01 |  |  | 9,43\% | BP | 12993 |  |
|  | MD | 304,80 | 385,56 | 723,90 | 13,50 | AP | 3,16 | 2,00 | 7.01 | Mk. 1 |  | 5,68\% | BP | 12710 |  |
|  | MD | 304,80 | 385,56 | 723,90 | 13,50 | CP | 3,80 | 2,00 | 7.01 |  |  | 9,43\% | BP | 12710 |  |
|  | " MD | 304,80 | 385,56 | 723,90 | 30,00 | CPC | 4,03 | 3,00 | 7.01 |  | 3,53\% | 9,41\% | BP | 20912 | Monitors during WW I |
|  | MD | 304,80 | 385,56 | 723,90 | 30,00 | HE | 4,03 | 3,00 | 7.01 |  |  | 12,59\% | L | 20912 |  |
|  | 12"/40 Mk. IX (s) | 304,80 | 385,56 | 796,14 | 13,50 | APC | 3,50 | 2,00 | 7.01 | Mk. IV | 3,33\% | 2,01\% | L | 14265 | King Edward VII |
|  | " | 304,80 | 385,56 | 796,14 | 13,50 | CP | 3,80 | 2,00 | 7.01 |  |  | 9,42\% | BP | 14307 |  |
|  | " | 304,80 | 389,84 | 791,57 | 30,00 | APC | 3,30 | 3,00 | 7.01 | Mk. VI a | 3,71\% | 3,08\% | L | 24231 |  |
|  | " | 304,80 | 385,56 | 796,14 | 30,00 | CPC | 4,03 | 3,00 | 7.01 |  |  | 9,41\% | BP | 24232 |  |
|  | $12 / 40 \mathrm{Mk}$. IX | 304,80 | 385,56 | 777,85 | 13,50 | AP | 3,16 | 2,00 | 7.01 | Mk. II |  | 5,68\% | BP | 13902 | Formidable, London, Duncan |
|  | " | 304,80 | 385,56 | 777,85 | 13,50 | CP | 3,80 | 2,00 | 7.01 |  |  | 9,42\% | BP | 13902 |  |
|  | " | 304,80 | 385,56 | 777,85 | 13,50 | APC | 3,50 | 2,00 | 7.01 | Mk. III | 3,33\% | 2,01\% | BP | 13853 |  |
|  | 12"/45 Mk. X | 304,80 | 385,56 | 830,58 | 13,50 | APC | 3,50 | 2,00 | 6.71 | Mk. IV | 3,33\% | 2,01\% | BP | 15042 | Dreadnought, Bellerophon, Invincible Indefatigable, Lord |
|  | " | 304,80 | 385,56 | 830,58 | 13,50 | CP | 3,80 | 2,00 | 6.71 |  |  | 9,42\% | BP | 15067 | Nelson |
|  | " | 304,80 | 385,56 | 830,58 | 13,50 | APC | 3,30 | 3,00 | 6.71 | Mk. IV a | 3,53\% | 3,10\% | BP | 16880 |  |
|  | " | 304,80 | 389,84 | 826,01 | 13,50 | APC | 3,30 | 3,00 | 6.71 | Mk. VI a | 3,49\% | 3,08\% | L | 17069 |  |
|  | " | 304,80 | 388,28 | 827,53 | 13,50 | APC | 3,17 | 3,00 | 6.71 | Mk. VII a | 12,04\% | 2,37\% | S | 17237 |  |
|  | " | 304,80 | 385,56 | 830,58 | 13,50 | CPC | 4,03 | 3,00 | 6.71 |  |  | 9,41\% | BP | 17236 |  |
|  | " | 304,80 | 398,20 | 807,72 | 13,50 | APCBC | 3,90 | 8,00 | 6.71 | Mk. VIII b |  | 2,50\% | S | 19320 |  |
|  | 12"/50 Mk. XI | 304,80 | 389,81 | 864,41 | 15,00 | APC | 3,30 | 3,00 | 6.71 | Mk. V a | 3,71\% | 3,07\% | L | 19385 | St. Vincent, Neptune, Colossus |
|  | " | 304,80 | 388,28 | 866,24 | 15,00 | APC | 3,17 | 4,00 | 6.71 | Mk. VII a | 12,04\% | 2,37\% | S | 19406 |  |
|  | " | 304,80 | 385,56 | 869,29 | 15,00 | CPC | 4,03 | 3,00 | 6.71 |  |  | 9,41\% | BP | 19391 |  |
|  | " | 304,80 | 398,20 | 845,82 | 15,00 | APCBC | 3,90 | 8,00 | 6.71 | Mk. VIII b |  | 2,50\% | S | 22109 |  |
| EOC | 12"/45 Mk. XIII | 304,80 | 385,56 | 830,58 | 13,50 | APC | 3,30 | 4,00 | 7.54 |  |  |  |  | 17210 | Agincourt |

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|  | 8"/50 Mk. IX | 203,20 | 131,54 | 813,82 | 45,00 | SAPCBC | 5,00 | 6,00 | 6.17 | Mks I, II, <br> III | 28621 |  |  |  |
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|  | 7.5"/45 Mk. I | 190,50 | 90,72 | 842,77 | 15,00 | APC | 3,85 | 2,00 | 6.09 |  | 2,00\% | BP | 12809 | Hampshire |
|  | " | 190,50 | 90,72 | 842,77 | 15,00 | CP | 3,70 | 2,00 | 6.09 | Mks I \& II | 7,81\% | BP | 12809 |  |
|  | " | 190,50 | 90,72 | 842,77 | 15,00 | APC | 3,85 | 3,00 | 6.09 |  |  |  | 13913 |  |
|  | " | 190,50 | 90,72 | 842,77 | 15,00 | CPC | 3,83 | 3,00 | 6.09 |  |  |  | 13913 |  |
|  | 7.5"/50 Mk. II | 190,50 | 90,72 | 861,67 | 15,00 | APC | 3,85 | 2,00 | 6.09 | Mks I, II, III | 2,00\% | BP | 13101 |  |
|  | " | 190,50 | 90,72 | 861,67 | 15,00 | CP | 3,70 | 2,00 | 6.09 | Mks I \& II | 7,81\% | BP | 13101 |  |
|  | " | 190,50 | 90,72 | 861,67 | 15,00 | APC | 3,85 | 3,00 | 5.64 | Mk IIla | 2,00\% | BP | 14238 | Achilles, Minotaur |
|  | " | 190,50 | 90,72 | 861,67 | 15,00 | CPC | 3,83 | 3,00 | 5.64 | Mk IIIa | 8,12\% | L | 14238 |  |
|  | " | 190,50 | 90,72 | 861,67 | 15,00 | APC | 3,85 | 3,00 | 5.64 | Mk IVa | 3,25\% | L | 14238 |  |
|  | " | 190,50 | 90,72 | 861,67 | 15,00 | CPC | 3,83 | 3,00 | 5.64 | Mk III*a | 8,12\% | S | 14238 |  |
| EOC \& VSM | 7.5"/50 Mks. III \& IV | 190,50 | 90,72 | 847,65 | 15,00 | APC Shot |  | 2,00 | 4,01 |  |  | BP | 12882 | Swiftsure \& Triumph |
|  | " | 190,50 | 90,72 | 847,65 | 15,00 | APC Shell |  | 2,00 | 4,01 |  |  | BP | 12882 |  |
|  | " | 190,50 | 90,72 | 847,65 | 15,00 | Common |  | 2,00 | 4,01 |  |  | BP | 12882 |  |
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|  | " | 190,50 | 90,72 | 847,65 | 15,00 | HE | 3,96 | 4,00 | 4,01 |  | 11,50\% | L | 13999 |  |
|  | 7.5"/45 Mk. VI | 190,50 | 90,72 | 844,30 | 30,00 | CPC | 3,83 | 3,00 | 6.09 | Mk III*a | 8,12\% | S | 19307 | Hawkins |
|  | " | 190,50 | 90,72 | 844,30 | 30,00 | APC | 3,85 | 3,00 | 6.09 | Mk III*a Mk la | 3,25\% | L | 19307 |  |
|  | " | 190,50 | 90,72 | 844,30 | 30,00 | SAPC | 4,00 | 3,00 | 6.09 | (1928) | 5,00\% | T | 19307 |  |
|  | 6"/40 QF Mks. I-III | 152,40 | 45,36 | 573,63 | 15,00 | AP | 3,21 | 2,00 | 2.59 | AP Mks II - IV CP Mks I | 5,50\% | BP | 7786 | Royal Soveriegn to $\mathrm{Ca}-$ nopus, Edgar to Diadem \& re-armed Blake |
|  | " EXE | 152,40 | 45,36 | 573,63 | 15,00 | CP |  | 2,00 | 2.59 | - III AP Mks II | 9,25\% | BP | 7786 | (casemates) <br> Diadem, re-armed |
|  | " EXE | 152,40 | 45,36 | 573,63 | 20,00 | AP | 3,21 | 2,00 | 2.59 | - IV <br> CP Mks I | 5,50\% | BP | 9138 | Blake, Aeolus, Brilliant, Highflyer, re-armed |
|  | " EXE | 152,40 | 45,36 | 573,63 | 20,00 | CP |  | 2,00 | 2.59 | - III <br> AP Mks II | 9,25\% | BP | 9138 | Hercules (deck mounts) |
|  | " EXE | 152,40 | 45,36 | 573,63 | 19,00 | AP | 3,21 | 2,00 | 2.59 | - IV CP Mks I | 5,50\% | BP | 8889 |  |
|  | " EXE | 152,40 | 45,36 | 573,63 | 19,00 | CP |  | 2,00 | 2.59 | - III <br> AP Mks II | 9,25\% | BP | 8889 |  |
|  | " Cordite | 152,40 | 45,36 | 679,71 | 15,00 | AP | 3,21 | 2,00 | 2.59 | - IV <br> CP Mks I | 5,50\% | BP | 9144 |  |
|  | " Cordite | 152,40 | 45,36 | 679,71 | 15,00 | CP |  | 2,00 | 2.59 | - III | 9,25\% | BP | 9144 |  |

Monitors during WW I
Formidable, London,
Duncan, Cressy, Drake,
Monmouth, re-armed
Barfleur class
Tiger, Iron Duke class
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| $\stackrel{\ominus}{\oplus}$ | $\begin{aligned} & \varrho \\ & \end{aligned}$ | $\stackrel{\ominus}{\text { ले }}$ | $\stackrel{\varrho}{\infty}$ | $\begin{aligned} & \varrho \\ & \end{aligned}$ | $\stackrel{\varphi}{\text { ¢ }}$ | $\stackrel{\ominus}{\oplus}$ | ¢ |  | $\begin{aligned} & \circ \\ & \text { M } \end{aligned}$ | $\stackrel{\ominus}{\dot{M}}$ | $\begin{aligned} & \circ \\ & \text { © } \end{aligned}$ | $\begin{aligned} & \text { ¢ } \\ & \text { M } \end{aligned}$ | ○. | $\begin{aligned} & \circ \\ & \text { M } \end{aligned}$ | $\underset{\sim}{\underset{\sim}{N}}$ | $\stackrel{N}{\sim}$ | $\stackrel{\sim}{\sim}$ | $\stackrel{N}{\sim}$ | $\underset{\sim}{\underset{\sim}{\sim}}$ | $\underset{\sim}{\underset{\sim}{+}}$ | $\underset{\sim}{\underset{\sim}{N}}$ | $\stackrel{\sim}{\sim}$ | $\stackrel{N}{\sim}$ |
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| 0 | $\begin{aligned} & \text { U } \\ & \text { 足 } \end{aligned}$ | $\begin{aligned} & u \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { U } \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & \text { U } \\ & \text { 足 } \end{aligned}$ | $\begin{aligned} & \text { U } \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 0 \\ & \text { Q } \end{aligned}$ | $\begin{aligned} & u \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 0 \\ & \text { Q } \end{aligned}$ | $\begin{aligned} & \text { U } \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & \text { U } \\ & \text { 足 } \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & \text { U } \\ & \frac{0}{4} \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & \text { U } \\ & \text { 足 } \end{aligned}$ | $\begin{aligned} & \text { u } \\ & \text { U } \end{aligned}$ | $\begin{aligned} & \text { U } \\ & \text { 足 } \end{aligned}$ | $\begin{aligned} & \text { U } \\ & \text { OU } \end{aligned}$ | $\begin{aligned} & u \\ & \text { 足 } \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \\ & 0 \end{aligned}$ | U | $\begin{aligned} & u \\ & 0 \\ & 0 \end{aligned}$ | U |
| $\begin{aligned} & 8 \\ & 0 \\ & \text { ni } \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{0}{0} \\ & \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 \\ & 1 \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{8}{1} \end{aligned}$ | B- | $\begin{aligned} & \mathrm{B} \\ & \text { ì } \end{aligned}$ | 8 <br> － | $\begin{aligned} & 8 \\ & \text { Bi } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { ले } \end{aligned}$ | $\begin{aligned} & \mathrm{B} \\ & \mathrm{~N} \end{aligned}$ | $\begin{aligned} & \mathrm{B} \\ & \text { Ni } \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { N- } \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 \\ & \text { Ni } \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{8}{7} \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{\text { I }}{1} \end{aligned}$ | $\begin{aligned} & 8 \\ & \underset{\sim}{7} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 \\ & \text { ni } \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{0}{7} \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { ì } \end{aligned}$ | $\begin{aligned} & \mathrm{B} \\ & \text { Di } \end{aligned}$ | \％ |
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| $\stackrel{\varrho}{\Sigma}$ | $\sum$ | $\stackrel{\varrho}{\Sigma}$ | U | ט | $\stackrel{0}{\Sigma}$ | ¢ | U | U | $\overline{\text { x }}$ |  |  |  |  |  | $\overline{\bar{x}}$ |  |  |  |  |  |  |  |  |
| $=$ | $=$ | $=$ | $=$ | $=$ | $=$ | $=$ | ＝ | $=$ |  | $=$ | $=$ | $=$ | $=$ | $=$ | $\begin{aligned} & \dot{\nu} \\ & \underset{\sim}{\infty} \\ & \stackrel{0}{\downarrow} \\ & \stackrel{\rightharpoonup}{0} \end{aligned}$ | $=$ | $=$ | $=$ | $=$ | $=$ | $=$ | $=$ | $=$ |


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| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{aligned} & \text { 긍 } \\ & \text { oे } \end{aligned}$ |  | $\begin{aligned} & \stackrel{\infty}{N} \\ & \underset{\sim}{N} \end{aligned}$ | $\begin{aligned} & \stackrel{-}{7} \\ & \underset{\sim}{\infty} \\ & \underset{\sim}{1} \end{aligned}$ | $\begin{aligned} & \text { ○ } \\ & \text { o } \\ & \infty \end{aligned}$ | $\begin{aligned} & \hat{\star} \\ & \underset{\sigma}{\prime} \end{aligned}$ | $\begin{aligned} & \text { io } \\ & \text { on } \\ & \text { O } \end{aligned}$ | $\begin{aligned} & \text { N} \\ & \text { B } \\ & \text { O- } \end{aligned}$ | $\begin{aligned} & \text { è } \\ & \text { M } \\ & \text { on } \end{aligned}$ | $\begin{aligned} & \text { p } \\ & \text { n } \\ & \text { o } \end{aligned}$ | $\begin{aligned} & \text { Һٌ0 } \\ & 0 \\ & \text { N } \end{aligned}$ | $\stackrel{\infty}{\underset{\sim}{7}}$ | $\stackrel{\circ}{\sim}$ | $\stackrel{N}{\hat{N}}$ | $\begin{aligned} & \stackrel{1}{0} \\ & \stackrel{1}{N} \\ & 0 \\ & \hline 1 \end{aligned}$ | $\begin{aligned} & \text { N } \\ & \text { O } \\ & 0 \end{aligned}$ | $\begin{aligned} & \text { N } \\ & \underset{1}{0} \end{aligned}$ | $\begin{aligned} & \text { og } \\ & \text { N } \\ & \infty \end{aligned}$ | N |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | $\begin{aligned} & 0 \\ & 0 \\ & \stackrel{0}{0} \\ & \stackrel{0}{0} \\ & \stackrel{\rightharpoonup}{5} \end{aligned}$ | - - $\circ$ - - -1 | $\begin{aligned} & \varangle \\ & \stackrel{\rightharpoonup}{\circ} \\ & \underset{\sim}{-} \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \\ & \stackrel{0}{0} \\ & \stackrel{\rightharpoonup}{0} \\ & \stackrel{\rightharpoonup}{5} \end{aligned}$ | - $\stackrel{-}{-}$ $\stackrel{-}{-}$ - | - $\stackrel{-}{-}$ - -1 -1 | $\begin{aligned} & 1 \\ & \text { oे } \\ & \hline 0 \\ & 0 \end{aligned}$ |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | $\begin{aligned} & \text { } \\ & \underset{\sim}{\infty} \\ & \dot{\Sigma} \end{aligned}$ | $\begin{aligned} & \underset{O}{\infty} \\ & \stackrel{1}{1} \\ & \dot{\Sigma} \end{aligned}$ |  | $\begin{aligned} & \overline{0} \\ & \dot{\widetilde{\sigma}} \\ & \dot{4} \end{aligned}$ | $\begin{aligned} & \underset{~}{\infty} \\ & \stackrel{1}{1} \\ & \dot{\Sigma} \end{aligned}$ |  |  | 烒 |
| $\begin{array}{ll} \hat{N} \\ \stackrel{N}{\mathrm{~N}} & \stackrel{y}{0} \end{array}$ | $\begin{array}{ll} \bullet & 0 \\ & \stackrel{0}{2} \end{array}$ | $\begin{array}{ll} \ominus & \varrho \\ \dot{\omega} & \stackrel{y}{c} \end{array}$ |  |  | $\stackrel{\sim}{\sim}$ | $\underset{\sim}{\sim}$ | $\underset{\sim}{\underset{\sim}{\sim}}$ | $\underset{\sim}{\sim}$ | $\stackrel{\infty}{\stackrel{\infty}{i}}$ |  |  | $\begin{array}{ll} \text { !o } \\ \text { ल } \end{array}$ |  | $\begin{aligned} & \text { N} \\ & \underset{\sim}{-} \end{aligned}$ | $\begin{aligned} & \varrho \\ & \varrho \\ & \end{aligned}$ | $\begin{aligned} & \varrho \\ & \stackrel{\circ}{\mathrm{N}} \end{aligned}$ | $\begin{aligned} & \bullet \\ & \varrho \\ & \end{aligned}$ | $\begin{aligned} & \bullet \\ & \varrho \\ & \end{aligned}$ | $\begin{aligned} & \text { ழ } \\ & \dot{\oplus} \end{aligned}$ | $\begin{aligned} & \bullet \\ & \oplus \end{aligned}$ | $\begin{aligned} & \varphi \\ & \stackrel{\ominus}{\Gamma} \end{aligned}$ | $\stackrel{\ominus}{\oplus}$ |
| $\begin{array}{ll} 8 & 8 \\ \dot{\gamma} & 8 \\ j \end{array}$ | $\begin{array}{ll} 8 & 0 \\ \dot{\sigma} & 0 \\ 0 \end{array}$ | $\begin{array}{ll} 8 & 8 \\ 7 & 0 \\ \hline \end{array}$ | $\begin{array}{ll} \mathrm{O} & \mathrm{O} \\ \text { Ni } \end{array}$ | ○ | $\begin{array}{ll} 8 & \stackrel{O}{8} \\ \text { ले } & 0 \end{array}$ | $\begin{aligned} & \mathrm{O} \\ & \text { ले } \end{aligned}$ | $\begin{gathered} 8 \\ 0 \end{gathered}$ | $\begin{aligned} & 8 \\ & 0^{-} \end{aligned}$ | ৪ | $\begin{aligned} & \circ \\ & \text { O } \end{aligned}$ | $\stackrel{\mathrm{O}}{\mathrm{~F}}$ | $\begin{aligned} & \mathrm{O} \\ & \text { m } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { ल } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { m } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \underset{\sim}{-} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\begin{aligned} & 8 \\ & \mathrm{~N} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { N } \end{aligned}$ |
| $\begin{array}{ll} \stackrel{\circ}{\mathrm{N}} & \stackrel{\rightharpoonup}{\mathrm{~N}} \\ \text { ले } \end{array}$ | $\begin{array}{ll} \stackrel{\rightharpoonup}{\mathrm{N}} & \stackrel{\rightharpoonup}{\mathrm{~F}} \\ \stackrel{\circ}{\circ} \end{array}$ | $\begin{array}{ll} \stackrel{0}{2} & \text { N } \\ \underset{\sim}{n} & \text { م } \end{array}$ | $\begin{aligned} & \text { O } \\ & \text { ल } \end{aligned}$ |  | $\begin{aligned} & \circ \\ & \text { m } \end{aligned}$ |  | $\begin{aligned} & \circ \\ & \infty \\ & \sigma^{-} \end{aligned}$ | $\begin{aligned} & 0 \\ & \infty \\ & + \end{aligned}$ | $\begin{aligned} & \circ \\ & \text { ल } \end{aligned}$ |  |  | $\begin{aligned} & \text { ค } \\ & \text { ल } \end{aligned}$ |  | $\begin{aligned} & \circ \\ & \stackrel{\circ}{2} \end{aligned}$ | $\begin{aligned} & \text { ○ } \\ & \text { ल } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { ले } \end{aligned}$ | $\begin{gathered} N \\ \end{gathered}$ | $\begin{aligned} & \text { N} \\ & \end{aligned}$ | $\stackrel{\text { N }}{\text { N }}$ | $\stackrel{N}{N}$ | $\stackrel{N}{N}$ | $\stackrel{N}{N}$ |








| " ${ }^{\text {" }}$ - | 76,20 | 5,87 | 778,77 | 30,00 | SAP | 3,53 | 4,00 | 3.66 | Amatol | 4,11\% | A | 11310 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12-pdr/20cwt QF Mks. I |  |  |  |  |  |  |  |  |  |  |  |  |  |
| - IV | 76,20 | 5,67 | 762,00 | 90,00 | CP | 3,72 | 2,00 | 3.66 | Lyddite | 6,00\% | L | 9931 |  |
| " | 76,20 | 5,87 | 748,29 | 90,00 | SAP | 3,53 | 4,00 | 3.66 | Amatol | 4,11\% | A | 11645 |  |
| 16.25"/30 BL Mk. I | 412,75 | 816,47 | 636,12 | 13,00 | AP | 2,68 | 2,00 | 4.57 | iron Palliser |  |  | 11339 | Benbow, Victoria |
| " | 412,75 | 816,47 | 636,12 | 13,00 | Common | 3,38 | 2,00 | 4.57 | Iron forged | 10,72\% | BP | 11339 |  |
| " | 412,75 | 816,47 | 636,12 | 13,00 | Common | 3,50 | 2,00 | 4.57 | steel | 10,42\% | BP | 11339 |  |
| " | 412,75 | 816,47 | 636,12 | 13,00 | Common | 3,50 | 2,00 | 4.57 | cast steel | 9,96\% | BP | 11339 |  |
| " | 412,75 | 816,47 | 636,12 | 13,00 | Shot | 3,65 | 2,00 | 4.57 | steel base |  |  | 11339 |  |
| " | 412,75 | 816,47 | 636,12 | 13,00 | CP | 3,53 | 2,00 | 4.57 | fuzed | 10,11\% | BP | 11339 |  |
| " cordite | 412,75 | 816,47 | 694,34 | 13,00 | Shot | 3,65 | 2,00 | 4.57 | steel base |  |  | 12788 |  |
| " | 412,75 | 816,47 | 694,34 | 13,00 | CP | 3,53 | 2,00 | 4.57 | fuzed | 10,11\% | BP | 12788 |  |
| 13.5"/30 BL Mks. I-IV | 342,90 | 567,00 | 614,48 | 13,50 | AP | 3,25 | 2,00 | 4.28 |  |  |  | 10927 | Royal Sovereign class, Hood |
| " | 342,90 | 567,00 | 614,48 | 13,50 | Common | 4,09 | 2,00 | 4.28 | cast steel | 6,76\% | BP | 10927 |  |
| " cordite | 342,90 | 567,00 | 639,78 | 13,50 | AP | 3,25 | 2,00 | 4.28 |  |  |  | 11540 |  |
| " | 342,90 | 567,00 | 639,78 | 13,50 | Common | 4,09 | 2,00 | 4.28 | cast steel | 6,76\% | BP | 11540 |  |
| " | 342,90 | 567,00 | 614,48 | 13,00 | AP | 4,42 | 2,00 | 4.28 |  |  |  | 10670 | Anson class, Nile, Trafalgar |
| " | 342,90 | 567,00 | 614,48 | 13,00 | Common | 4,28 | 2,00 | 4.28 | cast steel | 6,76\% | BP | 10670 |  |
| " cordite | 342,90 | 567,00 | 639,78 | 13,00 | AP | 4,42 | 2,00 | 4.28 |  |  |  | 11274 |  |
| " | 342,90 | 567,00 | 639,78 | 13,00 | Common | 4,28 | 2,00 | 4.28 | cast steel | 6,76\% | BP | 11274 |  |
| 12"/25.1 BL Mk. II | 304,80 | 323,87 | 583,39 | 13,00 | AP | 2,64 | 2,00 | 6.09 |  |  |  | 8806 | Collingwood |
| " | 304,80 | 323,87 | 583,39 | 13,00 | Common | 3,33 | 2,00 | 6.09 | Cast Iron | 4,42\% | BP | 8806 |  |
| " | 304,80 | 323,87 | 583,39 | 12,50 | AP | 2,64 | 2,00 | 6.09 |  |  |  | 8595 |  |
| " | 304,80 | 323,87 | 583,39 | 12,50 | Common | 3,33 | 2,00 | 6.09 | Cast Iron | 4,42\% | BP | 8595 |  |
| 12"/25.5 BL Mks. III-V | 304,80 | 323,87 | 583,39 | 13,00 | AP | 2,64 | 2,00 | 6.09 |  |  |  | 8806 | Collingwood |
| PB | 304,80 | 323,87 | 583,39 | 13,00 | Common | 3,33 | 2,00 | 6.09 | Cast Iron | 4,42\% | BP | 8806 |  |
| " cordite | 304,80 | 323,87 | 592,53 | 13,00 | AP | 2,64 | 2,00 | 6.09 |  |  |  | 8975 |  |
| " cordite | 304,80 | 323,87 | 592,53 | 13,00 | Common | 3,50 | 2,00 | 6.09 | Forged Steel | 13,31\% | BP | 8975 |  |




| MD | 233,70 | 172,37 | 638,56 | 30,00 | HE | 3,80 | 2,00 | 5.79 | $\begin{gathered} \text { Mks VI \& } \\ \text { VII } \\ \text { Iron } \end{gathered}$ |  | BP | 15238 | re-armed |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 8"/25.6 BL Mk. III | 203,20 | 95,26 | 605,64 | 10,00 | AP | 2,62 | 2,00 | 3.05 | Palliser Cast Iron | 1,10\% | BP | 6714 | Bellerophon |
| " | 203,20 | 95,26 | 605,64 | 10,00 | Common | 3,31 | 2,00 | 3.05 | Mk II | 6,43\% | BP | 6714 |  |
| " | 203,20 | 95,26 | 605,64 | 10,00 | Common | 3,63 | 2,00 | 3.05 | $\begin{gathered} \text { Steel Mk } \\ \text { III } \\ \text { Mk I } \end{gathered}$ | 13,81\% | BP | 6714 |  |
| ${ }^{\text {\% }}$ " ${ }^{\text {a }}$ | 203,20 | 95,26 | 605,64 | 10,00 | CP | 3,34 | 2,00 | 3.05 | (1894) | 8,72\% | BP | 6714 |  |
| 8"/29.6 BL Mks. IV \& |  |  |  |  |  |  |  |  | Iron |  |  |  |  |
| VI | 203,20 | 95,26 | 670,56 | 15,00 | AP | 2,62 | 2,00 | 6.4 | Palliser Cast Iron | 1,10\% | BP | 10020 | Mersey class |
| " | 203,20 | 95,26 | 670,56 | 15,00 | Common | 3,31 | 2,00 | 6.4 | Mk II Steel Mk | 6,43\% | BP | 10020 |  |
| $"$ | 203,20 | 95,26 | 670,56 | 15,00 | Common | 3,63 | 2,00 | 6.4 | $\begin{gathered} \text { III } \\ \text { Mk II } \end{gathered}$ | 13,81\% | BP | 10020 |  |
| " cordite | 203,20 | 95,26 | 653,80 | 15,00 | AP | 2,62 | 2,00 | 6.4 | $\begin{gathered} \text { (1904) } \\ \text { Steel Mk } \end{gathered}$ | 5,00\% | BP | 9761 |  |
| " | 203,20 | 95,26 | 653,80 | 15,00 | Common | 3,63 | 2,00 | 6.4 | $\begin{gathered} \text { III } \\ \text { Mk I } \end{gathered}$ | 13,81\% | BP | 9761 |  |
| " | 203,20 | 95,26 | 653,80 | 15,00 | CP | 3,34 | 2,00 | 6.4 | $\begin{aligned} & \text { (1894) } \\ & \text { Mk IV } \end{aligned}$ | 8,72\% | BP | 9761 |  |
| " | 203,20 | 95,26 | 653,80 | 15,00 | CP | 3,34 | 2,00 | 6.4 | $\begin{aligned} & \text { (1900) } \\ & \mathrm{Mk} \text { I C } \end{aligned}$ | 8,57\% | BP | 9761 |  |
| " | 203,20 | 95,26 | 653,80 | 15,00 | HE | 3,16 | 2,00 | 6.4 | $\begin{aligned} & \text { 1900) } \\ & \text { Mk II } \end{aligned}$ | 10,98\% | L | 9761 |  |
| " | 203,20 | 95,26 | 653,80 | 10,00 | AP | 2,62 | 2,00 | 6.4 | $\begin{gathered} (1904) \\ \text { Steel Mk } \end{gathered}$ | 5,00\% | BP | 9026 | Abyssinia |
| " | 203,20 | 95,26 | 653,80 | 10,00 | Common | 3,63 | 2,00 | 6.4 | $\begin{gathered} \text { III } \\ \text { Mk I } \end{gathered}$ | 13,81\% | BP | 9026 |  |
| " | 203,20 | 95,26 | 653,80 | 10,00 | CP | 3,34 | 2,00 | 6.4 | $\begin{aligned} & \text { (1894) } \\ & \text { Mk IV } \end{aligned}$ | 8,72\% | BP | 9026 |  |
| " | 203,20 | 95,26 | 653,80 | 10,00 | CP | 3,34 | 2,00 | 6.4 | $\begin{aligned} & \text { (1900) } \\ & \text { Mk I C } \end{aligned}$ | 8,57\% | BP | 9026 |  |
| " | 203,20 | 95,26 | 653,80 | 10,00 | HE | 3,16 | 2,00 | 6.4 | 1900) | 10,98\% | L | 9026 |  |
| 6"/26 BL Mk.I | 152,40 | 36,29 | 573,05 | 13,00 | Common | 2,90 | 2,00 | 3.35 |  | 7,66\% | BP | 6424 | re-armed Rover |
| 6"/26 BL Mk. II | 152,40 | 45,36 | 509,63 | 15,00 | Common | 3,60 | 2,00 | 3.35 |  | 7,37\% | BP | 6940 | Agamemnon \& Ajax |
| " | 152,40 | 45,36 | 509,63 | 15,00 | AP | 3,17 | 2,00 | 3.35 | AP Mk. 1 | 4,25\% | BP | 6940 |  |
| " | 152,40 | 45,36 | 509,63 | 20,00 | Common | 3,60 | 2,00 | 3.35 |  | 7,37\% | BP | 8237 | re-armed Comus, Canada, Cordelia |
| " | 152,40 | 45,36 | 509,63 | 20,00 | AP | 3,17 | 2,00 | 3.35 | AP Mk. 1 | 4,25\% | BP | 8237 |  |
| " | 152,40 | 45,36 | 509,63 | 16,00 | Common | 3,60 | 2,00 | 3.35 |  | 7,37\% | BP | 7220 | re-armed Volage, Active, Bacchante class, Emerald, <br> Raleigh, Dolphin class, |
| " | 152,40 | 45,36 | 509,63 | 16,00 | AP | 3,17 | 2,00 | 3.35 | AP Mk. 1 | 4,25\% | BP | 7220 | Pelican, Wild Swan, |



|  | 5"/25 BL Mks. IV \& V | 127,00 | 22,68 | 533,40 | 15,00 | Common | 3,10 | 2,00 | 3.05 | Cast Iron Forged | 8,12\% | BP | 6781 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | " | 127,00 | 22,68 | 533,40 | 15,00 | Common | 3,10 | 2,00 | 3.05 | Steel | 13,87\% | BP | 6781 |  |
|  | " | 127,00 | 22,68 | 533,40 | 20,00 | Common | 3,10 | 2,00 | 3.05 | Cast Iron Forged | 8,12\% | BP | 7988 |  |
|  | " | 127,00 | 22,68 | 533,40 | 20,00 | Common | 3,10 | 2,00 | 3.05 | Steel | 13,87\% | BP | 7988 |  |
|  | " | 127,00 | 22,68 | 533,40 | 22,00 | Common | 3,10 | 2,00 | 3.05 | Cast Iron Forged | 8,12\% | BP | 8404 |  |
|  | " | 127,00 | 22,68 | 533,40 | 22,00 | Common | 3,10 | 2,00 | 3.05 | Steel Forged | 13,87\% | BP | 8404 |  |
|  | 5"/25 BLC | 127,00 | 22,68 | 580,65 | 15,00 | Common | 3,10 | 2,00 | 3.05 | Steel Forged | 13,87\% | BP | 7306 |  |
|  | " | 127,00 | 22,68 | 580,65 | 20,00 | Common | 3,10 | 2,00 | 3.05 | Steel <br> Forged | 13,87\% | BP | 8541 |  |
|  | " | 127,00 | 22,68 | 580,65 | 22,00 | Common | 3,10 | 2,00 | 3.05 | Steel | 13,87\% | BP | 8965 |  |
|  | 4"/25 BL Mk. I | 101,60 | 11,34 | 545,59 | 18,50 | Common | 3,00 | 2,00 | 4.42 |  | 7,00\% | BP | 6584 | Swiftsure Inflexible, Sutan, Switt- |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  | Inflexible, Sultan, Swiftsure, Alexandra, Teme- |
|  | 4"/27 BL Mks. II-VI | 101,60 | 11,34 | 579,12 | 20,00 | Common | 3,00 | 2,00 | 4.42 |  | 7,00\% | BP | 7041 | raore, Superb, <br> Alert, Phoenix, Condor, |
|  | 4" QFC | 101,60 | 11,34 | 668,12 | 20,00 | Common | 3,00 | 2,00 | 4.42 |  | 7,00\% | BP | 7723 | Cadmus |
|  | " | 101,60 | 11,34 | 668,12 | 20,00 | CP | 3,00 | 2,00 | 4.42 |  | 12,75\% | BP | 7723 |  |
|  | 4"/40 QF Mks. I-III | 101,60 | 11,34 | 701,04 | 20,00 | CP | 3,00 | 2,00 | 3.05 |  | 7,00\% | BP | 8610 | Invincible, Amethyst, Pelorus |
|  | 20-pdr/29 BLR Mk. I | 87,00 | 8,85 | 511,15 | 15,00 | Common | 3,61 | 2,00 | 2,66 | Forged Steel | 10,58\% | BP | 5535 |  |
|  | " | 87,00 | 8,44 | 511,15 | 15,00 | Common | 3,73 | 2,00 | 2,66 | Cast Iron | 11,08\% | BP |  |  |
|  | 12-pdr/28 BLR Mk. I | 76,20 | 5,67 | 524,26 | 15,00 | Common | 3,65 | 2,00 | 4,57 | Cast Iron Forged | 5,00\% | BP | 5252 |  |
|  | " | 76,20 | 5,67 | 524,26 | 15,00 | Common | 3,73 | 2,00 | 4,57 | Steel | 12,25\% | BP | 5252 |  |
| Armstrong | 17.72"/20.48 RML Mk. II | 450,00 | 907,19 | 471,83 | 12,00 | AP | 2,74 | 2,00 | 7.62 | iron Palliser | 1,60\% | BP | 6733 | Coast Defence |
|  | " | 450,00 | 907,19 | 471,83 | 12,00 | Common | 2,74 | 2,00 | 7.62 |  | 3,90\% | BP | 6733 |  |
|  | (6)" ${ }^{\text {" }}$ | 450,00 | 907,19 | 471,83 | 12,00 | CP | 2,97 | 2,00 | 7.62 | cast steel | 9,70\% | BP | 6724 |  |
|  | 16"/18 RML Mk. I (80T) | 406,40 | 771,11 | 484,63 | 10,00 | AP | 2,70 | 2,00 | 3.96 | $\begin{aligned} & \text { iron } \\ & \text { Palliser } \end{aligned}$ | 0,94\% | BP | 6153 | Inflexible |
|  | " | 406,40 | 771,11 | 484,63 | 10,00 | Common | 3,19 | 2,00 | 3.96 |  | 3,53\% | BP | 6153 |  |
|  | " | 406,40 | 771,11 | 469,39 | 10,00 | AP | 2,70 | 2,00 | 3.96 | Palliser | 0,94\% | BP | 5874 |  |
|  | " | 406,40 | 771,11 | 469,39 | 10,00 | CP | 3,50 | 2,00 | 3.96 | cast steel | 6,63\% | BP | 5857 |  |
|  | 12.5"/15.8 RML Mk. I | 317,50 | 371,04 | 439,52 | 14,00 | AP | 2,69 | 2,00 | 4.42 |  |  |  | 6547 | Dreadnought, |


|  | Thunderer |
| :---: | :---: |
| 6547 |  |
| 7297 | Agamemnon |
| 7297 |  |
|  | Devastation， |
| 6172 | Thunderer |
| 5918 |  |
|  | Monarch，Captain， |
| 6400 | Hotspur |
| 6400 |  |
| 6433 |  |
| 9144 | Alexandra，Temeraire |
| 9468 |  |
|  | Sultan，Hercules， |
| 4562 | Alexandra，Temeraire |
| 4569 |  |
|  | Minotaur，Royal Alfred， Lord Clyde，Bellerophon， |
| 4534 | Audacious |
| 4534 | Sultan，Swiftsure，Her－ cules，Prince Consort |
| 4449 |  |
| 4439 |  |
| 4552 |  |
| 4546 |  |
| 4543 |  |
| 4532 |  |
| 3842 |  |
| 3832 |  |
|  | Warrior，Defence， |
| 4245 | Hector，Achilles， |
| 4243 | Northumberland，Lord |
| 4243 | Clyde |
| 4232 |  |
| 4241 |  |


| 0 | $\frac{0}{\infty}$ | $\frac{0}{\infty}$ | $\frac{0}{\infty}$ | $\frac{0}{\infty}$ | $\frac{0}{\infty}$ | n | n | 0 | $\frac{0}{\infty}$ | $\frac{0}{\infty}$ | 0 | $\frac{0}{0}$ | $\frac{0}{\infty}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \stackrel{0}{\circ} \\ & \hline \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{0} \\ & \stackrel{0}{\circ} \\ & \stackrel{0}{2} \end{aligned}$ | $\begin{aligned} & \text { 今े } \\ & \stackrel{0}{\circ} \\ & \text { - } \end{aligned}$ | $\begin{aligned} & \text { సे } \\ & \text { Ò } \\ & \text { - } \end{aligned}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{乌} \\ & \vdots \\ & \hline- \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \stackrel{\circ}{\circ} \end{aligned}$ | $\begin{gathered} \stackrel{\text { ®}}{\stackrel{1}{2}} \\ \stackrel{1}{-} \end{gathered}$ | $\circ$ <br> 0 <br> 6 <br> 6 | $\circ$ <br> 0 <br> 6 <br> 6 | $\frac{\stackrel{0}{2}}{\stackrel{0}{n}}$ | $\stackrel{\circ}{\stackrel{\circ}{+}}$ | $\begin{gathered} \text { సे } \\ \text { సे } \end{gathered}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{\circ} \\ & \underset{\sim-1}{2} \end{aligned}$ |  |



| 〒 | フ | $\stackrel{\text { }}{ }$ | フ | $\stackrel{\sim}{\sim}$ | $\underset{\sim}{\sim}$ | $\stackrel{\text { }}{ }$ | ～ | $\checkmark$ | $\stackrel{+}{*}$ | $\stackrel{\square}{\circ}$ | $\stackrel{1}{0}$ | $\stackrel{\square}{0}$ | 12. | $\stackrel{\square}{\circ}$ | $\stackrel{0}{0}$ | $\stackrel{\square}{0}$ | $\stackrel{1}{\circ}$ | 20． | $\stackrel{\square}{\circ}$ | $\stackrel{1}{0}$ | $\stackrel{\circ}{\circ}$ | $\stackrel{\square}{0}$ | $\stackrel{1}{0}$ | 12 | $\stackrel{\circ}{0}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\checkmark$ | $\stackrel{+}{+}$ | $\stackrel{+}{\circ}$ | $\stackrel{\square}{*}$ | $\stackrel{+}{\circ}$ | $\stackrel{+}{\circ}$ | $\checkmark$ | $\checkmark$ | $\bullet$ | $\bullet$ | $\cdots$ | $\cdots$ | m | $\cdots$ | m | $\cdots$ | $\cdots$ | $\cdots$ | $\cdots$ | m | $\cdots$ | m | $\cdots$ | $\cdots$ | $\cdots$ | ल |









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| $\dot{\Sigma}$ | $\bar{r}$ |  |
| $\stackrel{1}{2}$ | $\Sigma$ |  |
| $\sum_{\boxed{ }}$ | $=\sum_{n}^{1}$ |  |
| $\bigcirc$ | ¢ |  |
|  | $\stackrel{\square}{0}$ |  |
| H | $\stackrel{\sim}{-1}$ |  |
| $\xrightarrow{\sim}$ |  |  |




|  |  |  |  |  |  |  |  |  |  |  |  |  | o 0 0 0 0 |  |  |  |  |  |  |  | $\begin{aligned} & \mathbb{\otimes} \\ & \frac{\pi}{0} \\ & \hline> \end{aligned}$ |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \stackrel{0}{6} \\ & \underset{\sigma}{2} \end{aligned}$ | $\begin{array}{cc} \stackrel{N}{N} \\ \underset{\sim}{\sim} \\ \underset{\sim}{2} \end{array}$ | $\underset{\underset{J}{J}}{\underset{J}{*}}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{0} \\ & \underset{\sim}{2} \end{aligned}$ | ¢ | － | $\stackrel{m}{\underset{\sim}{n}}$ | $\begin{aligned} & \text { O} \\ & \text { గ్ర } \end{aligned}$ | $\underset{\sim}{\underset{\sim}{N}}$ | $\underset{\sim}{N}$ | $\stackrel{\text { O}}{\substack{2}}$ | $\begin{aligned} & \text { O} \\ & \underset{\sim}{2} \end{aligned}$ | $\begin{aligned} & \infty \\ & \underset{\sim}{\infty} \\ & \hline \end{aligned}$ | $\begin{aligned} & \infty \\ & \underset{\sim}{\infty} \\ & \hline \end{aligned}$ | $\underset{\underset{\sim}{7}}{\underset{\sim}{2}}$ | $\stackrel{m}{7}$ | $\begin{aligned} & 0 \\ & \stackrel{7}{7} \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \bullet \\ & \stackrel{\rightharpoonup}{7} \\ & \bullet \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{\Phi} \\ & \underset{\sim}{\infty} \end{aligned}$ | $\begin{aligned} & \underset{7}{J} \\ & \text { に } \end{aligned}$ | $\begin{aligned} & \text { N } \\ & \stackrel{0}{\circ} \\ & \text { in } \end{aligned}$ | － | $\begin{aligned} & \underset{\sim}{\circ} \\ & \text { O} \end{aligned}$ | ¢ | ¢ | $\stackrel{\circ}{\stackrel{+}{+}}$ | $\stackrel{\sim}{\sim}$ | $\stackrel{\sim}{0}$ |
|  | ¢0 | － | ¢0 |  |  | 0 | 0 |  | －0 |  | ¢ |  | 0 |  | 00 |  | 00 |  |  | ¢0 |  | ¢0 |  | 0 |  | ¢ | 0 |
|  | Ǹ | $\begin{aligned} & \stackrel{\rightharpoonup}{\mathrm{N}} \\ & \end{aligned}$ | $\begin{aligned} & \text { むे } \\ & \text { बे } \end{aligned}$ |  |  | 츠N | $\stackrel{\stackrel{\rightharpoonup}{N}}{\underset{N}{N}}$ |  | $\stackrel{\stackrel{1}{0}}{0}$ |  | $\begin{aligned} & \text { Ò } \\ & \text { Ö } \\ & \text { On } \end{aligned}$ |  | $\begin{aligned} & \stackrel{\rightharpoonup}{\circ} \\ & \text { م } \\ & \infty^{\circ} \end{aligned}$ |  | $\begin{aligned} & \text { Oे } \\ & \text { Ö } \\ & \text { On } \end{aligned}$ |  | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \text { O- } \\ & \text { on } \end{aligned}$ |  |  | $\begin{aligned} & \stackrel{\circ}{0} \\ & \stackrel{\infty}{\infty} \end{aligned}$ |  | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \text { İ } \end{aligned}$ |  | $\begin{aligned} & \text { ஃे } \\ & \text { (i) } \end{aligned}$ |  | ¢ | ¢ |
|  |  | $0$ |  |  |  |  |  | － |  |  |  |  |  | $\begin{aligned} & \stackrel{\rightharpoonup}{\stackrel{1}{n}} \\ & \frac{\text { N }}{0} \\ & \stackrel{\otimes}{\omega} \end{aligned}$ |  | $\begin{aligned} & \stackrel{\rightharpoonup}{0} \\ & \frac{\rightharpoonup}{\omega} \\ & \stackrel{\rightharpoonup}{\otimes} \\ & \stackrel{\otimes}{\omega} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |  |
| $\stackrel{\sim}{\sim}$ | $\stackrel{\sim}{\sim}$ | $\stackrel{\sim}{N}$ | $\stackrel{\sim}{\mathrm{O}}$ | $\stackrel{\sim}{\sim}$ | $\stackrel{\sim}{\sim}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\stackrel{\sim}{\sim}$ |  | $\stackrel{\llcorner }{\circ}$ | $\stackrel{\leftrightarrow}{\mathrm{m}}$ | $\stackrel{\leftrightarrow}{\circ}$ | $\stackrel{\leftrightarrow}{\mathrm{O}}$ | $\stackrel{\Perp}{\circ}$ | $\stackrel{\Perp}{\circ}$ | $\stackrel{\sim}{\circ}$ | $\stackrel{\llcorner }{\stackrel{\circ}{\mathrm{N}}}$ | $\stackrel{\llcorner }{\mathrm{O}}$ | N゙ | $\stackrel{\tilde{n}}{\substack{0}}$ | $\stackrel{H}{n}$ | $\stackrel{\sim}{0}$ | $\stackrel{\sim}{\sim}$ | $\stackrel{\sim}{\sim}$ | $\stackrel{\sim}{\text { n }}$ | $\stackrel{8}{\sim}$ | $\stackrel{8}{8}$ | $\stackrel{8}{\sim}$ |
| $\stackrel{8}{\mathrm{~N}}$ | $\begin{array}{ll} \mathrm{O} \\ \underset{\sim}{c} & \stackrel{0}{\mathrm{~N}} \end{array}$ | $\underset{\sim}{\mathrm{N}}$ | $\stackrel{8}{\mathrm{~N}}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\stackrel{8}{\mathrm{~N}}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\stackrel{\mathrm{O}}{\mathrm{~N}}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\stackrel{\text { i }}{\text { i }}$ | $\stackrel{8}{\mathrm{~N}}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\stackrel{\mathrm{B}}{\mathrm{~N}}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\underset{\sim}{\mathrm{O}}$ | $\stackrel{\circ}{\mathrm{O}}$ | $\stackrel{8}{\mathrm{~N}}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\begin{aligned} & \circ \\ & \text { i } \end{aligned}$ | $\stackrel{8}{\mathrm{~N}}$ | $\stackrel{8}{\circ}$ | $\stackrel{\text { ® }}{\text { N }}$ | $\stackrel{8}{\mathrm{i}}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\stackrel{8}{\text { i }}$ | $\stackrel{8}{\text { i }}$ |
| $\begin{aligned} & 0 \\ & \underset{\sim}{-} \end{aligned}$ |  | $\stackrel{\sim}{N}$ | $\begin{aligned} & \hat{0} \\ & \hline \end{aligned}$ | $\stackrel{0}{2}$ | $\stackrel{0}{7}$ | $\begin{aligned} & \stackrel{0}{0} \\ & \text { N } \end{aligned}$ | $\stackrel{\sim}{N}$ | $\underset{\sim}{\underset{\sim}{N}}$ | $\stackrel{\infty}{\sim}$ | $\stackrel{\mathrm{N}}{\mathrm{~N}}$ | $\stackrel{\sim}{\sim}$ | $\begin{gathered} \text { N゙ } \\ \hline \end{gathered}$ | $\stackrel{\text { ¢ }}{\sim}$ | $\stackrel{\mathrm{H}}{\mathrm{~N}}$ | $\underset{\sim}{\infty}$ | $\stackrel{\text { N̈ }}{N}$ | $\begin{gathered} \infty \\ \underset{N}{N} \end{gathered}$ | On | $\stackrel{\infty}{-}$ | $\stackrel{\text { N}}{\text { N}}$ | $\stackrel{-}{-}$ | $\stackrel{\text { İ }}{\text {－}}$ | $\stackrel{\square}{-}$ | $\stackrel{\square}{7}$ | $\stackrel{\text { N }}{\text { N }}$ | $\stackrel{\sim}{\sim}$ | $\stackrel{\text { ® }}{\text { N }}$ |
| 言 |  | O 0 0 0 0 |  | 흥 | \％ |  |  | ¢ |  | ¢ |  | ¢ |  | ¢ |  |  |  | 픔 | $\stackrel{\square}{4}$ | $\begin{aligned} & \text { ᄃ } \\ & 0 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | $\stackrel{\square}{4}$ |  | ¢ |  | 픔 |  | ¢ |
| $\begin{aligned} & 8 \\ & \hline \mathbf{0} \\ & \hline \end{aligned}$ | $\begin{array}{ll} 8 & 8 \\ 0 \\ \hline-1 & 0 \end{array}$ | $\begin{aligned} & 8 \\ & \stackrel{8}{0} \\ & \text { - } \end{aligned}$ |  | $\begin{aligned} & \mathrm{O} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \underset{\sim}{N} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \text { O } \\ & \text { İ } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { I } \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { N } \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \underset{\sim}{\prime} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \text { O } \\ & \text { N } \end{aligned}$ |  | $\begin{aligned} & \circ \\ & \stackrel{\circ}{0} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{8}{\mathrm{~N}} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \stackrel{0}{\mathrm{O}} \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{\circ}{0} \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \underset{\sim}{N} \end{aligned}$ | $\begin{aligned} & \text { O } \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { 心⿴囗入 } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { in } \end{aligned}$ | －8 |
| $\begin{aligned} & \circ \\ & \stackrel{0}{7} \\ & \stackrel{\sim}{0} \end{aligned}$ |  |  | $\begin{aligned} & \text { N } \\ & \text { o. } \\ & \text { m } \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{\circ}{7} \\ & \text { ion } \end{aligned}$ | $\begin{aligned} & \text { ه} \\ & \underset{\sim}{\text { E }} \end{aligned}$ | $\begin{aligned} & \text { 앙 } \\ & \text { Hem } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { in } \\ & \text { Nem } \end{aligned}$ |  | $\stackrel{9}{\text { ®．}}$ | $\underset{\text { が }}{\underset{\text { ® }}{2}}$ | ঞ্ণ | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \text { O} \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{\circ}{\circ} \\ & \text { \% } \end{aligned}$ | $\begin{aligned} & \otimes \\ & \text { ®i } \\ & \text { O} \end{aligned}$ |  | $\begin{aligned} & \underset{\sim}{N} \\ & \underset{\sim}{\circ} \\ & \hline \end{aligned}$ | $\begin{aligned} & N \\ & \underset{\sim}{\circ} \\ & \cline { 1 - 2 } \end{aligned}$ | $\begin{aligned} & \stackrel{\text { O}}{\underset{\sim}{*}} \end{aligned}$ | $\begin{aligned} & \text { Oi} \\ & \underset{\sim}{\sim} \end{aligned}$ | $\begin{aligned} & \text { ol} \\ & \text { ®ु } \end{aligned}$ | $\begin{aligned} & \text { O } \\ & \text { I } \\ & \text { I- } \end{aligned}$ | $\begin{aligned} & \text { B } \\ & \text { ※ } \\ & \text { ju } \end{aligned}$ | $\begin{aligned} & \text { ه } \\ & \text { H゙ } \end{aligned}$ | $\begin{aligned} & \text { \& } \\ & \text { j } \\ & \text { j} \end{aligned}$ | $\begin{aligned} & \stackrel{9}{4} \\ & \underset{\sim}{\mathbf{N}} \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{\circ}{0} \\ & \text { O } \end{aligned}$ |  |
| $\begin{aligned} & \text { n } \\ & \text { in } \end{aligned}$ |  | $\begin{aligned} & \dot{\sigma} \\ & \dot{\sigma} \end{aligned}$ | $\begin{aligned} & \underset{\sim}{7} \\ & \underset{子}{2} \end{aligned}$ | $\begin{aligned} & \text { n } \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \text { n } \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \underset{\sim}{2} \\ & \stackrel{\sim}{2} \end{aligned}$ | $\begin{aligned} & \text { ু } \\ & \text { ó } \end{aligned}$ | $\begin{aligned} & \text { O } \\ & \text { O } \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \text { o } \\ & \text { o. } \\ & \text { in } \end{aligned}$ | $\stackrel{\infty}{\stackrel{\infty}{-}}$ | $\stackrel{\infty}{\stackrel{\circ}{-}}$ | $\begin{aligned} & \circ \\ & \text { @ } \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \text { o } \\ & \text { o } \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \infty \\ & \stackrel{\infty}{-1} \end{aligned}$ | $\stackrel{\infty}{\stackrel{\infty}{i n}}$ | $\begin{aligned} & \stackrel{\infty}{-} \\ & \underset{i}{-1} \end{aligned}$ | $\begin{aligned} & \infty \\ & \stackrel{\infty}{i} \end{aligned}$ | $\begin{aligned} & \text { N్N } \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \text { N } \\ & \text { N- } \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{\circ}{-1} \end{aligned}$ | $\begin{gathered} \stackrel{\sim}{N} \\ \underset{\sim}{2} \end{gathered}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{\mathrm{N}} \\ & \stackrel{\rightharpoonup}{2} \end{aligned}$ | $\stackrel{\stackrel{N}{N}}{\sim}$ | $\begin{gathered} \stackrel{\circ}{\mathrm{N}} \\ \underset{\sim}{2} \end{gathered}$ | $\begin{aligned} & \stackrel{8}{\circ} \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & \hat{M} \\ & \infty \\ & \underset{\sim}{1} \end{aligned}$ | $\stackrel{0}{0}$ |
| $\begin{aligned} & \circ \\ & \stackrel{\circ}{N} \\ & \stackrel{7}{7} \end{aligned}$ | $\begin{aligned} & \infty \\ & \stackrel{\infty}{\circ} \\ & \underset{A}{N} \\ & \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{\circ}{\wedge} \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{\infty}{N} \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \stackrel{N}{N} \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{\circ}{N} \\ & \underset{A}{2} \end{aligned}$ | $\begin{aligned} & \text { ® } \\ & \stackrel{y}{\wedge} \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{\circ}{N} \\ & \underset{\sim}{2} \end{aligned}$ | $\begin{aligned} & \infty \\ & \stackrel{\infty}{\wedge} \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{\circ}{N} \\ & \hline \end{aligned}$ | $\stackrel{\circ}{\stackrel{\circ}{\wedge}}$ | $\begin{aligned} & \circ \\ & \stackrel{\circ}{N} \\ & \underset{\sim}{2} \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{\infty}{స} \\ & \underset{A}{2} \end{aligned}$ | $\stackrel{\circ}{\stackrel{\circ}{N}} \stackrel{1}{\wedge}$ | $\begin{aligned} & \circ \\ & \stackrel{\infty}{N} \\ & \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{\circ}{\wedge} \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{\circ}{\wedge} \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { \& } \\ & \stackrel{N}{N} \end{aligned}$ | $\begin{aligned} & \stackrel{\text { O}}{5} \\ & \text { Ë } \end{aligned}$ | $$ | $\begin{aligned} & \text { O} \\ & \text { Ö } \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 \\ & 0 \\ & \hline 1 \end{aligned}$ | $\begin{aligned} & \circ \\ & \hline 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 . \\ & 0 \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \\ & 0 \\ & \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \\ & \text { N } \end{aligned}$ | － |
|  | 응 \＃ \＃ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | $=$ |  |
| 은 <br> 운 <br> W |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |


|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\stackrel{\circ}{\circ}$ | $\underset{\underset{\sigma}{\circ}}{\stackrel{\rightharpoonup}{\circ}}$ | $\begin{array}{cc} \underset{\sim}{\sim} & \underset{\sim}{\infty} \\ \underset{\sim}{\infty} \end{array}$ | N్రి | $\underset{\sim}{\text { B }}$ | $\begin{aligned} & \text { ৪ } \\ & \text { 子 } \end{aligned}$ | $\underset{\underset{\sim}{7}}{\underset{\sim}{2}}$ | $\stackrel{\sim}{\sim}$ | $\underset{\sim}{\underset{\sim}{7}}$ | $\stackrel{\text { ¢ }}{\sim}$ | へ | $\begin{aligned} & \underset{\sim}{\circ} \\ & \underset{\sim}{2} \end{aligned}$ | $\stackrel{\text { ® }}{\sim}$ |  | $\begin{aligned} & \stackrel{0}{7} \\ & \underset{F}{7} \end{aligned}$ | $\stackrel{\sim}{\sim}$ | $\stackrel{\text { n }}{\text { ¢ }}$ | $\begin{aligned} & \stackrel{\circ}{\infty} \\ & \infty \\ & \stackrel{\infty}{\infty} \end{aligned}$ |  |  | $\begin{aligned} & \circ \\ & \stackrel{\rightharpoonup}{7} \\ & \stackrel{N}{0} \end{aligned}$ | ＋ |
|  | ¢0 | 0 | 0 | 0 | 0 | ） | 0 | ¢ |  |  |  |  |  |  | $\vdash$ |  | $\vdash$ |  |  | $\vdash$ | $\vdash$ |
|  | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \text { O} \\ & \text { on } \end{aligned}$ | $\stackrel{\circ}{\text { N० }}$ | $\begin{aligned} & \text { సे } \\ & \text { O- } \end{aligned}$ | $\begin{aligned} & \text { స్ } \\ & \text { İ } \end{aligned}$ | $\begin{aligned} & \text { ⿳⿵人一⿲丶丶㇒一⿱口灬心 } \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { స్ర } \\ & \text { © } \end{aligned}$ | $\begin{aligned} & \circ \circ \\ & \stackrel{\circ}{4} \\ & \underset{子}{2} \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \underset{\sim}{\circ} \end{aligned}$ |  |  |  |  |  |  |  | N | $\begin{gathered} \text { ®̀ } \\ \text { Ǹ } \end{gathered}$ |  |  | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \text { ì } \end{aligned}$ | －\％ |

$\stackrel{\circ}{\circ}$

|  | 40－pdr／22 RML Mk．II | 120，65 | 17，37 | 434，34 | 15，00 | AP | 2，32 | 2，00 | 3.05 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ＂ | 120，65 | 17，37 | 434，34 | 15，00 | Common | 3，02 | 2，00 | 3.05 |
|  | 25－pdr／22 RML Mk．I | 101，60 | 11，34 | 411，48 | 16，00 | AP Shot | 2，53 | 2，00 | 3.05 |
|  | ＂ | 101，60 | 11，34 | 411，48 | 16，00 | Common | 3，29 | 2，00 | 3.05 |
| Armstrong | RBL 25－pdr 13cwt Mk．I | 101，60 | 11，34 | 359，66 | 20，00 | Common | 3，00 | 2，00 | 2.66 |
|  | －＂ | 101，60 | 11，34 | 359，66 | 12，00 | Common | 3，00 | 2，00 | 2，66 |
| Armstrong | $\begin{aligned} & \text { RBL 20-pdr } 16 \mathrm{cwt} \\ & (/ 21.3) \\ & \text { RBL 20-pdr } 15 \mathrm{cwt} \end{aligned}$ | 95，25 | 9，89 | 426，72 | 16，00 | Common | 2，96 | 2，00 | 2.66 |
| Armstrong | （／14．4） <br> RBL 12－pdr 12 cwt | 95，25 | 9，89 | 335，28 | 16，00 | Common | 2，96 | 2，00 | 2，66 |
| Armstrong | （／20．4） | 76，20 | 5，10 | 377，65 | 16，00 | Common |  | 2，00 | 3，05 |
| Armstrong | RBL 9－pdr 6 cwt （／17．5） | 76，20 | 3，88 | 321，56 | 16，00 | Common |  | 2，00 | 3，05 |
|  | $68-\mathrm{pdr} 95 \mathrm{cwt}$ SB | 200，00 | 31，50 | 581，58 | 7，50 | BALL | 1，00 | 1，00 | 3.05 |
|  | 32－pdr 56cwt SB | 162，80 | 14，30 | 511，15 | 7，50 | BALL | 1，00 | 1，00 | 2.59 |
|  | 18－pdr 42cwt SB | 134，40 | 8，20 | 464，21 | 7，50 | BALL | 1，00 | 1，00 | 2.59 |
|  | 8＂ 65 cwt Carronade | 204，50 | 25，40 | 432，82 | 7，50 | BALL | 1，00 | 1，00 | 2.59 |
|  | 8＂ 36 cwt Carronade | 204，50 | 25，40 | 157，58 | 7，50 | BALL | 1，00 | 1，00 | 2.59 |
|  | ITALIAN |  |  |  |  |  |  |  |  |
| Ansaldo | $381 \mathrm{~mm} / 50 \mathrm{M} 1934$ | 381，00 | 885，00 | 870，00 | 35，00 | APCBC | 4，38 | 6，00 | 8.5 |
| Ansaldo | $320 \mathrm{~mm} / 43.8 \mathrm{M} 1934$ | 320，00 | 525，00 | 830，00 | 27，00 | APCBC | 4，36 | 4，00 | 5.7 |
| Ansaldo | 203mm／53 M1927 | 203，20 | 125，30 | 900，00 | 45，00 | APCBC | 4，17 | 4，00 | 7.3 |
|  | ＂ | 203，20 | 125，30 | 960，00 | 45，00 | APCBC | 4，17 | 4，00 | 7.3 |
| Ansaldo | 203mm／50 M1924 | 203，20 | 125，30 | 905，00 | 45，00 | APCBC | 4，17 | 4，00 | 7.7 |
|  | ＂ | 203，20 | 118，00 | 840，00 | 45，00 | APCBC | 4，17 | 8，00 | 7.7 |
| Ansaldo | $152 \mathrm{~mm} / 55 \mathrm{M} 1934$ | 152，40 | 50，00 | 910，00 | 45，00 | APCBC | 4，13 | 8，00 | 6.3 |
| Ansaldo | $152 \mathrm{~mm} / 53 \mathrm{M} 1926$ | 152，40 | 50，00 | 975，00 | 45，00 | APCBC | 4，13 | 8，00 | 6.3 |


|  | 2，00\％ | T | 23930 |  |
| :---: | :---: | :---: | :---: | :---: |
|  | 2，11\％ | T | 22600 |  |
|  |  |  |  | Ciao Duilio，Capitani |
|  |  | T | 19600 | Romani |
|  |  | T | 19600 |  |
|  | 5，31\％ | T | 15500 | Sella，Sauro，Turbine |
|  | 9，94\％ | T | 13470 |  |
|  |  | T | 19600 | Navigatori，Dardo， Folgore |
|  |  | T | 19310 | Cavour，Soldati（2nd group） |
|  |  | T | 19050 | Soldati（1st group） |
|  |  | T | 18200 | Oriani |
|  |  | T | 17790 | Maestrale |
|  |  | T | 15240 | Standard HA gun |
|  |  | T | 15310 | Spica thru Ariete |
|  | 4，36\％ | T | 19800 | Caracciolo |
|  | 6，40\％ | T | 21000 |  |
|  |  |  |  | Dante Alighieri，Conte di |
| 7，40\％ | 4，80\％ |  | 20050 | Cavour，Caio Duilio |
|  | 6，01\％ |  | 21500 |  |
|  | 3，69\％ | T | 24000 |  |
|  |  |  | 19000 | Coast Defence |
|  | 2，79\％ | T | 19000 | Regina Margherita |
|  | 6，59\％ | T | 19000 |  |
|  | 4，80\％ | T | 20000 |  |
|  | 6，35\％ | T | 20000 |  |
|  | 2，79\％ | T | 19555 | Regina Elena |
|  | 6，59\％ | T | 19555 |  |
|  | 4，80\％ | T | 20000 |  |
|  | 6，35\％ | T | 20000 |  |
|  | 1，94\％ | T | 25000 | Pisa，San Giorgio |


| $\stackrel{\Im}{6}$ | $\stackrel{\sim}{0}$ | $\stackrel{\bigcirc}{0}$ | $\stackrel{\bigcirc}{6}$ | $\stackrel{\text { N }}{ }$ | $\stackrel{\text { N }}{\text { N }}$ | $\stackrel{\sim}{\text { N}}$ | $\stackrel{N}{\text { N }}$ | N | N | $\stackrel{\sim}{*}$ | $\stackrel{\rightharpoonup}{6}$ | $\underset{6}{-1}$ | ก | $\stackrel{\sim}{\sim}$ | $\stackrel{\odot}{\bullet}$ | $\stackrel{\odot}{\bullet}$ | $\stackrel{\bullet}{\bullet}$ | $\infty^{\circ}$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\stackrel{\circ}{\bullet}$ | $\bigcirc$ | $\bigcirc$ | $\stackrel{\circ}{\circ}$ | $\bigcirc$ | $\xrightarrow{\circ}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \mathrm{O} \\ & \mathrm{o}^{-} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~m}^{-} \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{\circ}{\circ} \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{0}{5} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { m } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \infty^{\circ} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{o}^{-} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~m}^{-} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{o}^{-} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \infty^{-} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { ले } \end{aligned}$ | ৪ | $\begin{aligned} & 8 \\ & \underset{\gamma}{ } \end{aligned}$ | -৪ | $\begin{aligned} & \mathrm{O} \\ & \text { ल } \end{aligned}$ | 응 | $\begin{aligned} & \mathrm{O} \\ & \text { ले } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { - } \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { ले } \end{aligned}$ | - | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { ले } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { ले } \end{aligned}$ | $\stackrel{8}{8}$ |
| $\underset{\sim}{\underset{\sim}{7}}$ | $\underset{\sim}{7}$ | $\begin{aligned} & \text { O} \\ & \underset{\sim}{2} \end{aligned}$ |  | $\begin{aligned} & \mathrm{O} \\ & \underset{\sim}{\circ} \end{aligned}$ |  | $\begin{aligned} & \text { 앙 } \end{aligned}$ | $\begin{aligned} & \text { of } \\ & \underset{\sim}{2} \end{aligned}$ | $\begin{aligned} & \underset{\sim}{q} \end{aligned}$ | $\stackrel{\underset{\sim}{\circ}}{\substack{0}}$ | $\begin{aligned} & \stackrel{+}{\dot{\circ}} \\ & \hline \end{aligned}$ | $\begin{aligned} & \infty \\ & \text { © } \\ & \text { m } \end{aligned}$ | $\begin{aligned} & \infty \\ & \text { ल } \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \infty \\ & \text { ल } \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \infty \\ & \infty \\ & \infty \end{aligned}$ | $\begin{aligned} & \text { of } \\ & \text { m } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{j} \end{aligned}$ | $\begin{aligned} & \circ \\ & \text { O } \\ & \text { ल } \end{aligned}$ |  | $\begin{aligned} & \mathrm{O} \\ & \text { m } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { ल } \end{aligned}$ | $\begin{aligned} & \mathrm{q} \\ & \text { min } \end{aligned}$ | $\begin{aligned} & \circ \\ & \hline- \end{aligned}$ | 웅 | $\begin{aligned} & \circ \\ & 0 \\ & \text { ल } \end{aligned}$ | 안 | $\stackrel{\text { O}}{\substack{\text {－}}}$ | ले |
| $\begin{aligned} & \text { U } \\ & 0 \\ & 0 \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { U } \\ & 0 \\ & 0 \\ & \text { e } \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \\ & 0 \\ & \text { en } \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { U } \\ & \text { U } \\ & \text { O } \\ & \hline \end{aligned}$ | $\frac{0}{\frac{0}{2}}$ | U | $\frac{\bar{a}}{\sqrt{x}}$ | $$ | $$ | $$ | $\begin{aligned} & \text { u } \\ & 0 \\ & \frac{0}{c} \\ & \dot{心} \end{aligned}$ | $\frac{0}{6}$ | $\frac{0}{4}$ | $\begin{aligned} & 0 \\ & \frac{0}{4} \end{aligned}$ | $\begin{aligned} & \text { U } \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0 \\ & \frac{0}{4} \end{aligned}$ | $\begin{aligned} & \text { U } \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0 \\ & \frac{0}{4} \end{aligned}$ |  | $\begin{aligned} & 0 \\ & \frac{n}{4} \end{aligned}$ | $0$ | $\begin{aligned} & 0 \\ & \frac{n}{4} \end{aligned}$ | $\begin{aligned} & \text { U } \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \cup \\ & \frac{0}{4} \end{aligned}$ | 0 | $\begin{aligned} & \text { U } \\ & \text { 文 } \end{aligned}$ | $\begin{aligned} & \text { U } \\ & \text { O } \end{aligned}$ | U |
| $\begin{aligned} & 8 \\ & \stackrel{0}{5} \\ & \hline \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 \\ & 5 \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { 8- } \\ & \text { Hin } \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 \\ & 5 \end{aligned}$ | ৪- | $\begin{aligned} & \mathrm{O} \\ & \text { M. } \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{8}{7} \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { y } \end{aligned}$ | $\begin{aligned} & \text { O- } \\ & \text { ó } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { N-M } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { N్ల. } \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 . \\ & 0 . \end{aligned}$ | $\begin{aligned} & 8 \\ & 8 \\ & 8 \end{aligned}$ | $\begin{aligned} & \mathrm{B} \\ & \text { Di } \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { ì } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { - } \end{aligned}$ | 은 | $\begin{aligned} & \mathrm{O} \\ & \text { - } \end{aligned}$ | $\begin{aligned} & 8 \\ & \underset{\sim}{\mathrm{I}} \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { Ni } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { Nin } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { Nin } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { Nin } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { NiN } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { Nin } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { Nin } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { Nin } \end{aligned}$ | － |
| $\begin{aligned} & \mathrm{O} \\ & \text { Oi } \\ & 0 \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 . \\ & 0 \\ & \infty \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { N } \\ & \text { م } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { N } \\ & \text { م } \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 . \\ & \text { م) } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { O- } \\ & \text { م } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { N్ } \end{aligned}$ | $\begin{aligned} & \text { B } \\ & \text { N్ర } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { - } \\ & \text { O } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { - } \\ & \text { ס } \end{aligned}$ | $\begin{aligned} & \text { B } \\ & \text { N/ } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & 0 . \\ & \text { in } \\ & \text { م } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { N్ } \\ & \text { م } \end{aligned}$ | 8 | $\begin{aligned} & \circ \\ & \stackrel{\circ}{\mathrm{o}} \\ & \stackrel{1}{2} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & 0 . \\ & 0 . \\ & \infty \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { O- } \\ & \text { D } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { O} \\ & \text { O } \end{aligned}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{0} \\ & \stackrel{1}{\circ} \\ & \infty \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & 0 \\ & \text { p } \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & 0 \\ & \text { p } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { Юi } \\ & \hline 1 \end{aligned}$ | $\begin{aligned} & \circ \\ & 0 . \\ & 0 . \end{aligned}$ | $\begin{aligned} & \text { B } \\ & 0 . \\ & \hline \infty \end{aligned}$ | $\begin{aligned} & \circ \\ & 0 \\ & 0 \\ & \text { p } \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 \\ & 0 \\ & \hline \end{aligned}$ | － |
| $\begin{aligned} & \circ \\ & 0 . \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{\sim} \\ & \underset{\sim}{2} \end{aligned}$ | $\begin{aligned} & \text { ค } \\ & \stackrel{N}{N} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \underset{\sim}{N} \end{aligned}$ | $\begin{aligned} & \stackrel{\sim}{7} \\ & \underset{N}{2} \end{aligned}$ | $\begin{aligned} & \text { M } \\ & \underset{N}{N} \end{aligned}$ | $\begin{aligned} & \text { B } \\ & \text { N్ } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { Ǹ } \end{aligned}$ | $\begin{aligned} & \text { in } \\ & \stackrel{n}{n} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \underset{N}{\mathrm{~N}} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \stackrel{n}{N} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { ले } \\ & \underset{N}{2} \end{aligned}$ | $\begin{aligned} & \circ \\ & { }_{-}^{\prime} \\ & \end{aligned}$ | $\begin{aligned} & \text { O } \\ & \underset{\sim}{\infty} \\ & \infty \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{8}{N} \\ & \underset{\infty}{\prime} \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{-}{7} \\ & \underset{寸}{2} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { i- } \end{aligned}$ | $$ | $\begin{aligned} & \text { O } \\ & \text { U } \\ & \text { V } \end{aligned}$ | $\begin{aligned} & \text { ம } \\ & \text { م } \\ & \text { م } \\ & \hline \end{aligned}$ | $\begin{aligned} & \infty \\ & \sim_{0}^{0} \\ & \sim \\ & \infty \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \stackrel{-}{7} \end{aligned}$ | $\begin{aligned} & \text { O } \\ & \text { O} \\ & \text { O } \end{aligned}$ | $\begin{aligned} & \circ \\ & 1 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & \circ \\ & م \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{\rightharpoonup}{7} \\ & \underset{\gamma}{2} \end{aligned}$ | O | O |
| $\begin{aligned} & \circ \\ & \stackrel{+}{N} \\ & \stackrel{\sim}{n} \end{aligned}$ | $\begin{aligned} & 0 \\ & \underset{\sim}{N} \\ & \underset{\sim}{n} \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{0}{n} \\ & \underset{\sim}{7} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \stackrel{1}{1} \\ & \mathrm{~N} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { O } \\ & \text { Ni } \end{aligned}$ | O 든 | $\begin{aligned} & \text { O} \\ & \text { 거 } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { O } \\ & \text { N- } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { O } \\ & \text { Nָ } \end{aligned}$ |  | O－ | $\begin{aligned} & 8 \\ & 0 \\ & \hline-1 \end{aligned}$ | $\begin{aligned} & 8 \\ & 8 \\ & 8 \\ & \hline \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { O- } \\ & \text { M } \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { B- } \\ & \hline 0 \end{aligned}$ | $\begin{aligned} & \text { ob } \\ & \text { O- } \\ & \text { O- } \end{aligned}$ | $\begin{aligned} & \text { O } \\ & \text { O- } \\ & \text { O} \end{aligned}$ | $\begin{aligned} & \circ \\ & 0 \\ & \text { O} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \text { ob } \\ & \text { to } \\ & \text { N } \end{aligned}$ |  | $\begin{aligned} & \text { O } \\ & \text { O- } \\ & \text { O- } \end{aligned}$ |  | $\begin{aligned} & \text { O } \\ & \text { O- } \\ & \text { O- } \end{aligned}$ | $\begin{aligned} & \text { O } \\ & \text { } \\ & \text { O- } \end{aligned}$ | $\begin{aligned} & \text { O } \\ & \text { O- } \\ & \text { O- } \end{aligned}$ | $\begin{aligned} & \circ \\ & \infty \\ & \stackrel{\sim}{\circ} \end{aligned}$ | $\begin{aligned} & \circ \\ & \text { ○ } \\ & \text { ণ } \end{aligned}$ | 8 |


| OTO | 135mm／45 M1937 |
| :---: | :---: |
|  | ＂ |
| Terni | 120mm／45 M1924 |
|  | ＂ |
| Ansaldo | 120mm／50 M1926 |
|  | ＂ |
|  | ＂ |
|  | ＂ |
|  | ＂ |
| OTO | 100mm／47 M1924 |
| OTO | 100mm／47 M1931 |
| EOC \＆VSM | 381mm／40 M1914 |
|  | （Pattern A \＆Mk．A） |
| EOC \＆VSM | 305mm／46 M1909 |
|  | （Pattern T \＆Mk．G） |
|  | ＂ |
| EOC | 305mm／50 Pattern Q |
| EOC | $305 \mathrm{~mm} / 40 \mathrm{M} 1900$ |
|  | ＂ |
|  | ＂ |
|  | ＂ |
| EOC | 305mm／40 M 1904 |
|  | ＂ |
|  | ＂ |
|  | ＂ |
| EOC \＆ |  |
| VSM | 254mm／45 M1906 |



| EOC | 152mm/40 M1891 | 152,40 | 45,36 | 700,00 | 15,00 | AP | 2,88 | 2,00 |  | Steel | 1,25\% | BP | 9260 | Re Umberto, Umbria, Calabria, Vettor Pisani, |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | " | 152,40 | 45,36 | 700,00 | 15,00 | AP | 3,27 | 2,00 |  | Steel | 4,87\% | BP | 9260 | Marco Polo |
|  | " | 152,40 | 45,36 | 700,00 | 15,00 | Common | 3,61 | 2,00 |  | Steel | 9,81\% | BP | 9260 |  |
|  | " | 152,40 | 46,30 | 700,00 | 15,00 | HE | 3,61 | 2,00 |  | Mod. 1885 | 11,66\% | BA | 9260 |  |
|  | " | 152,40 | 45,94 | 700,00 | 15,00 | HE |  | 2,00 |  |  | 12,76\% | T | 9260 |  |
|  | " | 152,40 | 47,45 | 695,00 | 25,00 | SAP |  | 4,00 |  | [1913?] | 5,08\% | T | 13900 |  |
|  | " | 152,40 | 46,44 | 695,00 | 25,00 | CP |  | 4,00 |  | [1913?] | 5,19\% | T | 13900 |  |
|  | " | 152,40 | 48,57 | 695,00 | 25,00 | APC |  | 4,00 |  | [1915?] | 1,17\% | T | 13900 |  |
| EOC | 152mm/40 M1888 | 152,40 | 45,36 | 655,00 | 15,00 | AP | 2,88 | 2,00 |  | Steel | 1,25\% | BP | 8660 |  |
|  | " | 152,40 | 45,36 | 655,00 | 15,00 | AP | 3,27 | 2,00 |  | Steel | 4,87\% | BP | 8660 |  |
|  | " | 152,40 | 45,36 | 655,00 | 15,00 | Common | 3,61 | 2,00 |  | Steel | 9,81\% | BP | 8660 |  |
|  | " | 152,40 | 46,30 | 655,00 | 15,00 | HE | 3,61 | 2,00 |  | Mod. 1885 | 11,66\% | BA | 8660 |  |
|  | " | 152,40 | 45,94 | 700,00 | 15,00 | HE |  | 2,00 |  |  | 12,76\% | T | 9260 |  |
|  | " | 152,40 | 47,45 | 695,00 | 25,00 | SAPC |  | 4,00 |  | [1913?] | 5,08\% | T | 13900 |  |
|  | " | 152,40 | 46,44 | 695,00 | 25,00 | CPC |  | 4,00 |  | [1913?] | 5,19\% | T | 13900 |  |
|  | " | 152,40 | 48,57 | 695,00 | 25,00 | APC |  | 4,00 |  | [1915?] | 1,17\% | T | 13900 |  |
|  | 120mm/50 M1909 |  |  |  |  |  |  |  |  |  |  |  |  | Dante Alighieri, Conte di Cavour, Quarto, Nino |
| EOC | Pattern EE | 120,00 | 22,13 | 850,00 | 30,00 | CPC | 4,20 | 3,00 | 3.1 |  | 9,94\% | T | 13700 | Bixio |
|  | " | 120,00 | 24,43 | 805,00 | 30,00 | CPC |  | 3,00 | 3.1 |  | 6,96\% | T | 13610 |  |
|  | " | 120,00 | 24,30 | 805,00 | 30,00 | HE |  | 3,00 | 3.1 |  | 7,57\% | T | 13610 |  |
|  | 120mm/45 M1913 | 120,00 | 22,13 | 750,00 | 32,00 | CP | 4,20 | 3,00 | 5.1 |  | 9,94\% | T | 12235 | Libia |
|  | " | 120,00 | 23,15 | 750,00 | 32,00 | AP |  | 3,00 | 5.1 |  | 5,31\% |  | 13611 |  |
|  | " | 120,00 | 24,43 | 730,00 | 32,00 | CP |  | 3,00 | 5.1 |  | 7,53\% | T | 12996 | Coast Defence |
| Terni | 102mm/35 M1914 | 101,60 | 13,35 | 760,00 | 25,00 | HE | 3,80 | 2,00 | 3.7 | M 1914 | 8,58\% | PA | 11000 | Poerio, Mirabello, Audace (ii), Sirtori |
|  | " | 101,60 | 15,00 | 755,00 | 25,00 | AP |  | 2,00 | 3.7 | M 1914 |  |  | 11500 |  |
|  | " | 101,60 | 13,74 | 750,00 | 25,00 | CP | 3,80 | 4,00 | 3.7 | M 1917 | 9,46\% | T | 12180 |  |
| Ansaldo | 102mm/45 M1917 | 101,60 | 13,74 | 850,00 | 35,00 | CP | 3,80 | 4,00 | 3.7 | M 1917 | 9,46\% | T | 15000 | Leone, La Masa, Palestro, Cantore, Curtatone |
|  | " | 101,60 | 16,00 | 840,00 | 35,00 | CP |  | 3,00 | 3.7 | M 1917 |  |  | 14600 |  |
|  | $76 \mathrm{~mm} / 50 \mathrm{M} 1908$ | 76,20 | 6,30 | 795,00 | 20,00 | CP | 3,80 | 2,00 | 5.4 |  | 4,76\% |  | 9287 |  |
|  | " | 76,20 | 6,50 | 783,00 | 20,00 | CP | 3,00 | 2,00 | 5.4 |  | 4,62\% |  | 9370 |  |



|  | " | 254,00 | 225,00 | 665,00 | 35,00 | CPC |  | 4,00 | 4.0 | M. 1907 | 6,67\% | T | 20543 | Coast Defence |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | " | 254,00 | 216,30 | 675,00 | 35,00 | CPC |  | 3,00 | 4.0 | M. 1916 | 8,32\% | T | 21292 | Coast Defence |
| Armstrong | 254mm/26 M | 254,00 | 204,12 | 579,12 | 16,00 | AP | 2,88 | 2,00 | 4.0 |  | 1,58\% | BP | 10280 | Giovanni Bausan |
|  | " | 254,00 | 181,44 | 614,17 | 16,00 | Common | 3,57 | 2,00 | 4.0 |  | 4,95\% | BP | 10546 |  |
|  | " | 254,00 | 204,12 | 640,00 | 16,00 | AP |  | 2,00 | 4.0 |  | 1,58\% | BP | 11580 |  |
|  |  | 254,00 | 204,12 | 640,00 | 16,00 | Common |  | 2,00 | 4.0 |  | 6,25\% | BP | 11580 |  |
| Armstrong | 10"/14.6 18-Ton MLR No. 1 | 254,00 | 205,00 | 423,00 | 10,00 | AP | 3,44 | 2,00 | 3.35 | Palliser | 2,44\% | BP | 4720 | Principe Amedeo |
|  | " | 254,00 | 181,00 | 433,00 | 10,00 | Common | 3,30 | 2,00 | 3.35 |  | 5,97\% | BP | 4738 |  |
|  | 10"/14 18.1-Ton MLR No. 2 | 254,00 | 205,00 | 423,00 | 10,00 | AP | 3,44 | 2,00 | 3.35 | Palliser | 2,44\% | BP | 4720 | Messina, Conte Verde, Re di Portogallo (1870) |
| Armstrong | 10"/12.6 12.1-Ton MLR | 254,00 | 181,00 | 433,00 | 10,00 | Common | 3,30 | 2,00 | 3.35 |  | 5,97\% | BP | 4738 | Roma |
| Armstrong | No. 3 | 254,00 | 150,50 | 418,50 | 10,00 | AP | 2,53 | 2,00 | 3.35 | Palliser | 2,52\% | BP | 4380 | Re de Portogallo |
|  | " | 254,00 | 129,00 | 429,00 | 10,00 | Common | 2,35 | 2,00 | 3.35 |  | 6,40\% | BP | 4349 |  |
| Armstrong | 9"/13.9 12.6-Ton MLR | 228,60 | 143,50 | 423,00 | 10,00 | AP | 3,30 | 2,00 | 2.0 | Palliser | 2,06\% | BP | 4577 | Regina Maria Pia, Venezia, San Martino (1875), <br>  |
|  | " | 228,60 | 113,00 | 443,00 | 10,00 | Common | 2,83 | 2,00 | 2.0 |  | 7,52\% | BP | 4566 | Castelfidardo (1871) |
|  | " new chg | 228,60 | 143,50 | 439,50 | 10,00 | AP | 3,30 | 2,00 | 2.0 | Palliser | 2,06\% | BP | 4801 |  |
|  | " new chg | 228,60 | 113,00 | 471,00 | 10,00 | Common | 2,83 | 2,00 | 2.0 |  | 7,52\% | BP | 4908 |  |
| Armstrong | 8"/13.1 7-Ton MLR | 203,20 | 87,50 | 449,00 | 10,00 | AP | 2,86 | 2,00 | 2.0 | Palliser | 1,86\% | BP | 4633 | Formidabile, Principe di Carignano, Re D'Italia Regina Maria Pia, Palestro |
|  | " | 203,20 | 68,00 | 494,00 | 10,00 | Common | 2,90 | 2,00 | 2.0 |  | 6,47\% | BP | 4776 |  |
|  | " new chg | 203,20 | 87,50 | 412,00 | 10,00 | AP | 2,86 | 2,00 | 2.0 | Palliser | 1,86\% | BP | 4202 |  |
|  | " new chg $16 \mathrm{~cm} / 15.5$ 3.54-Ton | 203,20 | 68,00 | 425,00 | 10,00 | Common | 2,90 | 2,00 | 2.0 |  | 6,47\% | BP | 4094 | Formidabile, Principe di |
| Palliser | MLR <br> $16 \mathrm{~cm} / 16.8$ 5.12-Ton | 164,00 | 30,00 | 312,00 | 12,00 | Common | 2,07 | 2,00 | 2.0 |  | 4,23\% | BP | 3144 | Carignano, Re D'Italia |
| Palliser | MLR | 164,00 | 46,00 | 397,00 | 12,00 | AP | 2,53 | 2,00 | 2.0 | Palliser | 1,86\% | BP | 4404 | " " |
|  | " | 164,00 | 30,00 | 325,00 | 12,00 | Common | 2,07 | 2,00 | 2.0 |  | 4,23\% | BP | 3299 |  |
| Armstrong | 152mm/26.1 Pattern B | 152,40 | 36,29 | 593,00 | 12,00 | AP | 2,37 | 2,00 | 4.57 |  | 1,87\% | BP | 6410 | Giovanni Bausan |
|  | " | 152,40 | 36,29 | 593,00 | 12,00 | Common | 3,12 | 2,00 | 4.57 |  | 6,26\% | BP | 6410 |  |
|  | " | 152,40 | 45,23 | 530,00 | 12,00 | CP |  | 2,00 | 4.57 |  | 4,45\% | BP | 6340 |  |
|  | " | 152,40 | 45,72 | 530,00 | 12,00 | CP |  | 2,00 | 4.57 | above refilled | 5,47\% | T | 6340 |  |










EOC

| Armstrong | " | 120,00 | 16,50 | 395,00 | 15,00 | Common |  | 2,00 | 2,0 | M. 1885 | 6,06\% | BP | 4650 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & 120 \mathrm{~mm} / 23.5 \text { 1.38-Ton } \\ & \text { BLR } \end{aligned}$ | 120,00 | 16,50 | 485,00 | 15,00 | Common |  | 2,00 | 2.0 | M. 1885 | 6,06\% | BP | 5430 | Ancona \& Castelfidardo (1884), Affondatore (1885) |
|  | 120mm/32 Patt. M [1885] | 120,00 | 16,33 | 580,00 | 30,00 | AP |  | 2,00 | 4.0 | M. 1885 | 5,08\% | BP | 8530 | Lepanto, Italia, Ruggiero di Lauria, Tripoli, Confienza |
| EOC | " | 120,00 | 16,33 | 580,00 | 30,00 | Common | 2,88 | 2,00 | 4.0 |  | 8,39\% | BP | 8530 |  |
|  | " | 120,00 | 16,33 | 580,00 | 30,00 | Common |  | 2,00 | 4.0 | refilled | 2,78\% | BP | 8530 |  |
|  | " | 120,00 | 16,50 | 580,00 | 30,00 | HE |  | 2,00 | 4.0 | Common refilled | 2,75\% | PA | 8530 |  |
|  | " | 120,00 | 17,23 | 580,00 | 30,00 | HE | 2,88 | 2,00 |  | Common refilled | 12,19\% | PA | 8530 |  |
|  | " | 120,00 | 20,38 | 580,00 | 30,00 | AP | 3,02 | 2,00 |  | Palliser refilled | 3,71\% | T | 9850 |  |
|  | " | 120,00 | 20,55 | 580,00 | 30,00 | HE |  | 2,00 |  | Common | 8,58\% | T | 9850 |  |
|  | " | 120,00 | 24,43 | 580,00 | 30,00 | CPC |  | 3,00 |  |  | 7,53\% | T | 10710 |  |
|  | $120 \mathrm{~mm} / 40 \mathrm{M} 1889$ | 120,00 | 24,30 | 580,00 | 30,00 | HE |  | 3,00 |  |  | 7,00\% | T | 10710 |  |
|  | 120mm/40 M1889 [Patt.M] | 120,00 | 20,41 | 665,00 | 30,00 | AP | 3,02 | 2,00 | 4.0 | $\begin{aligned} & \text { iron } \\ & \text { Palliser } \end{aligned}$ | 1,94\% | BP | 10790 | Duilio, Partenope, Piemonte |
| EOC | " | 120,00 | 20,41 | 665,00 | 30,00 | AP | 3,02 | 2,00 | 4.0 | Steel | 4,44\% | BP | 10790 |  |
|  | " | 120,00 | 20,41 | 665,00 | 30,00 | Common |  | 2,00 | 4.0 |  | 5,56\% | BP | 10790 |  |
|  | " | 120,00 | 20,41 | 665,00 | 30,00 | CP | 3,63 | 2,00 | 4.0 | cast steel refilled | 10,00\% | BP | 10790 |  |
|  | " | 120,00 | 20,38 | 665,00 | 30,00 | AP | 3,02 | 2,00 | 4.0 | Palliser refilled | 3,71\% | T | 10790 |  |
|  | " | 120,00 | 20,55 | 665,00 | 30,00 | HE |  | 2,00 | 4.0 | Common | 8,58\% | T | 10790 |  |
|  | " | 120,00 | 24,43 | 605,00 | 30,00 | CPC |  | 3,00 | 4.0 |  | 7,53\% | T | 11040 |  |
|  | " | 120,00 | 24,30 | 605,00 | 30,00 | HE |  | 3,00 | 4.0 |  | 7,00\% | T | 11040 |  |
|  | $120 \mathrm{~mm} / 40 \mathrm{M} 1891$ [Patt P] | 120,00 | 20,41 | 665,00 | 30,00 | AP | 3,02 | 2,00 | 4.0 | iron Palliser | 1,94\% | BP | 10790 | Re Umberto, Ammiraglio de St. Bon, Umbria |
|  | " | 120,00 | 20,41 | 665,00 | 30,00 | AP | 3,02 | 2,00 | 4.0 | Steel | 4,44\% | BP | 10790 | Calabria, Marco Polo, Vettor Pisani |
|  | " | 120,00 | 20,41 | 665,00 | 30,00 | Common |  | 2,00 | 4.0 |  | 5,56\% | BP | 10790 |  |
|  | " | 120,00 | 20,41 | 665,00 | 30,00 | CP | 3,63 | 2,00 | 4.0 | cast steel refilled | 10,00\% | BP | 10790 |  |
|  | " | 120,00 | 20,38 | 665,00 | 30,00 | AP | 3,02 | 2,00 | 4.0 | Palliser refilled | 3,71\% | T | 10790 |  |
|  | " | 120,00 | 20,55 | 665,00 | 30,00 | HE |  | 2,00 | 4.0 | Common | 8,58\% | T | 10790 |  |
|  | " | 120,00 | 24,43 | 605,00 | 30,00 | CPC |  | 3,00 | 4.0 |  | 7,53\% | T | 11040 |  |


| 7，00\％ | T | 11040 |  |
| :--- | :--- | ---: | :--- |
| 4，76\％ | BP | 8494 |  |
|  |  | 9051 |  |
| 4，62\％ |  | 8544 | Terribile（1880）， <br> 4，23\％ |
| BP | 3634 | Affondatore（1885） <br> Re di Portogallo |  |
| 4，23\％ | BP | 1807 | （1871） |

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 $27 \mathrm{~cm} . \mathrm{K} .120 \mathrm{M} / 74$ 27cm．K．／19 M／69 25 cm ．K．$/ 34$ M／85 25 cm. K．$/ 34 \mathrm{M} / 89$


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| Wahrendorff | 30-pdr KK/16.75M/1853 | 162,40 | 14,40 | 479,00 | 5,00 | Ball | 1,00 |  |  |  | 1771 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Wahrendorff | 24-pdr KK L/11M/1854 | 162,40 | 10,30 | 556,00 | 5,00 | Shell |  | 1,00 |  |  | 2,91\% | BP | 1698 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | 154,80 | 12,00 | 347,00 | 5,00 | Ball |  | 1,00 |  |  |  |  | 1285 |  |
| Wahrendorff | 24-pdr KK L/18.5M/1854 | 154,80 | 8,60 | 402,00 | 5,00 | Shell |  | 1,00 |  |  | 2,91\% | BP | 1274 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | 154,80 | 12,00 | 474,00 | 5,00 | Ball |  | 1,00 |  |  |  |  | 1644 |  |
|  | 24-pdr RK/20 M/1854 | 154,80 | 8,60 | 550,00 | 5,00 | Shell |  | 1,00 |  |  | 2,91\% | BP | 1556 |  |
| Wahrendorff |  | 153,50 | 12,25 | 428,00 | 5,00 | Shot |  | 2,00 |  |  |  |  | 1870 |  |
|  |  | 153,50 | 24,80 | 301,00 | 5,00 | Shell |  | 2,00 |  |  | 5,40\% | BP | 1460 |  |
| Armstrong | $15 \mathrm{~cm} . \mathrm{K} . / 28 \mathrm{M} / 83$ | 152,40 | 45,36 | 506,00 | 13,00 | AP | 2,96 | 2,00 | 4.0 |  |  |  | 6107 | Edda, Svea |
|  | 15 cm. K./32 M/89$15 \mathrm{~cm} . \mathrm{K} . / 32 \mathrm{M} / 98-02$ <br> $(\mathrm{QFC})$ | 152,40 | 45,36 | 506,00 | 13,00 | Common | 3,86 | 2,00 | 4.0 |  |  |  | 6107 |  |
| Bofors |  | 152,40 | 45,36 | 630,00 | 13,00 | AP | 2,96 | 2,00 | 4.0 |  |  |  | 7665 | Gota, Thule, \& Disa, Urd, \& Skagul re-armed |
|  |  | 152,40 | 45,36 | 506,00 | 13,00 | Common | 3,86 | 2,00 | 4.0 |  |  |  | 6107 |  |
|  |  | 152,40 | 45,36 | 700,00 | 15,00 | AP | 2,96 | 2,00 | 4.0 |  |  |  | 9130 |  |
| Bofors | 15cm.K./44.5 M/98 <br> " new chg '30s | 152,40 | 45,36 | 700,00 | 15,00 | Common | 3,86 | 2,00 | 4.0 |  |  |  | 9130 |  |
|  |  | 152,40 | 45,40 | 750,00 | 15,00 | AP | 2,97 | 2,00 | 4.5 | M/98 |  |  | 9780 | Aran, Dristigheten, re-armed Svea |
|  |  | 152,40 | 46,00 | 770,00 | 15,00 | SAPBC | 4,20 | 8,50 | 4.5 | M/30 |  |  | 13700 |  |
| Bofors | $15 \mathrm{~cm} . \mathrm{K} .143 .4 \mathrm{M} / 98 \mathrm{~B}$ | 152,40 | 45,40 | 770,00 | 12,00 | AP |  | 2,00 | 4,0 | M/98 |  |  | 8990 | Coast Defence |
| Bofors | $15 \mathrm{~cm} . \mathrm{K} .150 \mathrm{M} / 03$ | 152,40 | 45,40 | 850,00 | 15,00 | APC | 3,15 | 4,00 | 5.0 | M/03 |  |  | 13000 | Fylgia |
|  | " | 152,40 | 46,00 | 850,00 | 15,00 | SAPBC | 4,20 | 8,50 | 5.0 | M/30 |  |  | 15300 |  |
|  | " | 152,40 | 45,40 | 850,00 | 12,00 | APC | 3,15 | 4,00 | 5.0 | M/03 |  |  | 11700 | Oscar II |
|  | " | 152,40 | 46,00 | 850,00 | 12,00 | SAPBC | 4,20 | 8,50 | 5.0 | M/30 |  |  | 13700 |  |
| Bofors | $15 \mathrm{~cm} . \mathrm{K} .150 \mathrm{M} / 12$ | 152,40 | 45,40 | 850,00 | 15,00 | APC | 3,47 | 4,00 | 5.0 | M/03 |  |  | 13000 | Sverige |
|  | " | 152,40 | 46,00 | 850,00 | 17,50 | SAPBC | 4,20 | 8,50 | 5.0 | M/30 |  |  | 16500 |  |
| Wofors | 15cm.K./55 M/30 18-pdr RK/17.2 | 152,40 | 46,00 | 900,00 | 45,00 | SAPBC | 4,20 | 8,50 | 6.5 | M/30 |  |  | 24700 | Gotland |
|  | M/1854 | 138,50 | 9,00 | 433,00 | 5,00 | Shot |  | 2,00 |  |  |  |  | 1797 |  |
|  | ${ }^{\text {" }}$ | 138,50 | 17,50 | 328,00 | 5,00 | Shell |  | 2,00 |  |  | 2,86\% | BP | 1590 |  |
| Wahrendorff | $\begin{aligned} & \text { 12-pdr RK/20 } \\ & \text { M/1841/45 } \end{aligned}$ | 127,50 | 6,00 | 471,00 | 5,00 | Shot |  | 2,00 |  |  |  |  | 1787 |  |
|  | " | 127,50 | 13,50 | 314,00 | 5,00 | Shell |  | 2,00 |  |  | 2,96\% | BP | 1488 |  |


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|  |  |  | 3166 | Blenda \& Urd originally |
|  |  |  | 5967 | Blenda \& Urd re-armed |
|  |  |  | 5000 |  |
|  |  |  | 8200 | Oden, re-armed Berserk, Solve, |
|  |  |  | 8200 | \& Ulf, Ornen class |
|  |  |  | 12900 |  |
|  |  |  | 8000 | Coast Defence |
|  |  |  | 8000 |  |
|  |  |  | 14200 |  |
|  |  |  | 10000 | Clas Fleming |
|  |  |  | 16000 |  |
|  |  |  | 19300 | Ehrenskold, Clas Horn, Goteborg |
|  |  |  | 14947 | Psilander |
|  |  |  | 15500 | Arholma |
|  |  |  | 18200 | Mode |
|  |  |  | 14708 | Romolus |
|  |  |  | 5900 | Coast Defence |
|  |  |  | 6000 | Coast Defence |
|  | 4,88\% |  | 8715 | Ragnar, Hugin, Sverige |
|  | 4,88\% |  | 8930 | Wale, Wrangel |
|  | 4,88\% |  | 10880 |  |
|  | 4,88\% |  | 14245 |  |
|  | 4,88\% |  | 15000 |  |
|  | 4,88\% |  | 15000 | Gotland |
| 9,40\% | 2,48\% | M | 41700 | Richelieu |
| 16,05\% | 3,63\% | M | 41700 | Dunkerque |
|  | 3,25\% |  | 31400 | Duquesne, Suffren |



| 121,70 | 15,60 | 411,00 | 9,00 | Common | 2,42 | 2,00 | 4.0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 121,70 | 22,00 | 500,00 | 13,50 | AP Shot |  | 2,00 | 4.0 |
| 121,70 | 15,70 | 500,00 | 13,50 | Common |  | 2,00 | 4.0 |
| 120,00 | 21,00 | 740,00 | 15,00 | AP | 2,81 | 2,00 | 4.5 |
| 120,00 | 21,00 | 740,00 | 15,00 | Common | 3,30 | 2,00 | 4.5 |
| 120,00 | 21,00 | 830,00 | 15,00 | SAPBC | 3,72 | 10,00 | 4.5 |
| 120,00 | 21,00 | 860,00 | 10,00 | AP | 2,81 | 2,00 | 4,0 |
| 120,00 | 21,00 | 860,00 | 10,00 | Common |  | 2,00 | 4,0 |
| 120,00 | 21,00 | 860,00 | 17,00 | SAPBC | 3,72 | 10,00 | 4,0 |
| 120,00 | 21,00 | 860,00 | 17,00 | SAP | 3,33 | 2,00 | 4,0 |
| 120,00 | 21,00 | 860,00 | 22,50 | SAPBC | 3,72 | 10,00 | 4,0 |
| 120,00 | 20,50 | 800,00 | 45,00 | HC |  | 10,00 | 4.0 |
| 120,00 | 23,15 | 850,00 | 33,00 | SAP | 4,30 | 3,00 | 5.2 |
| 105,00 | 16,00 | 700,00 | 60,00 | SAP | 4,28 | 5,00 | 5,0 |
| 105,00 | 16,00 | 840,00 | 60,00 | SAP | 4,28 | 5,00 | 5,0 |
| 100,00 | 13,80 | 855,00 | 60,00 | SAP | 3,80 | 3,00 | 6.1 |
| 84,00 | 6,70 | 470,00 | 21,00 | Common | 3,04 | 2,00 | 4,0 |
| 84,00 | 6,70 | 470,00 | 20,00 | Common |  | 2,00 | 4,0 |
| 75,00 | 6,50 | 780,00 | 20,00 | CP | 4,30 | 2,00 | 3.0 |
| 75,00 | 6,50 | 810,00 | 20,00 | CP | 4,30 | 2,00 | 4,0 |
| 75,00 | 6,50 | 810,00 | 75,00 | CP | 4,30 | 2,00 | 4,0 |
| 75,00 | 6,50 | 780,00 | 80,00 | CP |  | 2,00 | 4,0 |
| 75,00 | 6,50 | 840,00 | 90,00 | CP |  | 2,00 | 4,0 |
| 75,00 | 6,50 | 840,00 | 90,00 | CP | 4,20 | 2,00 | 4,0 |
| 380,00 | 884,00 | 830,00 | 35,00 | APCBC | 5,00 | 10,00 | 9.0 |
| 330,00 | 560,00 | 870,00 | 35,00 | SAPCBC | 5,00 | 10,00 | 9.2 |
| 203,00 | 123,10 | 850,00 | 45,00 | APCBC | 4,95 | 10,00 | 6.2 |


| $\begin{aligned} & \text { 12.2cm.K./22 M/73 } \\ & \text { MLR } \end{aligned}$ |  |
| :---: | :---: |
| 12cm. K./26 M/81 |  |
| " |  |
| $\begin{aligned} & \text { 12cm.K./45 M/94 \& } \\ & / 97 \end{aligned}$ |  |
| " |  |
|  |  |
| 12cm.K./50 M/03 |  |
| " |  |
| " | (1940) |
| 12cm.K./50 M/11 |  |
|  | (1940) |
| 12cm.K. $/ 45 \mathrm{M} / 24$ |  |
| 120mm/45 M1926 |  |
| 10 cm . K./41 M/40 |  |
| 10cm. K./50 M/42 |  |
| 100mm/47 M1931 |  |
| 8cm.K./27.4 M/83 |  |
| 8cm.K./26.2 M/94 |  |
| 7.5cm.K./53 M/05 |  |
| 7.5cm.K./53 M/12 |  |
| 7.5 cm . LK./53 M/15 |  |
| 7.5cm. LK./53.2 M/24 |  |
| 7.5 cm . LK./60 M/26 |  |
| 7.5cm.K./60 M/28 |  |
| FRANCE |  |
| 380mm/45 M1935 |  |
| $330 \mathrm{~mm} / 50 \mathrm{M} 1931$ |  |
| $203 \mathrm{~mm} / 50 \mathrm{M}$ | 924 |



| " | 203,00 | 134,00 | 820,00 | 45,00 | APCBC | 4,78 | 7,00 |  | M1936 |  |  | 29973 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 203mm/55 M1931 | 203,00 | 134,00 | 840,00 | 45,00 | APCBC | 4,78 | 7,00 | 7.0 | M1936 |  |  | 31030 | Algerie |
| 155mm/50 M1920 | 155,00 | 56,50 | 850,00 | 40,00 | SAPBC | 4,88 | 10,00 | 5.7 |  | 5,91\% | M | 26100 | Bearn, Duguay Trouin, Jeanne D'Arc |
| " | 155,00 | 56,50 | 850,00 | 40,00 | CPBC | 5,16 | 10,00 |  | M1925 | 9,96\% |  | 26100 |  |
| " | 155,00 | 59,00 | 830,00 | 40,00 | SAPBC | 4,69 |  |  |  | 5,00\% |  | 26100 |  |
| 152mm/55 M1930 | 152,40 | 54,50 | 882,00 | 80,00 | APCBC | 4,70 | 7,00 | 6.1 | M1931 |  |  | 26441 | Richelieu, Emile Bertin, La Galissonniere, |
| " | 152,40 | 56,00 | 855,00 | 80,00 | APCBC | 4,76 | 4,00 |  | M1931 | 5,96\% |  | 26470 | De Grasse |
| " | 152,40 | 57,15 | 847,00 | 80,00 | APCBC | 5,40 | 12,50 |  | M1937 |  |  | 27000 |  |
| " | 152,40 | 54,44 | 867,00 | 80,00 | SAPBC | 4,77 | 5,00 |  | M1936 |  |  | 27049 |  |
| " | 152,40 | 49,00 | 909,00 | 80,00 | SAPBC | 4,77 | 5,00 |  | M1937 |  |  | 27075 |  |
| $138.6 \mathrm{~mm} / 40 \mathrm{M} 1923$ | 138,60 | 40,60 | 700,00 | 35,00 | SAPBC | 4,93 | 8,00 | 5.0 |  | 5,91\% | T | 18200 | Guepard Pluton, Aigle, Vauquelin, |
| $138.6 \mathrm{~mm} / 40 \mathrm{M} 1927$ $138.6 \mathrm{~mm} / 50 \mathrm{M} 1929$. | 138,60 | 40,60 | 700,00 | 28,00 | SAPBC | 4,93 | 8,00 | 5.0 |  | 5,91\% | T | 16600 | Bougainville |
| $138.6 \mathrm{~mm} / 50 \mathrm{M} 1929$ - $34$ | 138,60 | 40,60 | 800,00 | 30,00 | SAPBC | 4,93 | 8,00 | 5.0 |  | 5,91\% | T | 20000 | Le Fantasque, Mogador |
| 130mm/40 M1919 | 130,00 | 32,11 | 739,00 | 36,00 | SAPBC | 5,00 | 10,00 | 4.0 |  | 5,61\% | T | 18081 | Chacal, Bourrasque |
| " | 130,00 | 33,40 | 725,00 | 36,00 | SAPBC | 4,98 | 10,00 |  |  | 4,79\% | T | 18700 |  |
| 130mm/40 M1924 | 130,00 | 32,11 | 739,00 | 35,00 | SAPBC | 5,00 | 10,00 | 4.0 |  | 5,61\% | T | 18241 | L'Adrpot |
| " | 130,00 | 33,40 | 725,00 | 35,00 | SAPBC | 4,98 | 10,00 |  |  | 4,79\% | T | 18871 |  |
| 130mm/45 M1932-35 | 130,00 | 32,11 | 800,00 | 75,00 | SAPBC | 5,00 | 10,00 | 4.0 |  | 5,61\% | T | 20870 | Dunkerque, Joffre, Le Hardi |
| " | 130,00 | 33,40 | 784,00 | 75,00 | SAPBC | 4,98 | 10,00 |  |  | 4,79\% | , | 21683 |  |
| 100mm/45 M1932 | 100,00 | 14,95 | 755,00 | 34,00 | SAPBC | 5,00 | 5,00 | 4.0 |  |  |  | 15000 | Richelieu, Algerie, La Melpomene, Le Fier |
| 450mm/45 M1920 | 450,00 | 1365,00 | 850,00 | 40,00 | APCBC |  | 7,00 | 8,0 |  |  |  | 52000 |  |
| 450mm/45 M1918 | 450,00 | 1300,00 | 785,00 | 23,00 | APC | 3,74 | 4,00 | 7.2 |  |  |  | 26520 |  |
| 400mm/45 M1917 | 400,00 | 990,00 | 760,00 | 23,00 | APC | 4,05 | 4,00 | 7.0 |  |  |  | 24860 |  |
| $380 \mathrm{~mm} / 45 \mathrm{M} 1917$ | 380,00 | 800,00 | 785,00 | 23,00 | APC | 3,34 | 2,00 | 7.8 |  | 5,00\% | M | 21860 |  |
| " | 380,00 | 800,00 | 785,00 | 23,00 | APC |  | 4,00 | 7.8 |  | 5,00\% | M | 24900 |  |
| $370 \mathrm{~mm} / 45 \mathrm{M} 1916$ | 370,00 | 780,00 | 785,00 | 23,00 | APC | 3,92 | 2,00 | 6.9 |  |  |  | 22150 | Durand-Viel 'B' |
| $340 \mathrm{~mm} / 45 \mathrm{M} 1912 \mathrm{M}$ | 340,00 | 570,00 | 786,00 | 18,00 | APC | 3,80 | 4,00 | 7.2 | M.1912M |  |  | 20650 | Lyon, Durand-Viel 'A' |
| " | 340,00 | 590,00 | 772,00 | 18,00 | APC | 3,82 | 2,00 | 7.2 |  | 3,66\% | M | 18070 |  |



|  |  |  |  |  |  |  |  | 0 0 0 0 0 0 0 0 0 0 0 0 0 0 |  |  |  |  |  |  | $\check{\circ}$ |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \stackrel{N}{N} \\ & \underset{\sim}{n} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & 0 \\ & 0 \end{aligned}$ | O | $\begin{aligned} & \text { 응 } \\ & \text { 구 } \end{aligned}$ | 응 | $\begin{array}{ll} \circ & 0 \\ \circ & 8 \\ \underset{-}{ } & \vdots \end{array}$ | $\begin{aligned} & \text { O} \\ & \text { n } \end{aligned}$ | O O M | O त त | $\begin{aligned} & \text { O} \\ & \text { İ } \end{aligned}$ | － | 8 <br>  <br> 7 |  | 8 ¢ 7 | $\begin{aligned} & \text { O} \\ & \text { N } \\ & \text { In } \end{aligned}$ | O a a | $\circ$ <br> 0 <br> 0 <br> -1 | $\circ$ <br> 0 <br> 0 | O － | $\stackrel{\circ}{\circ}$ $\sim$ $\sim$ | $\begin{aligned} & \circ \\ & \underset{\sim}{\circ} \\ & \end{aligned}$ |  | $\stackrel{\circ}{\sim}$ | ㅇ I － |  |
| $\Sigma$ | $\Sigma$ |  | $\Sigma$ |  |  | $\Sigma$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | $\Sigma$ |  |
| $\begin{aligned} & \stackrel{\circ}{\grave{0}} \\ & \stackrel{\rightharpoonup}{0} \end{aligned}$ | $\stackrel{\stackrel{\circ}{\circ}}{\stackrel{\rightharpoonup}{0}}$ |  | $\begin{aligned} & \text { oे } \\ & \text { ले } \end{aligned}$ |  |  | $\begin{aligned} & \text { O} \\ & \stackrel{0}{0} \\ & \text { nj } \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | $\begin{aligned} & \text { oे̀ } \\ & \text { ले } \end{aligned}$ |  |
|  |  |  | $\begin{aligned} & \stackrel{\rightharpoonup}{7} \\ & \underset{\sim}{7} \end{aligned}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{\circ} \\ & \underset{\sim}{7} \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{0} \\ & \stackrel{1}{n} \\ & 0 \end{aligned}$ |  |  | $\begin{aligned} & \text { ®ั } \\ & \stackrel{\sim}{N} \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \underset{\sim}{N} \end{aligned}$ | $\begin{aligned} & \text { oे } \\ & \text { స̀ } \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{\sim} \\ & \stackrel{\sim}{N} \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{\sim} \\ & \underset{\sim}{\sim} \end{aligned}$ |  | $\begin{aligned} & \text { oे } \\ & \text { N゙ } \end{aligned}$ | $\begin{aligned} & \stackrel{0}{\circ} \\ & \stackrel{1}{0} \\ & \text { - } \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \stackrel{0}{9} \end{aligned}$ | $\begin{aligned} & \text { oे } \\ & \stackrel{\circ}{\circ} \\ & \text { mad } \end{aligned}$ | － |  |  |  |  | तै － － |  |
| $\begin{aligned} & \vec{\Omega} \\ & \stackrel{\rightharpoonup}{\mathbf{N}} \end{aligned}$ | $\stackrel{\underset{\sim}{N}}{\underset{\Sigma}{2}}$ | $\begin{aligned} & \infty \\ & \frac{0}{0} \\ & \stackrel{7}{2} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \stackrel{\text { a }}{1} \\ & \sum \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \stackrel{\rightharpoonup}{7} \\ & \sum \end{aligned}$ |  |  | $\begin{aligned} & \text { N. } \\ & \stackrel{\infty}{\infty} \\ & \underset{\Sigma}{7} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \stackrel{\text { O}}{2} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \stackrel{\text { O}}{2} \\ & \Sigma \end{aligned}$ | $\begin{aligned} & \text { ब̈. } \\ & \text { बे } \\ & \stackrel{\rightharpoonup}{\Sigma} \end{aligned}$ |  | $\begin{aligned} & \text { O} \\ & \stackrel{\text { O}}{2} \\ & \Sigma \end{aligned}$ | $\begin{aligned} & \text { B } \\ & \stackrel{\rightharpoonup}{7} \\ & \Sigma \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{0} \\ & \stackrel{7}{\mathbf{T}} \end{aligned}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{\vec{~}} \\ & \stackrel{\rightharpoonup}{\mathrm{~N}} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \stackrel{\text { N }}{2} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \stackrel{\rightharpoonup}{2} \\ & \stackrel{N}{2} \end{aligned}$ | $\begin{aligned} & \text { N. } \\ & \stackrel{\rightharpoonup}{\circ} \\ & \stackrel{\rightharpoonup}{\Sigma} \end{aligned}$ | $\begin{aligned} & \mathrm{N} \\ & \underset{\sim}{\infty} \\ & \stackrel{1}{1} \\ & \Sigma \end{aligned}$ | $\begin{aligned} & \hat{\sim} \\ & \stackrel{\infty}{\infty} \\ & \stackrel{1}{N} \end{aligned}$ |  | $\begin{aligned} & \underset{\sim}{\infty} \\ & \stackrel{\infty}{\infty} \\ & \stackrel{N}{\Sigma} \end{aligned}$ | $\begin{aligned} & \stackrel{8}{\circ} \\ & \stackrel{\rightharpoonup}{7} \end{aligned}$ |  |
|  |  | $\bigcirc$ | $\stackrel{\text { ® }}{\text { ¢ }}$ |  |  |  |  | $\stackrel{\sim}{\square}$ |  |  |  |  | $\stackrel{\bigcirc}{6}$ |  |  | $\stackrel{\cap}{+}$ |  |  | $\bigcirc$ |  |  |  |  |  |
| $\stackrel{\circ}{\sim}$ | $\begin{aligned} & \circ \\ & \hline- \\ & \hline \end{aligned}$ | $\stackrel{8}{\mathrm{~N}}$ | $\stackrel{\text { ® }}{\text { ® }}$ | $\stackrel{\circ}{\mathrm{N}}$ | - 은 | O | $\stackrel{\circ}{\mathrm{N}}$ | $\stackrel{8}{\mathrm{~N}}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\stackrel{\circ}{\mathrm{o}}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\stackrel{8}{\mathrm{~N}}$ | － | $\stackrel{\stackrel{\rightharpoonup}{\mathrm{N}}}{\mathrm{i}}$ | $\stackrel{8}{8}$ | $\stackrel{\text { ¢ }}{\text { ¢ }}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\stackrel{8}{8}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\begin{aligned} & \mathrm{O} \\ & \text { i } \end{aligned}$ |  | － | $\underset{\sim}{c} \underset{\sim}{\circ}$ | $\stackrel{8}{\text { ¢ }}$－ |
| $\stackrel{\circ}{\square}$ | 안 | $\underset{\sim}{\mathrm{N}}$ | $\stackrel{\circ}{\mathrm{o}}$ | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \hline \end{aligned}$ | $\stackrel{\stackrel{\rightharpoonup}{N}}{\text { N }}$ | $\underset{\sim}{\underset{\sim}{\circ}}$ | $\stackrel{\stackrel{\rightharpoonup}{\mathrm{N}}}{\mathbf{N}}$ | $\stackrel{\perp}{\sim}$ | $\stackrel{\text { ®- }}{\text { ® }}$ | $\begin{aligned} & \text { OM } \\ & \hline \end{aligned}$ | $\stackrel{0}{N}$ | $\stackrel{\mathrm{O}}{\mathrm{O}}$ | $\stackrel{+}{\circ}$ | $\begin{aligned} & \stackrel{\infty}{\infty} \\ & \stackrel{N}{i} \end{aligned}$ | $\underset{\sim}{\mathrm{N}}$ | $\stackrel{\circ}{\circ}$ | $\begin{aligned} & \infty \\ & \underset{N}{\circ} \end{aligned}$ | $\stackrel{\text { ® }}{\text { m }}$ | $\stackrel{\text { ® }}{\underset{\sim}{c}}$ | ${ }_{\text {O- }}^{\mathbf{N}}$ | $\stackrel{\sim}{\circ}$ | － | $\stackrel{\circ}{\circ}$ | $\stackrel{8}{\sim}$ |
| $\begin{aligned} & \text { u } \\ & 00 \\ & 0 \end{aligned}$ | $\begin{aligned} & \text { U } \\ & \text { Ò } \\ & \hline \end{aligned}$ | $\begin{aligned} & 0 \\ & \frac{0}{4} \end{aligned}$ | $\begin{aligned} & 0 \\ & \frac{0}{4} \end{aligned}$ | U | $\begin{aligned} & 0 \\ & \frac{0}{4} \end{aligned}$ | ¢ | 0 | $\begin{aligned} & 0 \\ & \frac{0}{4} \end{aligned}$ | O | $\begin{aligned} & \text { O } \\ & \text { 足 } \end{aligned}$ | $\begin{aligned} & \text { U } \\ & \text { 足 } \end{aligned}$ | $\begin{aligned} & \text { u } \\ & \text { O } \end{aligned}$ | $\begin{aligned} & \text { U } \\ & \frac{n}{4} \end{aligned}$ | $\begin{aligned} & \text { U } \\ & \text { 0 } \end{aligned}$ | $\begin{aligned} & \text { U } \\ & \frac{0}{4} \end{aligned}$ | $\begin{aligned} & 0 \\ & \frac{0}{4} \end{aligned}$ | U | U | ¢ |  |  |  | － | O |
| $\begin{aligned} & \text { Bi } \\ & \text { Ni } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \stackrel{\rightharpoonup}{N} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \underset{\sim}{\mathrm{H}} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { I } \end{aligned}$ | $\begin{aligned} & 8 \\ & \underset{\sim}{\mathrm{H}} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { Ni } \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{0}{7} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { İ } \end{aligned}$ | $\begin{aligned} & 0 \\ & \\ & \text { In } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{\circ}{0} \\ & \text { O } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \underset{\sim}{\circ} \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{0} \\ & \underset{\sim}{\circ} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { in } \end{aligned}$ | －8 | $\begin{aligned} & \mathrm{O} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { N } \end{aligned}$ |  | $\cdots$ | $\begin{aligned} & \mathrm{O} \\ & \text { N } \end{aligned}$ |  |
| $\begin{aligned} & \text { \& } \\ & \stackrel{\text { I }}{2} \end{aligned}$ | $\begin{aligned} & 8 \\ & 8 \\ & \hline 8 \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { ס్ర } \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{8}{2} \\ & \infty \\ & \infty \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \stackrel{\rightharpoonup}{\infty} \\ & \infty \end{aligned}$ | $$ | $\begin{aligned} & \text { B } \\ & \stackrel{0}{\circ} \\ & 0 \end{aligned}$ | 8 | $\begin{aligned} & \circ \\ & \stackrel{8}{\circ} \\ & \stackrel{\circ}{\infty} \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{8}{0} \\ & \text { in } \end{aligned}$ | 8． | 8 － － － | $\begin{aligned} & 8 \\ & \hline \text { O } \\ & \text { O. } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { O } \\ & \text { O } \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{0}{0} \\ & \infty \end{aligned}$ | $\begin{aligned} & 8 \\ & \underset{\infty}{\infty} \\ & \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{\rightharpoonup}{0} \\ & 0 \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{8}{0} \\ & \stackrel{0}{\circ} \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 \\ & 0 \\ & \infty \end{aligned}$ | $\begin{aligned} & 8 \\ & 8 . \\ & 0.8 \end{aligned}$ | 8 |  | $\infty$ | $\begin{aligned} & 8 \\ & \hline 0 \\ & \hline \end{aligned}$ | $\begin{array}{cc} 8 & 8 \\ 0.0 \\ \sim & 0 \\ 0 \end{array}$ |
| $\stackrel{\stackrel{8}{\mathrm{e}}}{\stackrel{1}{2}}$ | $\begin{aligned} & \text { Oin } \\ & \text { N్ల } \end{aligned}$ | $\stackrel{g}{6}$ | $\begin{aligned} & \text { O} \\ & \stackrel{-}{\dot{O}} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \stackrel{0}{0} \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{\circ}{-} \\ & \text { O. } \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \stackrel{8}{\mathrm{~N}} \\ & \underset{\sim}{2} \end{aligned}$ | $\begin{aligned} & \text { B } \\ & \underset{\sim}{\sim} \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { N్గ్N } \\ & \text { N } \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{8}{0} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \dot{N} \\ & \text { Oi } \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 \\ & \hline- \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 . \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & 8 \\ & \hline \\ & \infty \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \stackrel{\circ}{\infty} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { N- } \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { ì } \end{aligned}$ | $\begin{aligned} & \text { B } \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { 今in } \end{aligned}$ | $\begin{aligned} & \text { B } \\ & \stackrel{-}{4} \\ & \underset{\sim}{2} \end{aligned}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{0} \\ & \stackrel{\rightharpoonup}{\mathcal{F}} \end{aligned}$ |  | $\begin{array}{cc} 3 \\ \hline & 8 \\ \text { N } \\ \text { N } \end{array}$ | $\begin{aligned} & \text { O} \\ & \text { O} \\ & \text { jum } \end{aligned}$ |  |
| $\begin{aligned} & \stackrel{\circ}{0} \\ & \infty \\ & \end{aligned}$ |  | $\begin{aligned} & 8 \\ & \stackrel{8}{n} \\ & \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { Li } \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \stackrel{\rightharpoonup}{0} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{0}{0} \\ & \text { م̀ } \end{aligned}$ | $\begin{aligned} & \text { B } \\ & \text { 心్లి } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \stackrel{0}{0} \end{aligned}$ | $\begin{aligned} & \stackrel{g}{J} \\ & \underset{\sim}{N} \end{aligned}$ | $\begin{aligned} & \text { o} \\ & \stackrel{y}{4} \end{aligned}$ |  | $\begin{aligned} & \text { O} \\ & \text { O} \\ & \text { j} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \stackrel{-}{\circ} \\ & \text { d } \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{8}{\circ} \\ & \stackrel{1}{\prime} \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{8}{9} \\ & \stackrel{1}{\prime} \end{aligned}$ |  | $\circ$ $\stackrel{0}{G}$ | $\begin{aligned} & \stackrel{\circ}{+} \\ & \stackrel{+}{+} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \stackrel{+}{+} \\ & \text { O- } \end{aligned}$ | $\begin{aligned} & \text { \& } \\ & \text { O} \\ & \text { Gे } \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{0} \\ & \stackrel{-}{j} \end{aligned}$ |  |  | $\begin{aligned} & \text { O} \\ & \stackrel{0}{0} \end{aligned}$ | $\begin{array}{ll} \circ \\ \stackrel{0}{0} & \stackrel{0}{0} \\ \text { in } \\ \hline 0 \end{array}$ |
| $=$ |  | $\begin{aligned} & 0_{0}^{\infty} \\ & \sum_{n}^{1} \\ & 0 \\ & 0 \\ & 0 \\ & N \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |  | $=$ |  |  |  |  |  | $=$ |  |  |  | ＝$=$ |


| 274mm/45 M1893 | 274,40 | 216,00 | 800,00 | 12,00 | AP | 2,44 | 2,00 | 6.5 | M 1887? |  |  |  | 11370 | Masena, Bouvet, rearmed Courbet |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| " | 274,40 | 216,00 | 800,00 | 12,00 | Common | 2,95 | 2,00 |  | M 1887? |  |  |  | 11370 |  |
| " | 274,40 | 255,00 | 800,00 | 12,00 | APC | 2,70 | 2,00 |  | M 1900 | 15,29\% |  |  | 12000 |  |
| " | 274,40 | 255,00 | 800,00 | 12,00 | CPC | 3,00 | 2,00 |  | M 1900 | 15,29\% |  |  | 12000 |  |
| " | 274,40 | 262,60 | 780,00 | 12,00 | APC | 3,30 | 4,00 |  | M 1919? | 17,90\% |  |  | 14140 |  |
| 240mm/40 M1893 | 240,00 | 144,00 | 800,00 | 12,00 | AP | 2,43 | 2,00 | 8.5 | M 1893? |  |  |  | 10650 | D'Entrecasteaux |
| " | 240,00 | 144,00 | 800,00 | 12,00 | Common | 2,94 | 2,00 |  | M 1893? |  |  |  | 10650 |  |
| " | 240,00 | 170,00 | 800,00 | 12,00 | APC | 2,70 | 2,00 |  | M1900 | 15,29\% |  |  | 11235 |  |
| " | 240,00 | 170,00 | 800,00 | 12,00 | CPC | 3,00 | 2,00 |  | M 1900 | 15,29\% |  |  | 11235 |  |
| 194mm/40 M1893 | 194,00 | 75,00 | 800,00 | 12,00 | AP | 2,40 | 2,00 | 6.5 | M 1887? |  |  |  | 9450 | Pothuau |
| " | 194,00 | 75,00 | 800,00 | 12,00 | Common | 2,89 | 2,00 |  | M 1887? |  |  |  | 9450 |  |
| " | 194,00 | 86,00 | 770,00 | 12,00 | APC | 2,60 | 2,00 |  | M 1900 | 12,79\% |  |  | 9500 |  |
| " | 194,00 | 89,50 | 770,00 | 12,00 | APC | 3,20 | 4,00 |  | M 1919? | 16,20\% |  |  | 11750 |  |
| $164.7 \mathrm{~mm} / 45 \mathrm{M} 1893$ | 164,70 | 45,00 | 800,00 | 12,00 | AP | 2,35 | 2,00 | 4.0 | M 1887? |  |  |  | 9730 | Brennus, Guichen, Chateaurenault, Linois |
| " | 164,70 | 45,00 | 800,00 | 12,00 | Common | 2,84 | 2,00 |  | M 1887? |  |  |  | 9730 |  |
| " | 164,70 | 52,00 | 765,00 | 12,00 | APC | 2,50 | 2,00 |  | M 1900 | 13,46\% |  |  | 10000 |  |
| " | 164,70 | 55,00 | 770,00 | 12,00 | APC | 2,70 | 3,00 |  | M 1919? | 18,18\% |  |  | 10840 |  |
| $138.6 \mathrm{~mm} / 45 \mathrm{M} 1893$ - |  |  |  |  |  |  |  |  |  |  |  |  |  | Bouvet, Charlemagne, |
| 91 | 138,60 | 30,00 | 770,00 | 12,00 | AP | 2,63 | 2,00 | 5.5 | M 1893? |  |  |  | 7920 | Henri IV, Pothuau, Jeanne D'Arc, Friant, |
| " | 138,60 | 30,00 | 770,00 | 12,00 | Common | 3,18 | 2,00 |  | M 1887? |  |  |  | 7920 | Descartes, D'Assas, Catinat, Guichen, |
| " | 138,60 | 38,00 | 730,00 | 12,00 | CPC | 3,45 | 2,00 |  | M 1900 | 21,05\% |  |  | 8700 | Chateaurenault, |
| " | 138,60 | 36,50 | 725,00 | 12,00 | SAP | 3,60 | 2,00 |  | M 1910 |  |  |  | 8455 | Jurien de la Graviere Bouclier, Bisson, |
| 100mm/45 M1893-91 | 100,00 | 14,00 | 740,00 | 25,00 | Common | 3,94 | 2,00 | 7.0 | M 1881? |  |  |  | 10225 | Enseigne Roux, <br> Enseigne Gabolde, |
| " | 100,00 | 16,00 | 710,00 | 25,00 | CP | 3,20 | 2,00 |  | M 1905 |  | 10,63\% | M | 10750 | Bouvet, Massena |
| $340 \mathrm{~mm} / 42 \mathrm{M} 1887$ | 340,00 | 420,00 | 780,00 | 12,00 | AP | 2,49 | 2,00 | 5.0 | M 1887? |  |  |  | 12370 | Brennus, Jammapes |
| " | 340,00 | 420,00 | 780,00 | 12,00 | Common | 3,01 | 2,00 |  | M 1887? |  |  |  | 12370 |  |
| $305 \mathrm{~mm} / 45 \mathrm{M} 1887$ | 305,00 | 292,00 | 800,00 | 12,00 | AP | 2,40 | 2,00 | 5.0 | M 1887? |  | 3,60\% | M | 11623 | Charles Martel, Carnot, Jaureguiberry, |
| " | 305,00 | 292,00 | 800,00 | 12,00 | Common | 2,90 | 2,00 |  | M 1887? |  |  |  | 11623 |  |


| " | 305,00 | 340,00 | 780,00 | 12,00 | APC | 2,60 | 2,00 |  | M 1900 | 14,12\% | 3,09\% | M | 12000 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| " | 305,00 | 340,00 | 780,00 | 12,00 | CPC | 2,90 | 2,00 |  | M 1900 | 14,12\% |  |  | 12000 |  |
| " | 305,00 | 292,00 | 800,00 | 10,00 | AP | 2,40 | 2,00 | 5.0 | M 1887? |  | 3,60\% | M | 10579 | Bouvines |
| " | 305,00 | 292,00 | 800,00 | 10,00 | Common | 2,90 | 2,00 |  | M 1887? |  |  |  | 10579 |  |
| " | 305,00 | 340,00 | 780,00 | 10,00 | APC | 2,60 | 2,00 |  | M 1900 | 14,12\% | 3,09\% | M | 10879 |  |
| " | 305,00 | 340,00 | 780,00 | 10,00 | CPC | 2,90 | 2,00 |  | M 1900 | 14,12\% |  |  | 10879 |  |
| 274mm/45 M1887 | 274,40 | 216,00 | 800,00 | 15,50 | AP | 2,44 | 2,00 | 6.5 | M 1887? |  |  |  | 12800 | Charles Martel, Carnot, Jaureguiberry |
| " | 274,40 | 216,00 | 800,00 | 15,50 | Common | 2,95 | 2,00 |  | M 1887? |  |  |  | 12800 |  |
| " | 274,40 | 255,00 | 780,00 | 15,50 | APC | 2,70 | 2,00 |  | M 1900 | 15,29\% |  |  | 13310 |  |
| " | 274,40 | 255,00 | 780,00 | 15,50 | CPC | 3,00 | 2,00 |  | M 1900 | 15,29\% |  |  | 13310 |  |
| 194mm/45 M1887 | 194,00 | 75,00 | 800,00 | 11,00 | AP | 2,40 | 2,00 | 5.0 | M 1887? |  |  |  | 9046 | Dupuy de Lome, Amiral Charner |
| " | 194,00 | 75,00 | 800,00 | 11,00 | Common | 2,89 | 2,00 |  | M 1887? |  |  |  | 9046 |  |
| " | 194,00 | 86,00 | 770,00 | 12,00 | APC | 2,60 | 2,00 |  | M 1900 | 12,79\% |  |  | 9000 |  |
| " | 194,00 | 86,00 | 770,00 | 12,00 | CPC | 2,85 | 2,00 |  | M 1900 | 12,79\% |  |  | 9000 |  |
| $164.7 \mathrm{~mm} / 45 \mathrm{M} 1887$ | 164,70 | 45,00 | 800,00 | 12,00 | AP | 2,35 | 2,00 | 5.0 | M 1887? |  |  |  | 8490 | Dupuy de Lome, |
| " | 164,70 | 45,00 | 800,00 | 12,00 | Common | 2,84 | 2,00 |  | M 1887? |  |  |  | 8490 |  |
| " | 164,70 | 52,00 | 765,00 | 12,00 | APC | 2,50 | 2,00 |  | M 1900 | 13,46\% |  |  | 10000 |  |
| $138.6 \mathrm{~mm} / 45 \mathrm{M} 1887$ | 138,60 | 30,00 | 800,00 | 15,00 | Common | 3,18 | 2,00 | 3.5 | M 1881? |  |  |  | 9100 | Charles Martel, Carnot, Jairegioberry, <br> Massena, Amiral |
| " | 138,60 | 30,00 | 770,00 | 15,00 | Common | 3,18 | 2,00 |  | M 1887? |  |  |  | 8815 | Charner |
| " | 138,60 | 36,50 | 725,00 | 15,00 | Common | 3,70 | 2,00 |  | M 1910 |  |  |  | 9315 |  |
| 100mm/50 M1889 | 100,00 | 14,00 | 760,00 | 25,00 | Common | 3,94 | 2,00 | 6.5 | M 1881? |  |  |  | 10415 |  |
| " | 100,00 | 16,00 | 740,00 | 25,00 | CP | 3,20 | 3,00 |  | M 1905 |  | 10,63\% | M | 11085 |  |
| $340 \mathrm{~mm} / 30 \mathrm{M} 1884$ | 340,00 | 420,00 | 600,00 | 13,50 | AP | 2,49 | 2,00 | 4,0 | M 1887? |  |  |  | 9356 | Neptune |
| " | 340,00 | 350,00 | 621,00 | 13,50 | Common | 2,51 | 2,00 |  | M 1875? |  |  |  | 9109 |  |
| 274mm/30 M1884 | 274,40 | 216,00 | 600,00 | 35,00 | AP | 2,44 | 2,00 | 6.5 | M 1870? |  |  |  | 13903 | Coast Defence |
| " | 274,40 | 180,00 | 657,00 | 35,00 | Common | 2,45 | 2,00 |  | M 1870? |  |  |  | 13585 |  |
| 240mm/30 M1884 | 240,00 | 144,00 | 600,00 | 11,00 | AP | 2,43 | 2,00 | 3.5 | M 1870? |  |  |  | 7225 | re-armed [\#2] Redoutable |
| " | 240,00 | 120,00 | 657,00 | 11,00 | Common | 2,45 | 2,00 |  | M 1870? |  |  |  | 7356 |  |


| 5482 | Amiral Cecille |
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| 5482 |  |
| 7474 | Tage |
| 7474 |  |
| 11008 | Amiral Baudin, Tage, |
| 11008 | Amiral Cecille, Davout, |
| 11508 |  |
| 11508 |  |
| 7234 | Marhet, Forbin |
| 10604 | Amirala Cecille, Arethuse |
| Forbin, Inconstant, |  |
| 7614 |  |
| 11019 |  |


| 8710 | Hoche |
| :--- | :--- |
| 8506 |  |
| 9356 | Marceau, Magenta |
| 9109 |  |
| 7821 | Courbet |
| 8210 |  |
| 9373 | Amiral Duperre, Furieux |
| 9709 |  |
| 8512 | re-armed Devastation \#1 |
| 8746 |  |
| 9535 |  |
| 9702 |  |
| 8068 | Acheron |
| 8195 |  |
| 13903 |  |



M 1870?















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##  <br> ${ }_{\infty}$

super-charged
$274 \mathrm{~mm} / 28.5 \mathrm{M} 1881$



| $\stackrel{-1}{\Sigma}$ | $\begin{aligned} & \text { o. } \\ & \text { ò } \\ & \stackrel{1}{2} \end{aligned}$ | $\begin{aligned} & \text { o. } \\ & \text { ion } \\ & \stackrel{1}{\Sigma} \end{aligned}$ | $\begin{aligned} & \text { N. } \\ & \text { o } \\ & \text { in } \\ & \Sigma \end{aligned}$ | $\begin{aligned} & \text { ò } \\ & \infty \\ & \underset{\infty}{\infty} \end{aligned}$ | $\begin{aligned} & \text { ô } \\ & 0 \\ & \stackrel{1}{\infty} \\ & \dot{\Sigma} \end{aligned}$ | $\begin{aligned} & \text { N. } \\ & \text { ion } \\ & \stackrel{1}{\Sigma} \end{aligned}$ | $\begin{aligned} & \text { ö } \\ & \text { on } \\ & \underset{\sim}{n} \end{aligned}$ | $\begin{aligned} & \stackrel{0}{\circ} \\ & \stackrel{\infty}{\infty} \\ & \underset{\Sigma}{n} \end{aligned}$ | $\begin{aligned} & \text { N. } \\ & \substack{\infty \\ \stackrel{1}{1}} \end{aligned}$ | $\begin{aligned} & \text { Nij } \\ & \stackrel{\text { Non }}{+1} \end{aligned}$ | $\begin{aligned} & \hat{0} \\ & \stackrel{0}{\infty} \\ & \stackrel{N}{\Sigma} \end{aligned}$ |  | $\begin{aligned} & \text { N. } \\ & \text { م } \\ & \underset{\Sigma}{\infty} \end{aligned}$ | $\begin{aligned} & \text { c. } \\ & \text { on } \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \text { N } \\ & \text { ion } \\ & \underset{\Sigma}{\infty} \end{aligned}$ |  |  |  | $\Sigma$ |  |  |  | $\begin{aligned} & \stackrel{\sim}{n} \\ & \stackrel{0}{0} \\ & \stackrel{1}{2} \end{aligned}$ | $\begin{aligned} & \stackrel{N}{n} \\ & \underset{\sim}{\infty} \\ & \underset{\Sigma}{1} \end{aligned}$ | $\begin{aligned} & \stackrel{N}{n} \\ & \stackrel{y}{\infty} \\ & \stackrel{1}{2} \end{aligned}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
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| $\stackrel{\mathrm{N}}{\mathrm{~N}}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\underset{\sim}{\mathrm{N}}$ | $\stackrel{\mathrm{O}}{\mathrm{~N}}$ | $\underset{\sim}{\mathrm{N}}$ | $\begin{aligned} & 8 \\ & i \end{aligned}$ | $\stackrel{8}{\mathrm{~N}}$ | $\stackrel{\text { ® }}{\text { N }}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | O | $\begin{aligned} & 8 \\ & \text { N } \end{aligned}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\stackrel{8}{\mathrm{i}}$ | $\stackrel{\circ}{\mathrm{i}}$ | $\underset{\sim}{8}$ | $\stackrel{\text { ì }}{i}$ | $\stackrel{8}{\mathrm{~N}}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\underset{\sim}{\mathrm{N}}$ | $\stackrel{\circ}{\mathrm{N}}$ | oi | $\stackrel{\mathrm{i}}{\mathrm{~N}}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\stackrel{8}{\mathrm{~N}}$ | $\stackrel{\mathrm{N}}{\mathrm{~N}}$ | $\underset{\sim}{\mathrm{N}}$ |
| $\stackrel{\text { g }}{\sim}$ | $\underset{N}{\underset{N}{j}}$ | $\stackrel{\downarrow}{\sim}$ | $\underset{\sim}{Z}$ | $\stackrel{\unrhd}{N}$ | $\stackrel{\text { N}}{N}$ | $\stackrel{!}{\sim}$ | $\stackrel{\sim}{\sim}$ | $\stackrel{\llcorner }{\sim}$ | $\stackrel{N}{N}$ | $\begin{aligned} & \text { } \\ & \underset{\sim}{\circ} \end{aligned}$ | $\stackrel{\sim}{N}$ | $\stackrel{\underset{\sim}{\infty}}{\stackrel{+}{i}}$ | $\stackrel{\sim}{N}$ | $\underset{\sim}{\perp}$ | $\stackrel{\infty}{\stackrel{\infty}{m}}$ | $\stackrel{\infty}{\sim}$ | $\stackrel{\infty}{\sim}$ | $\underset{\sim}{\infty}$ | ボ |  | $\stackrel{\sim}{\infty}$ | $\stackrel{\circ}{\circ}$ | $\stackrel{\ominus}{N}$ | $\underset{\sim}{\underset{N}{N}}$ | $\stackrel{\text { ¢ }}{\substack{\text { N }}}$ | $\stackrel{\text { N }}{\text { N }}$ | $\stackrel{\sim}{\sim}$ |
|  | ¢ |  | 只 | $\begin{aligned} & \text { O} \\ & \text { O} \\ & \text { E} \\ & \text { OU } \end{aligned}$ | $\stackrel{\square}{4}$ |  | $\stackrel{\square}{8}$ |  | $\stackrel{0}{8}$ |  | ¢ |  | ¢ |  |  | ᄃ 0 0 0 0 |  | $\begin{aligned} & \text { Ø} \\ & \text { O} \\ & \text { O} \\ & 0 \end{aligned}$ | ©̄ | $\stackrel{\square}{8}$ | ¢ | U | ¢ | EOU | ¢ | ¢ |  |
| $\begin{aligned} & \mathrm{O} \\ & \stackrel{\rightharpoonup}{0} \\ & \hline \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{0}{i} \\ & \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 \\ & \hline-1 \end{aligned}$ | $\begin{aligned} & \text { Oin } \\ & \text { Con } \end{aligned}$ | $\begin{aligned} & \stackrel{0}{0} \\ & \stackrel{0}{0} \end{aligned}$ | $\begin{aligned} & 8 \\ & \underset{7}{-} \end{aligned}$ | $\stackrel{\circ}{-}$ | ৪্ল্লি | -( | $\begin{aligned} & \text { O} \\ & \text { in } \end{aligned}$ | $\begin{aligned} & 8 . \\ & \stackrel{8}{0} \end{aligned}$ | $8$ | $\begin{aligned} & 8 \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \stackrel{8}{2} \\ & \text { L్ల } \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{y}{0} \\ & \hline \end{aligned}$ | $8$ | $\begin{aligned} & 8 \\ & \stackrel{\rightharpoonup}{0} \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{\rightharpoonup}{\mathrm{H}} \end{aligned}$ | $\stackrel{8}{\mathrm{O}}$ | $\stackrel{\sim}{\sim}$ | $\stackrel{\otimes}{\mathrm{N}}$ | $\stackrel{\sim}{\sim}$ | -i | $\begin{aligned} & \mathrm{O} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \stackrel{8}{\mathrm{~N}} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \text { ৪ } \\ & \underset{\sim}{\prime} \end{aligned}$ | $\stackrel{8}{8}$ |
| $\begin{aligned} & \stackrel{8}{0} \\ & \stackrel{1}{0} \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{\circ}{\circ} \\ & \text { in } \end{aligned}$ |  | $\begin{aligned} & 8 \\ & \stackrel{8}{5} \\ & \stackrel{5}{5} \end{aligned}$ | $\begin{aligned} & 8 . \\ & 0.0 \\ & \hline \end{aligned}$ | 8 <br> 8 <br> 8 | $\begin{aligned} & 8 \\ & \stackrel{8}{5} \\ & \hline 1 \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 . \\ & 0 \end{aligned}$ | $\begin{aligned} & \text { 8} \\ & \stackrel{y}{0} \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{\rightharpoonup}{0} \\ & \text { R } \end{aligned}$ | 8 $\stackrel{3}{0}$ 융 | 8 <br> 8 | 8 <br> 8 <br> 0 | 8 <br> 0 <br> 0 | 8 <br> 8 <br> 0 <br> 0 | 8 <br> 8 <br> 8 | 8 <br> 8 <br> 8 | $\begin{aligned} & \text { O} \\ & \text { O} \\ & \text { GO } \end{aligned}$ | $\begin{aligned} & \mathrm{B} \\ & \stackrel{y}{6} \\ & \text { O} \end{aligned}$ | in | $\begin{aligned} & 8 \\ & 8 . \\ & 0 \end{aligned}$ | Oio |  | $\begin{aligned} & \stackrel{8}{0} \\ & \stackrel{0}{0} \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { Oin } \\ & \text { N } \end{aligned}$ | $\begin{aligned} & 8 \\ & \hline . \\ & \text { O} \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{0}{0} \\ & \text { in } \end{aligned}$ | 8 |
| $\begin{aligned} & \circ \\ & \stackrel{\circ}{0} \\ & \text { © } \\ & \text { O- } \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{8}{0} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \circ \\ & \hline 0 \\ & \hline 0 \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { - } \\ & \text { - } \end{aligned}$ | $\stackrel{8}{\circ}$ | 8 咢 | $\begin{aligned} & \text { O} \\ & \text { ̇․ } \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{\rightharpoonup}{J} \\ & \underset{\sim}{\prime} \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{\circ}{-} \\ & \text { त्र } \end{aligned}$ |  | $\begin{aligned} & \stackrel{8}{2} \\ & \text { 令 } \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { ¢ } \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { \& } \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { \&in } \end{aligned}$ |  | $8$ | $\stackrel{\circ}{0}$ | $\stackrel{\circ}{\circ}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{0} \\ & \stackrel{\rightharpoonup}{m} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \underset{\sim}{\mathrm{~J}} \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{\dot{J}} \\ & \text {. } \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{-} \\ & \underset{\sim}{2} \end{aligned}$ | $\stackrel{8}{\circ}$ | $\begin{aligned} & \text { O} \\ & \text { O } \\ & \text { © } \end{aligned}$ | $\begin{aligned} & 8 \\ & \hline 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & \circ \\ & \text { O. } \\ & \text { D } \end{aligned}$ | O | 8 |
| $\begin{gathered} \text { O} \\ \underset{\sim}{N} \end{gathered}$ | $$ | $\begin{aligned} & \stackrel{g}{\mathrm{~J}} \\ & \underset{\sim}{\prime} \end{aligned}$ | $\begin{aligned} & \text { o} \\ & \text { 寺 } \end{aligned}$ | $\begin{aligned} & \text { o} \\ & \underset{\sim}{A} \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{8}{\circ} \\ & \text { d } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \stackrel{-}{-} \\ & \text { d } \end{aligned}$ | $\circ$ <br> － <br> － <br>  | $\begin{aligned} & \text { O} \\ & \text { O} \\ & \text { d } \end{aligned}$ | $\begin{aligned} & \stackrel{Q}{0} \\ & \underset{\sim}{\prime} \end{aligned}$ | $\begin{aligned} & \text { ○ } \\ & \stackrel{+}{+} \\ & \stackrel{1}{2} \end{aligned}$ | $\begin{aligned} & \text { Q } \\ & \text { + } \\ & \text { + } \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{0} \\ & \stackrel{\text { N }}{+} \end{aligned}$ | $\circ$ $\stackrel{+}{+}$ $\stackrel{+}{+}$ | $\begin{aligned} & \text { ค } \\ & \stackrel{\text { d }}{+} \end{aligned}$ | $\begin{aligned} & \circ \\ & 0 \\ & \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{0} \\ & \infty \\ & \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{0} \\ & \infty \\ & \underset{\sim}{\circ} \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{\infty} \\ & \infty \\ & \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 . \\ & 0 \\ & \hline \end{aligned}$ | 8 8 -1 | O- | － | $\begin{aligned} & 8 \\ & \text { B } \\ & \text { H } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & 8 \\ & \underset{\sim}{7} \end{aligned}$ | 국 | $8$ |



|  |  | 10389 |  |
| :---: | :---: | :---: | :---: |
|  |  | 7066 | Courbet |
|  |  | 7481 |  |
|  |  | 8541 | Furieux |
|  |  | 8922 |  |
|  |  | 6700 | Devastation, Courbet |
|  |  | 6776 |  |
|  |  | 8138 | Amiral Duperre, Tonnant, Furieux |
|  |  | 8158 |  |
|  |  | 5890 | Vengeur |
|  |  | 5994 |  |
|  | BP | 5773 | Redoutable |
| 6,08\% | BP | 5514 |  |
|  | BP | 7240 |  |
| 6,08\% | BP | 6873 |  |
|  | BP | 9048 |  |
| 6,08\% | BP | 8545 |  |
|  | BP | 11971 |  |
| 6,08\% | BP | 11200 |  |
|  | BP | 5337 | Courbet, Tonnerre, Tempete |
| 6,08\% | BP | 5514 |  |
|  | BP | 8507 | Courbet |
| 6,08\% | BP | 8545 |  |
|  | BP | 11100 | Courbet |
| 6,08\% | BP | 10969 |  |
|  |  | 5412 |  |
|  |  | 5681 |  |
|  |  | 9700 | Coast Defence |
|  |  | 4900 |  |
|  |  | 4240 |  |




| $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\begin{aligned} & 8 \\ & \mathrm{~N} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { N } \end{aligned}$ | O | $\begin{aligned} & \mathrm{O} \\ & \text { in } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| ก7 | 7 | $\xrightarrow{-1}$ | $\stackrel{9}{7}$ | $\cdots$ | \% |
| N | N | $\cdots$ | $\sim$ | $\cdots$ | N |


| jacketed | 100,00 | 14,00 | 510,00 | 10,00 | Common | 3,94 | 2,00 |  |  |  |  | 4660 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $90 \mathrm{~mm} / 25.3 \mathrm{M} 1878$ | 90,00 | 7,90 | 455,00 | 20,00 | Common | 3,05 | 2,00 | 3.6 | M 1878? |  |  | 3750 |  |
| $90 \mathrm{~mm} / 24 \mathrm{M} 1877$ | 90,00 | 8,30 | 455,00 | 20,00 | Common | 3,21 | 2,00 | 3.5 | M 1875? |  |  | 3800 |  |
| $320 \mathrm{~mm} / 19.5 \mathrm{M} 1870$ | 320,00 | 345,00 | 438,00 | 14,00 | AP | 2,46 | 2,00 | 4.0 | M 1870? |  |  | 6475 | Coast Defence |
| " | 320,00 | 286,00 | 480,00 | 14,00 | Common | 2,46 | 2,00 |  | M 1870? | 5,87\% | BP | 6826 |  |
| $320 \mathrm{~mm} / 19.5 \mathrm{M}$ 1870M | 320,00 | 345,00 | 470,00 | 14,00 | AP | 2,46 | 2,00 | 4.0 | M 1870? |  |  | 7050 |  |
| " | 320,00 | 309,00 | 496,00 | 14,00 | Common | 2,66 | 2,00 |  | M 1870? | 5,44\% | BP | 7240 |  |
| 274mm/17.98 M1870 | 274,40 | 216,00 | 434,00 | 14,00 | AP Shot | 2,44 | 2,00 | 3.5 | M 1870? |  |  | 6167 | Ocean, Friedland, Richelieu, Colbert |
| " | 274,40 | 180,00 | 475,00 | 14,00 | Common | 2,45 | 2,00 |  | M 1870 | 6,08\% | BP | 6450 |  |
| " | 274,40 | 216,00 | 434,00 | 25,00 | AP Shot | 2,44 | 2,00 | 3.5 |  |  |  | 8953 | Friedland, Colbert |
| " | 274,40 | 180,00 | 475,00 | 25,00 | Common | 2,45 | 2,00 |  |  | 6,08\% | BP | 9175 |  |
| $\begin{aligned} & 274 \mathrm{~mm} / 17.98 \mathrm{M} \\ & 1870 \mathrm{M} \end{aligned}$ | 274,40 | 216,00 | 480,00 | 14,00 | AP Shell | 2,44 | 2,00 | 3.5 | M 1875 |  | BP | 6914 | Ocean, Friedland, Richelieu, Colbert |
| " | 274,40 | 180,00 | 510,00 | 14,00 | Common | 2,45 | 2,00 |  | M 1870 | 6,08\% | BP | 6944 |  |
| " | 274,40 | 216,00 | 480,00 | 25,00 | AP Shell | 2,44 | 2,00 | 3.5 | M 1875 |  | BP | 9830 | Friedland, Colbert |
| " | 274,40 | 180,00 | 510,00 | 25,00 | Common | 2,45 | 2,00 |  | M 1870 | 6,08\% | BP | 9746 |  |
| $240 \mathrm{~mm} / 18.1 \mathrm{M} 1870$ | 240,00 | 144,00 | 440,00 | 10,00 | AP | 2,43 | 2,00 | 2.5 | M 1870? |  |  | 4766 | Colbert, Cerbere |
| " | 240,00 | 120,00 | 482,00 | 10,00 | Common | 2,45 | 2,00 |  | M 1870? |  |  | 5065 |  |
| " | 240,00 | 144,00 | 440,00 | 14,00 | AP | 2,43 | 2,00 | 2.5 |  |  |  | 6067 | La Galissonniere |
| " | 240,00 | 120,00 | 482,00 | 14,00 | Common | 2,45 | 2,00 |  |  |  |  | 6341 |  |
| " | 240,00 | 144,00 | 440,00 | 20,00 | AP | 2,43 | 2,00 | 2.5 |  |  |  | 7692 | Ocean, Richelieu, La Galissonniere, |
| " | 240,00 | 120,00 | 482,00 | 20,00 | Common | 2,45 | 2,00 |  |  |  |  | 7914 | Bayard, Vauban |
| " | 240,00 | 144,00 | 440,00 | 33,00 | AP | 2,43 | 2,00 | 2.5 |  |  |  | 10069 | Colbert |
| " | 240,00 | 120,00 | 482,00 | 33,00 | Common | 2,45 | 2,00 |  |  |  |  | 10175 |  |
| 240mm/18.1 M 1870M | 240,00 | 144,00 | 495,00 | 14,00 | AP | 2,43 | 2,00 | 2.5 | M 1870? |  |  | 6889 |  |
| " | 240,00 | 120,00 | 523,00 | 14,00 | Common | 2,45 | 2,00 |  | M 1870? |  |  | 6876 |  |
| " | 240,00 | 144,00 | 495,00 | 20,00 | AP | 2,43 | 2,00 | 2.5 |  |  |  | 8601 |  |
| " | 240,00 | 120,00 | 523,00 | 20,00 | Common | 2,45 | 2,00 |  |  |  |  | 8495 |  |
| $194 \mathrm{~mm} / 19.8 \mathrm{M} 1870$ | 194,00 | 75,00 | 448,00 | 10,00 | AP Shot | 2,42 | 2,00 | 2.5 | M 1870 |  |  | 4567 | Couronne, Belliqueuse, Alma, |


| 4785 8231 | La Galissonniere, Bayard, Vauban Duguay-Trouin, Duquesne, Tourville |
| :---: | :---: |
| 8272 |  |
| 5539 |  |
| 5707 |  |
| 9445 |  |
| 9379 |  |
| 5115 | Iphigenie, Naiade, Alma |
| 5497 |  |
| 7667 | Bourayne, Guichen |
| 7851 |  |
| 8116 | Alma |
| 8245 |  |
| 6658 | Iphigenie, Naiade, Alma |
| 6658 |  |
| 9448 | Bourayne, Guichen |
| 9448 |  |
| 9943 | Alma |
| 9943 |  |
|  | Friedland, Bayard, |
| 5145 | Tourville, Duquesne, |
| 7355 | Naiade, Iphigenie |
| 7925 |  |
| 5113 | Richelieu, Colbert, Redoutable, Villars, Sane, La Galissonniere, Du- |
| 7600 | guay-Trouin, Laperouse, |
| 8308 |  |
|  | Redoutable, Amiral |
| 5741 | Duperre |
| 8340 |  |
| 9081 |  |


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| $\begin{aligned} & \stackrel{\circ}{0} \\ & \stackrel{0}{-} \\ & - \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \stackrel{1}{-} \\ & \stackrel{1}{*} \end{aligned}$ |


| " | 194,00 | 62,00 | 492,70 | 10,00 | Common | 2,65 | 2,00 | 2.5 | M 1870 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| " | 194,00 | 75,00 | 448,00 | 25,00 | AP Shot | 2,42 | 2,00 | 2.5 | M 1870 |
| " | 194,00 | 62,00 | 492,70 | 25,00 | Common | 2,65 | 2,00 | 2.5 | M 1870 |
| $194 \mathrm{~mm} / 19.8 \mathrm{M} \mathrm{1870M}$ | 194,00 | 75,00 | 534,00 | 10,00 | AP Shell | 2,82 | 2,00 | 2.5 | M 1870 |
| " | 194,00 | 62,50 | 585,00 | 10,00 | Common | 2,68 | 2,00 | 2.5 | M 1870 |
| " | 194,00 | 75,00 | 534,00 | 25,00 | AP Shell | 2,82 | 2,00 | 2.5 | M 1870 |
| " | 194,00 | 62,50 | 585,00 | 25,00 | Common | 2,68 | 2,00 | 2.5 | M 1870 |
| $164.7 \mathrm{~mm} / 21.2 \mathrm{M} 1870$ | 164,70 | 45,00 | 400,00 | 15,00 | AP |  | 2,00 | 2.5 | M 1870? |
| " | 164,70 | 31,30 | 480,00 | 15,00 | Common |  | 2,00 |  | M 1870? |
| " | 164,70 | 45,00 | 400,00 | 30,00 | AP |  | 2,00 | 2.5 |  |
| " | 164,70 | 31,30 | 480,00 | 30,00 | Common |  | 2,00 |  |  |
| " | 164,70 | 45,00 | 400,00 | 35,00 | AP |  | 2,00 | 2.5 |  |
| " | 164,70 | 31,30 | 480,00 | 35,00 | Common |  | 2,00 |  |  |
|  |  |  |  |  |  |  |  |  |  |
| 1870M | 164,70 | 45,00 | 544,00 | 15,00 | AP |  | 2,00 | 2.5 |  |
| " | 164,70 | 45,00 | 544,00 | 15,00 | Common |  | 2,00 |  |  |
| " | 164,70 | 45,00 | 544,00 | 30,00 | AP |  | 2,00 | 2.5 |  |
| " | 164,70 | 45,00 | 544,00 | 30,00 | Common |  | 2,00 |  |  |
| " | 164,70 | 45,00 | 544,00 | 35,00 | AP |  | 2,00 | 2.5 |  |
| " | 164,70 | 45,00 | 544,00 | 35,00 | Common |  | 2,00 |  |  |
| $138.6 \mathrm{~mm} / 21.1 \mathrm{M} 1870$ | 138,60 | 21,00 | 455,00 | 15,00 | Common | 2,22 | 2,00 | 7,0 | M 1870? |
| " | 138,60 | 21,00 | 455,00 | 30,00 | Common |  | 2,00 | 7,0 |  |
| " | 138,60 | 21,00 | 455,00 | 42,00 | Common |  | 2,00 | 7,0 |  |
| " | 138,60 | 28,00 | 406,00 | 15,00 | Common | 2,96 | 2,00 | 7,0 | M 1875 |
| " | 138,60 | 28,00 | 406,00 | 30,00 | Common |  | 2,00 | 7,0 |  |
| " | 138,60 | 28,00 | 406,00 | 42,00 | Common |  | 2,00 | 7,0 |  |
| $138.6 \mathrm{~mm} / 21.1 \mathrm{M}$ |  |  |  |  |  |  |  |  |  |
| 1870M | 138,60 | 28,00 | 466,00 | 15,00 | Common | 2,96 | 2,00 | 7,0 | M 1875 |
| " | 138,60 | 28,00 | 466,00 | 30,00 | Common |  | 2,00 | 7,0 |  |
| " | 138,60 | 28,00 | 466,00 | 42,00 | Common |  | 2,00 | 7,0 |  |
| 120mm/25 M1870 | 120,00 | 14,80 | 455,00 | 10,00 | Common | 2,41 | 2,00 | 4.0 | M 1870? |


| 90mm/36 M1870 | 90,00 | 7,90 | 455,00 | 12,00 | Common | 3,05 | 2,00 | 3,5 |  |  |  | 3750 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 274mm/18 M1864-66 | 274,00 | 216,00 | 331,00 | 14,00 | AP Shot |  | 2,00 | 3.5 | M 1864 |  |  | 4413 | Ocean |
| " | 274,00 | 144,00 | 361,90 | 14,00 | Common |  | 2,00 |  | M 1864 |  |  | 4682 |  |
| 240mm/17.5 M186466 | 240,00 | 144,00 | 340,00 | 10,00 | AP Shot |  | 2,00 | 2.0 | M 1864? |  |  | 3450 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  | Magenta, Provence, |
| " | 240,00 | 100,00 | 363,60 | 10,00 | Common |  | 2,00 |  | M 1864? |  |  | 3560 | Taureau |
| " | 240,00 | 144,00 | 340,00 | 16,50 | AP Shot |  | 2,00 | 2.0 | M 1864? |  |  | 5155 | Magenta |
| " | 240,00 | 100,00 | 363,60 | 16,50 | Common |  | 2,00 |  | M 1864? |  |  | 5182 |  |
| " | 240,00 | 144,00 | 340,00 | 25,00 | AP Shot |  | 2,00 | 2.0 | M 1864? |  |  | 6873 | Ocean |
| " | 240,00 | 100,00 | 363,60 | 25,00 | Common |  | 2,00 |  | M 1864? |  |  | 6773 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  | Gloire (re-armament 3), Couronne (re-armament |
| 194mm/19 M1864 | 194,00 | 75,00 | 341,00 | 15,00 | AP Shot |  | 2,00 | 2.0 | M 1864 |  |  | 4551 | 1), Embuscade |
| " | 194,00 | 52,25 | 366,00 | 15,00 | Comm |  | 2,00 |  | M 1864 |  |  | 4632 |  |
| $164.7 \mathrm{~mm} / 18 \mathrm{M} 1864$ | 164,70 | 31,30 | 392,50 | 15,00 | Common | 2,12 | 2,00 | 2.0 | M 1860? | 4,14\% | BP | 4604 | Gloire (re-armament 2) |
| " | 164,70 | 30,00 | 400,00 | 15,00 | AP Shot | 1,48 | 2,00 |  |  |  |  | 4556 |  |
| $138.6 \mathrm{~mm} / \mathrm{M} 1864$ | 138,60 | 21,00 |  | 15,00 | Comm |  | 2,00 |  | M 1864 |  |  |  |  |
| $164.7 \mathrm{~mm} / 17.9$ M1858- <br> 60 | 164,70 | 31,30 | 317,00 | 15,00 | Common | 2,12 | 2,00 | 2.0 | M 1860? | 4,14\% | BP | 3827 | Gloire (armament 1), Couronne, Magenta, Palestro |
| $138.6 \mathrm{~mm} / 16$ | 164,70 | 30,00 | 353,70 | 15,00 | AP Shot | 1,48 | 2,00 |  | M 1859 |  |  | 4133 |  |
| $\begin{aligned} & 138.6 \mathrm{~mm} / 16.7 \\ & \text { M1858-60 } \end{aligned}$ | 138,60 | 21,00 | 325,00 | 15,00 | Common | 2,12 | 2,00 | 2.5 | M 1858 |  | BP | 3887 |  |
| $120 \mathrm{~mm} / 16 \mathrm{M} 1858-60$ <br> $164.7 \mathrm{~mm} / 17.9$ MLR | 120,00 | 17,40 | 419,00 | 15,00 | Common | 2,80 | 2,00 | 2.5 | M 1860? |  |  | 4795 |  |
| M1858 <br> Marie Jeanne 30-pdr | 164,70 | 31,30 | 322,00 | 15,00 | Common | 2,12 | 2,00 | 2.5 | M 1858 | 4,14\% | BP | 3833 | Gloire |
| (10kg chg) Marie Jeanne 30 -pdr | 164,70 | 30,00 | 480,00 | 35,00 | Shot | 1,68 | 2,00 | 2.0 |  |  |  | 7675 | Test Gun |
| ( 12 kg chg ) <br> Marie Jeanne 30-pdr | 164,70 | 30,00 | 505,00 | 35,00 | Shot | 1,68 | 2,00 | 2.0 |  |  |  | 7890 | Test Gun |
| ( 12 kg chg ) <br> Marie Jeanne $30-\mathrm{pdr}$ | 164,70 | 45,00 | 413,00 | 35,00 | Shot | 2,53 | 2,00 | 2.0 |  |  |  | 8300 | Test Gun |
| (12kg chg) | 164,70 | 80,00 | 309,00 | 35,00 | Shot | 4,49 | 2,00 | 2.0 |  |  |  | 7370 | Test Gun |
| 164.7 mm M1855 (/16) | 164,70 | 26,40 | 347,00 | 21,00 | Common | 1,48 | 2,00 | 2.5 |  |  |  | 4925 | gunboats 1856 |
| Canon-Obusier 50 | 194,00 | 25,25 | 509,00 | 5,00 | BALL | 1,00 | 1,00 | 2,00 |  |  |  | 1740 | Couronne, Magenta |


| Canon-Obusier 30 | 164,70 | 15,00 | 485,00 | 5,00 | BALL | 1,00 | 1,00 | 2,50 |  |  |  | 1739 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SOVIET UNION |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 406mm/50 B-37 | 406,40 | 1108,00 | 830,00 | 45,00 | APCBC | 4,68 | 8,00 | 4,5 | M.1915/28 | 2,32\% | T | 45670 | Sovyetskiy Soyuz |
| " | 406,40 | 1108,00 | 830,00 | 45,00 | SAPCBC | 5,00 | 8,00 | 4,5 | M.1915/28 | 7,94\% | T | 45670 |  |
| $305 \mathrm{~mm} / 56$ | 305,00 | 470,00 | 900,00 | 45,00 | APCBC | 4,70 | 12,50 | 4.6 | M. 1928 |  |  | 47580 | Kronshtadt |
| " | 305,00 | 470,00 | 900,00 | 45,00 | SAPBC | 5,00 | 12,50 | 4.6 | M. 1928 |  |  | 47580 |  |
| $180 \mathrm{~mm} / 57$ | 181,00 | 97,50 | 920,00 | 50,00 | APCBC | 5,04 | 12,50 | 4.3 | M. 1928 | 2,00\% | T | 37494 | Krasnyi Kavkaz, Kirov, Maxim Gorkiy |
| " | 181,00 | 97,50 | 920,00 | 50,00 | SAPCBC | 5,30 | 12,50 | 4.3 | M. 1928 | 7,18\% | T | 37494 |  |
| " | 181,00 | 97,50 | 920,00 | 50,00 | CPC | 5,30 | 12,50 | 4.3 | M. 1928 | 8,06\% | T | 37494 |  |
| $152 \mathrm{~mm} / 57$ | 152,40 | 55,00 | 950,00 | 45,00 | APCBC | 4,50 | 8,00 | 4,5 | M.1915/28 | 2,00\% | T | 30070 | Sovyetskiy Soyus, Kronshtadt, Chapayev |
| " | 152,40 | 55,00 | 950,00 | 45,00 | SAPCBC | 4,84 | 8,00 | 4,5 | M.1915/28 | 7,31\% | T | 30070 |  |
| " | 152,40 | 55,00 | 950,00 | 45,00 | CPC | 5,11 | 8,00 | 4,5 | M.1915/28 | 10,91\% | T | 30070 |  |
| 130mm/50 B-13 | 130,00 | 33,50 | 870,00 | 50,00 | SAPBC | 5,00 | 12,50 | 3,0 | M. 1928 | 7,01\% | T | 25731 | Tashkent, Gnevnyi, Kiev, Storohevoi |
| " | 130,00 | 33,50 | 870,00 | 50,00 | SAPBC | 4,82 | 12,50 | 3,0 | M. 1928 | 4,99\% | T | 25731 |  |
| " | 130,00 | 33,50 | 870,00 | 50,00 | CPC | 4,90 | 12,50 | 3,0 | M. 1928 | 8,09\% | T | 25731 |  |
| $102 \mathrm{~mm} / 45 \mathrm{~B}-2$ | 101,60 | 17,50 | 755,00 | 45,00 | CPC | 5,00 | 4,00 | 4,4 | M1915 | 12,00\% | T | 16470 |  |
| $100 \mathrm{~mm} / 47$ | 100,00 | 15,80 | 800,00 | 45,00 | CPC | 5,05 | 6,00 | 5,0 | M. 1915 | 12,47\% | T | 18546 |  |
| " | 100,00 | 15,80 | 800,00 | 45,00 | SAPCBC | 5,20 | 12,50 | 5,0 | M. 1928 | 7,85\% | T | 19570 |  |
| 100mm/51 B-24 | 100,00 | 15,80 | 872,00 | 45,00 | SAPCBC | 5,20 | 12,50 | 4.7 | M. 1928 | 8,23\% | T | 22314 |  |
| 100MM/56 B-24m | 100,00 | 15,80 | 895,00 | 85,00 | SAPCBC | 5,20 | 12,50 | 4,7 | M. 1928 | 8,23\% | T | 23005 | Kirov, Maxim Gorkiy, Chapayev |
| $76 \mathrm{~mm} / 55 \mathrm{~K}-34$ | 76,20 | 6,60 | 813,00 | 85,00 | SAP | 4,00 | 4,00 | 4.4 | M. 1928 |  |  | 13500 |  |
| IMPERIAL RUSSIA |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 16"/45 M. 1916 | 406,40 | 1116,00 | 758,00 | 25,00 | APCBC | 3,89 | 6,00 | 8.8 | M. 1915 |  |  | 26160 | Imperator Nikolai I, design 1916 |
| " | 406,40 | 1116,00 | 758,00 | 25,00 | SAPCBC | 4,25 | 6,00 | 8.8 | M. 1915 |  |  | 26160 |  |
| " | 406,40 | 1116,00 | 758,00 | 25,00 | CPCBC | 4,73 | 6,00 | 8.8 | M. 1915 |  |  | 26160 |  |


| 6242 | planned for Petr Veliki |
| ---: | :--- |
| 5993 |  |
| 23200 | Borodino |
| 23200 |  |
| 23228 | Gangut, Imperatritsa |
| 23228 | Mariya |
| 22614 |  |
| 22614 | Tri Svititelia, Sissoi Veli- |
| 14630 | ki, Petropavlovsk |
| 14630 | Potemkin, Retvisan, |
| 16276 | Tsessarevitch, Borodino |
| 16276 | Slava, Tsessarevich |
| 21031 | Tri Svititelia (1912), |
| 21031 | Slava (1916) |
| 24140 | Evsatfi, Andrei |
| 24140 | Pervoswanni, |
| 10614 | Tchesma \& Georgi |
| 10614 | Pobiedonosets |
| 10058 |  |
| 10058 |  |
| 10614 |  |
| 13168 |  |
| 13168 |  |
| 13168 |  |
| 9510 | Navarin |
| 9510 |  |
| 8870 |  |
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16-inch/20 M. 1867




| 254,00 | 225,20 | 693,00 | 35,00 | Common | 3,60 | 2,00 | 6.5 | M.1884/04 | 4,26\% | W | 17373 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 254,00 | 225,20 | 777,00 | 30,00 | APC | 3,00 | 2,00 | 6.5 | M. 1896 | 0,89\% | W | 18288 | Pobeda |
| 254,00 | 225,20 | 777,00 | 30,00 | CP | 3,20 | 2,00 | 6.5 | M. 1898 | 3,86\% | W | 18288 |  |
| 254,00 | 225,20 | 777,00 | 30,00 | Common | 3,60 | 2,00 | 6.5 | M.1884/04 | 4,26\% | W | 18288 |  |
| 254,00 | 225,20 | 693,00 | 35,00 | APC | 3,07 | 3,00 | 6.5 | M. 1907 | 1,73\% | T | 21031 | Rostislav |
| 254,00 | 225,20 | 693,00 | 35,00 | CP | 4,00 | 3,00 | 6.5 | M. 1907 | 12,57\% | T | 21031 |  |
| 254,00 | 225,20 | 693,00 | 35,00 | CP | 3,20 | 3,00 | 6.5 | M. 1911 | 3,86\% | T | 21031 |  |
| 228,60 | 126,10 | 653,00 | 15,00 | AP | 2,60 | 2,00 | 3.7 | M. 1891 | 1,78\% | BP | 9343 | Imperator Alexandr II, Gangut, Grozyaschchi, |
| 228,60 | 126,10 | 653,00 | 15,00 | Common | 2,70 | 2,00 | 3.7 | M. 1891 | 4,44\% | BP | 9343 |  |
| 228,60 | 208,80 | 534,00 | 15,00 | AP | 3,50 | 2,00 | 3.7 | M. 1894 | 2,87\% | BP | 9005 |  |
| 228,60 | 208,80 | 534,00 | 15,00 | Common | 4,20 | 2,00 | 3.7 | M. 1894 | 5,32\% | BP | 9005 |  |
| 228,60 | 188,40 | 569,00 | 15,00 | AP |  | 2,00 | 3.7 | M. 1896 | 2,97\% | W | 9250 |  |
| 228,60 | 126,10 | 709,00 | 15,00 | CP | 2,70 | 2,00 | 3.7 | M. 1896 | 4,76\% | W | 9998 |  |
| 228,60 | 126,10 | 561,00 | 12,00 | AP | 2,50 | 2,00 | 3.7 | M. 1877 | 1,31\% | BP | 7037 | Sivuch |
| 228,60 | 113,40 | 561,00 | 12,00 | Common | 2,50 | 2,00 | 3.7 | M. 1877 | 4,43\% | BP | 6902 |  |
| 228,60 | 126,10 | 597,00 | 12,00 | AP | 2,60 | 2,00 | 3.7 | M. 1891 | 1,78\% | BP | 7489 |  |
| 228,60 | 126,10 | 597,00 | 12,00 | CP | 2,70 | 2,00 | 3.7 | M. 1891 | 4,76\% | BP | 7489 | armed Latnik |
| 228,60 | 126,10 | 471,00 | 9,00 | AP | 2,50 | 2,00 | 2.5 | M. 1877 | 0,65\% | BP | 4726 | Lava, Charodeika |
| 228,60 | 113,40 | 486,00 | 9,00 | Common | 2,50 | 2,00 | 2.5 | M. 1877 | 4,43\% | BP | 4771 |  |
| 228,60 | 126,10 | 471,00 | 9,00 | Common | 2,70 | 2,00 | 2.5 | M. 1891 | 4,44\% | W | 4704 |  |
| 228,60 | 126,10 | 420,00 | 9,00 | AP | 2,20 | 2,00 | 2.5 | M. 1867 | 0,65\% | BP | 3917 | Bronenosetz, Smerch, Charodeika, Admiral Lazaev, |
| 228,60 | 122,80 | 434,00 | 9,00 | Common | 2,40 | 2,00 | 2.5 | M. 1867 | 3,84\% | BP | 4023 | Admiral Chichagov |
| 228,60 |  |  |  | Shot |  |  |  |  |  |  |  |  |
| 228,60 |  |  |  | Common |  |  |  |  |  |  |  |  |
| 203,20 | 112,20 | 807,70 | 35,00 | CPC | 3,89 | 2,00 | 8.0 | M. 1907 | 12,57\% | $T$ | 17585 | Imperator Pavel, Rurik <br> (ii) |
| 203,20 | 112,20 | 807,70 | 19,00 | CPC | 3,89 | 2,00 | 8.0 | M. 1907 | 12,57\% | T | 14283 | (casemates) |
| 203,20 | 139,20 | 792,50 | 35,00 | CPC | 4,75 | 4,00 | 8.0 | M. 1913 | 10,99\% | T | 23574 |  |
| 203,20 | 139,20 | 792,50 | 19,00 | CPC | 4,75 | 4,00 | 8.0 | M. 1913 | 10,99\% | T | 17889 |  |
| 203,20 | 112,20 | 807,70 | 35,00 | SAPC | 3,85 | 4,00 | 8.0 | M. 1915 | 6,77\% | T | 20593 |  |



|  |  |  |  |  |  |  |  |  |  | $\begin{aligned} & \text { N } \\ & \stackrel{0}{0} \\ & \frac{0}{3} \\ & \underline{y} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \stackrel{\infty}{0} \\ & \stackrel{1}{0} \end{aligned}$ | $\begin{aligned} & \text { N } \\ & \stackrel{0}{2} \\ & \stackrel{\sim}{2} \end{aligned}$ | $\begin{aligned} & \infty \\ & \stackrel{\sim}{0} \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & \text { ö } \\ & \stackrel{+}{\text { I }} \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \stackrel{1}{7} \end{aligned}$ | $\begin{aligned} & \dot{\theta} \\ & \underset{\sim}{\sim} \end{aligned}$ | $\begin{aligned} & \text { ® } \\ & \text { O } \\ & 0 \end{aligned}$ | $$ |  | $\begin{gathered} \underset{\sigma}{J} \\ \underset{\sigma}{2} \end{gathered}$ | $\begin{aligned} & \underset{ন}{J} \\ & \underset{\sigma}{2} \end{aligned}$ | $\begin{aligned} & \text { L } \\ & \text { O } \\ & \infty \end{aligned}$ | $\begin{aligned} & \text { 毋 } \\ & \text { \& } \\ & \infty \end{aligned}$ | $\begin{aligned} & \text { N } \\ & \text { No } \end{aligned}$ | N | $\stackrel{\substack{\mathrm{N} \\ \stackrel{N}{n}}}{ }$ | $\underset{\sim}{\mathcal{F}}$ | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \underset{\sim}{2} \end{aligned}$ | $\begin{aligned} & \stackrel{\ominus}{\circ} \\ & \underset{6}{2} \end{aligned}$ | $\stackrel{\sim}{N}$ | $\underset{\sim}{\sim}$ | $\underset{\substack{\text { H } \\ \text { On }}}{ }$ | $\begin{aligned} & \text { N } \\ & \underset{\sim}{0} \end{aligned}$ | $\underset{i}{\underset{\sim}{Z}}$ | $\begin{gathered} \hat{N} \\ \underset{\sim}{2} \end{gathered}$ | $\begin{aligned} & \text { of } \\ & \underset{\sim}{0} \end{aligned}$ | ¢ | กٌ |
| $\vdash$ | $\vdash$ | $\vdash$ |  | 3 | $\vdash$ |  |  | $\vdash$ | 0 | 0 | 0 | ） | 3 | 3 | 0 | － | 0 | ¢ | 3 | 3 |  |  |  |  |  |  |  |
| $\stackrel{\stackrel{\rightharpoonup}{\mathrm{N}}}{\stackrel{\circ}{6}}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{\circ} \\ & \underset{\sim}{9} \\ & \end{aligned}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{\mathrm{N}} \\ & \text { ल్త్ } \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \text { è } \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \stackrel{\infty}{\infty} \end{aligned}$ | $\begin{aligned} & \text { oे } \\ & \stackrel{0}{0} \\ & \underset{-1}{2} \end{aligned}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{\circ} \\ & \text { io } \end{aligned}$ | $\underset{\substack{\circ \\ \stackrel{\rightharpoonup}{n}}}{ }$ | $\begin{aligned} & \stackrel{\rightharpoonup}{\circ} \\ & \stackrel{1}{N} \\ & \end{aligned}$ | $\begin{aligned} & \text { oे } \\ & \text { ले } \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \stackrel{0}{\circ} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { © } \\ & \underset{\sim}{\infty} \end{aligned}$ | $\begin{aligned} & \text { oे̀ } \\ & \text { Ni } \end{aligned}$ | $\begin{aligned} & \stackrel{0}{0} \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { ò } \\ & \stackrel{0}{N} \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{\mathrm{O}} \\ & \text { ले } \end{aligned}$ | $\stackrel{\circ}{\text { ले }}$ | $\begin{aligned} & \circ \stackrel{\circ}{\circ} \\ & \stackrel{\circ}{\circ} \end{aligned}$ | $\begin{aligned} & \text { ò } \\ & \text { Nin } \end{aligned}$ | $\begin{aligned} & \text { А̀ } \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{\circ}{0} \\ & \underset{N}{2} \end{aligned}$ |  | $\stackrel{\text { ⿵冂人}}{\stackrel{\circ}{0}}$ | $\begin{aligned} & \stackrel{(1)}{0} \\ & \stackrel{0}{0} \end{aligned}$ |  |  |  |  |
| $\begin{aligned} & \stackrel{n}{9} \\ & \stackrel{\rightharpoonup}{\underset{~}{2}} \end{aligned}$ |  | $\begin{aligned} & \stackrel{\Omega}{\text { an }} \\ & \stackrel{\rightharpoonup}{\text { In }} \end{aligned}$ | $\begin{aligned} & \text { N } \\ & \stackrel{0}{0} \\ & \stackrel{1}{\Sigma} \end{aligned}$ | $\begin{aligned} & \text { N } \\ & \stackrel{\infty}{\infty} \\ & \underset{\Sigma}{\Sigma} \end{aligned}$ |  | $\begin{aligned} & \hat{0} \\ & \stackrel{\rightharpoonup}{\Sigma} \end{aligned}$ | $\begin{aligned} & \stackrel{\Omega}{\text { an }} \\ & \stackrel{\rightharpoonup}{\mathrm{N}} \end{aligned}$ | $\begin{aligned} & \stackrel{\Omega}{3} \\ & \stackrel{\rightharpoonup}{7} \\ & \stackrel{\rightharpoonup}{2} \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{\circ}{\infty} \\ & \stackrel{1}{\Sigma} \\ & \sum \end{aligned}$ | $\begin{aligned} & \underset{\infty}{\infty} \\ & \stackrel{1}{\infty} \\ & \stackrel{1}{\Sigma} \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{\infty}{\sim} \\ & \stackrel{7}{\Sigma} \end{aligned}$ |  | $\begin{aligned} & \text { N } \\ & \stackrel{0}{0} \\ & \stackrel{1}{\Sigma} \end{aligned}$ | $\begin{aligned} & \tilde{\sim} \\ & \stackrel{\infty}{\top} \\ & \Sigma \end{aligned}$ | $\begin{aligned} & \otimes \\ & \otimes \\ & \stackrel{0}{\sim} \\ & \stackrel{1}{2} \end{aligned}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{\infty} \\ & \stackrel{\infty}{\infty} \\ & \stackrel{1}{\Sigma} \end{aligned}$ | $\begin{aligned} & \infty \\ & \infty \\ & \underset{\sum}{\infty} \end{aligned}$ | $\begin{aligned} & \infty \\ & \stackrel{\infty}{\infty} \\ & \stackrel{7}{\Sigma} \end{aligned}$ | $\begin{aligned} & \text { N } \\ & \stackrel{0}{\infty} \\ & \underset{\Sigma}{\Sigma} \end{aligned}$ | $\begin{aligned} & \underset{\sim}{\infty} \\ & \stackrel{\sim}{\Sigma} \\ & \stackrel{1}{\Sigma} \end{aligned}$ | $\begin{aligned} & \hat{0} \\ & \stackrel{\otimes}{1} \\ & \dot{\Sigma} \end{aligned}$ | $\begin{aligned} & \hat{0} \\ & \stackrel{\infty}{1} \\ & \dot{\Sigma} \end{aligned}$ | $\begin{aligned} & \hat{0} \\ & \stackrel{\infty}{\sim} \\ & \dot{\Sigma} \end{aligned}$ | $\begin{aligned} & \hat{0} \\ & \stackrel{\infty}{\infty} \\ & \dot{\Sigma} \end{aligned}$ | $\begin{aligned} & \hat{\infty} \\ & \stackrel{\infty}{\infty} \\ & \underset{\Sigma}{\Sigma} \end{aligned}$ |  | $\begin{aligned} & \hat{\infty} \\ & \stackrel{\rightharpoonup}{\infty} \\ & \underset{\sim}{\Sigma} \end{aligned}$ |
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| $\stackrel{\curvearrowleft}{\infty}$ | $\underset{\sim}{\text { ® }}$ | $\stackrel{\stackrel{\rightharpoonup}{\mathrm{m}}}{2}$ | $\stackrel{0}{\mathrm{~N}}$ | $\stackrel{8}{i}$ | ষ্ল゙ | $\stackrel{8}{\circ}$ | $\stackrel{\infty}{\infty}$ | $\stackrel{\text { ® }}{\text { ® }}$ | $\stackrel{\mathrm{O}}{\mathrm{~N}}$ | $\stackrel{\mathrm{O}}{\mathrm{~N}}$ | $\stackrel{8}{\circ}$ | O | $\stackrel{\mathrm{O}}{\mathrm{~N}}$ | $\stackrel{\circ}{\circ}$ | $\stackrel{0}{\mathrm{~N}}$ | $\stackrel{\mathrm{O}}{\mathrm{~N}}$ | $\stackrel{\circ}{\square}$ | $\stackrel{\circ}{0}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\stackrel{\circ}{i}$ | $\stackrel{\text { o }}{i}$ | $\begin{aligned} & \stackrel{N}{N} \end{aligned}$ | $\stackrel{\mathrm{N}}{\mathrm{~N}}$ | $\stackrel{N}{N}$ | $\stackrel{\text { N }}{\text { N }}$ | N | $\stackrel{\text { N }}{ }$ |
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| $\begin{aligned} & \text { N } \\ & \underset{\sim}{I} \end{aligned}$ | $\begin{aligned} & \text { N} \\ & \underset{7}{7} \end{aligned}$ | $\begin{aligned} & \text { N } \\ & \text { N̈ } \end{aligned}$ | $\stackrel{\infty}{\infty}$ | $\stackrel{\infty}{\infty}$ | $\begin{aligned} & \stackrel{\circ}{\infty} \\ & \stackrel{\infty}{\infty} \end{aligned}$ | $\begin{aligned} & \text { \& } \\ & \stackrel{-}{\circ} \\ & \hline-1 \end{aligned}$ | $\begin{aligned} & \stackrel{N}{N} \\ & \underset{\sim}{7} \end{aligned}$ | $\begin{aligned} & \stackrel{\text { N}}{N} \\ & \underset{\sim}{7} \end{aligned}$ | $\stackrel{\infty}{\infty}$ | $\stackrel{\infty}{\infty}$ | $\begin{aligned} & \text { O} \\ & \underset{\sim}{m} \end{aligned}$ | $\begin{aligned} & \text { O-1 } \\ & \underset{\sim}{m} \end{aligned}$ | $\stackrel{\infty}{\infty}$ | $\stackrel{\infty}{\infty}$ | $\stackrel{\infty}{\infty}$ | $\begin{aligned} & \underset{\sim}{\circ} \\ & \stackrel{y}{\circ} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \underset{\sim}{N} \end{aligned}$ | $\begin{aligned} & \text { O-1 } \\ & \underset{\sim}{n} \end{aligned}$ | $\stackrel{\infty}{\infty}$ | $\stackrel{\infty}{\infty}$ | $\begin{aligned} & \infty \\ & \stackrel{\infty}{\infty} \\ & \stackrel{1}{\infty} \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{n} \\ & \text { N } \end{aligned}$ | $\stackrel{\rho}{\sim}$ | $\stackrel{0}{c}$ | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \sim \end{aligned}$ |  | $\begin{aligned} & \text { ò } \\ & \hline . \end{aligned}$ |
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Nikolai I，Gangut，
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Grozyashchi，Rurik（i）
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Novik, Bespoloiny,
llin, Orfej, Gavri,,
Izyaslav, Gogland,
Kerch

| 35112 |  |
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| 30998 | Colorado |
| 34839 | South Dakota, Lexington |
| 35333 |  |
| 32004 | re-armed Colorado |
| 33695 | North Carolina, South |
| 38720 | Dakota |
| 19202 | New, Montana |
| 19202 | Pennsylvania Nevada, |
| 19246 |  |
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| 21973 | New Mexico, California |

UNITED STATES

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|  | $\begin{aligned} & \text { Ò } \\ & \underset{6}{\circ} \end{aligned}$ |  |  |  | $\begin{aligned} & \text { oें } \\ & \text { ì } \end{aligned}$ |  | $\begin{aligned} & \text { oे } \\ & \text { İ } \end{aligned}$ |  |  | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \stackrel{0}{i} \\ & \hline \end{aligned}$ |  | $$ |  | $\begin{aligned} & \stackrel{\text { ®}}{\mathrm{N}} \\ & \hline \end{aligned}$ |  |  | $\stackrel{\text { ¢0\％}}{\text { Ni }}$ |  |  |  |  |  |  |  | O－ |
| $\begin{aligned} & o \infty \\ & \dot{\omega} \dot{\sim} \\ & \dot{\Sigma} \frac{\pi}{0} \end{aligned}$ | $\sum_{\frac{0}{4}}^{\infty}$ | － | ${ }^{\circ}$ | \％ |  | cio |  |  |  | ETo |  |  |  | Ein ois |  |  |  |  |  |  |  |  |  | $\sum_{\substack{\text { n } \\ \stackrel{y}{c}}}^{n}$ | $\sum_{0}^{\infty}$ |
|  | $\stackrel{\ddagger}{\mathrm{N}}$ |  | $\begin{aligned} & \stackrel{\ominus}{\uparrow} \\ & \end{aligned}$ |  | $\stackrel{\ominus}{\underset{\sim}{\wedge}}$ |  | $\stackrel{\text { 4 }}{\stackrel{1}{c}}$ |  | ! ion | $\begin{aligned} & \text { OR } \\ & \stackrel{n}{n} \end{aligned}$ | $$ | ボ | $\underset{\substack{\text { ה }}}{ }$ | $\stackrel{\underset{\hat{N}}{ }}{ }$ | $\underset{\substack{-1}}{ }$ | Oo | $\begin{aligned} & \text { O} \\ & i \end{aligned}$ | $\begin{aligned} & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { n } \\ & \text { in } \end{aligned}$ | $\stackrel{\text { ® }}{\text { ¢ }}$ | $\stackrel{\stackrel{9}{i}}{\stackrel{1}{2}}$ | $\stackrel{\infty}{\infty}$ | $\stackrel{\infty}{\infty}$ | ষু | $\stackrel{+}{+}$ |
| $\stackrel{\circ}{\circ}$ | $\begin{aligned} & 8 \\ & \text { in } \end{aligned}$ | $\stackrel{8}{\circ}$ | $\underset{\sim}{8}$ | $\begin{aligned} & 8 \\ & \stackrel{\circ}{\prime} \end{aligned}$ | $\stackrel{\text { O}}{\mathrm{N}}$ | $\stackrel{8}{\circ}$ | $\stackrel{8}{\mathrm{O}}$ | $\begin{aligned} & 8 \\ & \stackrel{\circ}{\circ} \end{aligned}$ | $\stackrel{8}{\mathrm{~N}}$ | $\stackrel{8}{\mathrm{~N}}$ | $\stackrel{8}{\mathrm{i}}$ | $\begin{aligned} & \mathrm{O} \\ & \text { N } \end{aligned}$ | $\stackrel{8}{\mathrm{~N}}$ | $\stackrel{8}{\mathrm{~N}}$ | $\stackrel{8}{\circ}$ | $\stackrel{8}{\mathrm{~N}}$ | $\stackrel{8}{\mathrm{i}}$ | $\stackrel{8}{\circ}$ | $\stackrel{8}{\mathrm{i}}$ | $\stackrel{8}{\text { i }}$ | $\stackrel{\circ}{-}$ | $\stackrel{8}{8}$ | $\stackrel{8}{7}$ | $\stackrel{8}{\circ}$ | $\stackrel{8}{-}$ |
| $\stackrel{\circ}{\circ}$ | $\underset{\sim}{M}$ | $\stackrel{\stackrel{\rightharpoonup}{\circ}}{\stackrel{-}{2}}$ | $\begin{aligned} & \mathrm{O} \\ & \stackrel{\text { r }}{2} \end{aligned}$ | $\stackrel{8}{\mathrm{o}}$ | $\begin{aligned} & \mathrm{O} \\ & \stackrel{\text { V }}{2} \end{aligned}$ | $\stackrel{\circ}{\mathrm{O}}$ | $\stackrel{\mathrm{O}}{\mathrm{~F}}$ | $\begin{aligned} & \mathrm{O} \\ & \stackrel{\text { I }}{2} \end{aligned}$ | $\underset{\sim}{N}$ | $\underset{\sim}{\underset{\sim}{J}}$ | $\underset{\sim}{N}$ | $\underset{\sim}{\underset{\sim}{7}}$ | $\begin{aligned} & 0 \\ & \stackrel{0}{m} \end{aligned}$ | $\underset{\sim}{\mathrm{m}}$ |  | $\stackrel{\stackrel{0}{-}}{\stackrel{-}{2}}$ | $\begin{aligned} & \text { O. } \\ & \text { ले } \end{aligned}$ | ت্ল゙ | $\stackrel{0}{\stackrel{\circ}{m}}$ | $\stackrel{\text { M }}{\substack{2}}$ | ন্ল্ল゙ | $\stackrel{\text { N }}{\substack{(1)}}$ | $\stackrel{\text { ¢ }}{\text { c }}$ | $\stackrel{\circ}{\circ}$ | $\stackrel{0}{0}$ |
| 0 | $\begin{aligned} & 0 \\ & \frac{n}{4} \end{aligned}$ | 0 | $\begin{aligned} & \text { U } \\ & \text { O } \\ & \text { 足 } \end{aligned}$ | 0 | $\begin{aligned} & \text { U } \\ & \text { O } \\ & \text { n } \end{aligned}$ | $\bigcirc$ | U O O 号 | 0 | ¢ | U | $\stackrel{0}{4}$ | U | $\frac{8}{4}$ | U | $\begin{aligned} & \text { O } \\ & \text { 足 } \end{aligned}$ | $\stackrel{\square}{4}$ | U | $\begin{aligned} & \text { U } \\ & \text { 足 } \end{aligned}$ | $\stackrel{\square}{4}$ | U | $\begin{aligned} & \text { U } \\ & \text { 足 } \end{aligned}$ | $\begin{aligned} & 0 \\ & \frac{0}{4} \end{aligned}$ | $\begin{aligned} & 0 \\ & \frac{0}{4} \end{aligned}$ | $\begin{aligned} & 0 \\ & \frac{0}{4} \end{aligned}$ | 年 |
| $\begin{aligned} & 8 \\ & \stackrel{8}{n} \end{aligned}$ | $\begin{aligned} & \circ \\ & \hline \text { - } \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { oे } \end{aligned}$ | $\begin{aligned} & \text { O- } \\ & \text { o- } \end{aligned}$ | $\begin{aligned} & \text { O- } \\ & \text { o- } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \stackrel{8}{\circ} \\ & \stackrel{1}{7} \end{aligned}$ | $\begin{aligned} & \text { O- } \\ & \text { - } \end{aligned}$ | $\begin{aligned} & \circ \\ & \text { O- } \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { in } \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { Oi } \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \stackrel{\sim}{\mathrm{~N}} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \underset{\sim}{2} \end{aligned}$ | $\begin{aligned} & \text { O } \\ & \underset{寸}{\prime} \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{\text { I }}{ } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { in } \end{aligned}$ | $\stackrel{8}{8}$ | $\begin{aligned} & \mathrm{O} \\ & \text { in } \end{aligned}$ | $\stackrel{\circ}{\mathrm{i}}$ | $\stackrel{\circ}{\mathrm{i}}$ |  | $\begin{aligned} & \circ \\ & \stackrel{0}{0} \end{aligned}$ |
| $\underset{\substack{\infty}}{\mathbb{O}}$ | $\begin{aligned} & \mathbb{Z} \\ & \underset{\sim}{0} \\ & \text { Non } \end{aligned}$ | $\begin{aligned} & \mathbb{N} \\ & \underset{\sim}{\circ} \end{aligned}$ | $\begin{aligned} & \infty \\ & \stackrel{\sim}{\tilde{N}} \\ & \text { 欠 } \end{aligned}$ | $\underset{\infty}{\stackrel{\text { N}}{N}}$ | $\begin{gathered} \stackrel{\circ}{N} \\ \text { Nָ } \end{gathered}$ | $\begin{aligned} & \circ \\ & \underset{\sim}{N} \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{\tilde{N}} \\ & \underset{\sim}{N} \end{aligned}$ | $\begin{aligned} & \underset{\sim}{\mathscr{N}} \\ & \stackrel{y}{*} \end{aligned}$ | $\begin{aligned} & \infty \\ & \stackrel{0}{0} \\ & \text { O- } \end{aligned}$ | 8 8 8 8 | $\begin{aligned} & \text { İ } \\ & \text { ì } \end{aligned}$ | $\begin{aligned} & \text { J } \\ & \text { İ } \end{aligned}$ |  | o | ® <br> － <br> G | $\begin{aligned} & \text { oo } \\ & \text { O- } \\ & \hline \end{aligned}$ | $$ | $$ |  | $\begin{aligned} & \text { ơ } \\ & \text { Ni } \end{aligned}$ | N্ত্শ | $\begin{aligned} & \infty \\ & \stackrel{\sim}{\tilde{N}} \\ & \text { 欠, } \end{aligned}$ | $\begin{aligned} & \text { N} \\ & \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{\tilde{\infty}} \\ & \underset{\infty}{N} \end{aligned}$ | $\infty$ $\infty$ $\infty$ $\infty$ 0 |
| $\begin{aligned} & \text { No } \\ & \text { N్ర } \\ & \hline \end{aligned}$ |  | $\begin{aligned} & \hat{N} \\ & \stackrel{0}{0} \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { Oi } \end{aligned}$ | $$ | $\begin{aligned} & \text { g } \\ & \text { O} \\ & 0 \end{aligned}$ | $\begin{aligned} & \hat{N} \\ & \stackrel{్}{6} \end{aligned}$ | $\begin{aligned} & \text { of } \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & \text { N్ } \\ & \text { o్ర } \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \infty \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { O } \\ & \text { İ } \\ & \text { İ } \end{aligned}$ |  | $\begin{aligned} & \text { ® } \\ & \text { N̈ } \\ & \text { İ } \end{aligned}$ |  |  | $\begin{aligned} & \text { ơ } \\ & \stackrel{+}{\mathrm{O}} \end{aligned}$ |  | $\begin{aligned} & \text { ö } \\ & \stackrel{\rightharpoonup}{\circ} \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { ö } \\ & \stackrel{\sim}{\mathrm{O}} \end{aligned}$ |  | $\begin{aligned} & \text { M } \\ & \stackrel{+}{\overleftarrow{~}} \end{aligned}$ | $\begin{aligned} & \text { ơ } \\ & \stackrel{\text { I }}{0} \end{aligned}$ | $\begin{aligned} & \stackrel{0}{0} \\ & \stackrel{+}{\infty} \end{aligned}$ |  | $\begin{aligned} & \infty \\ & \stackrel{\circ}{\circ} \\ & \text { L్ల } \end{aligned}$ | $\begin{aligned} & \text { O. } \\ & \stackrel{0}{0} \\ & \text { Non } \end{aligned}$ |
| $\begin{aligned} & \text { \& } \\ & \text { O. } \\ & \text { N0 } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { in } \\ & \text { Nen } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \stackrel{0}{0} \\ & \text { Non } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { in } \\ & \text { Nen } \end{aligned}$ | $\begin{aligned} & 0.0 \\ & \stackrel{0}{0} \\ & \text { nen } \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{8}{0} \\ & \text { Nem } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { in } \\ & \text { N0 } \end{aligned}$ | $\begin{aligned} & \stackrel{8}{0} \\ & \stackrel{0}{0} \\ & \text { n } \end{aligned}$ | $\begin{aligned} & \stackrel{0}{0} \\ & \stackrel{H}{0} \end{aligned}$ | $\begin{aligned} & \text { N} \\ & \stackrel{\rightharpoonup}{\circ} \\ & \text { Nem } \end{aligned}$ | $\begin{aligned} & \text { No } \\ & \text { ò } \end{aligned}$ | $\begin{aligned} & \text { N} \\ & \text { ס్ల } \end{aligned}$ | $\begin{aligned} & \text { N్ } \\ & \text { 응 } \end{aligned}$ | $\begin{aligned} & \text { O } \\ & \text { } \\ & \text { Oi } \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{0}{0} \\ & \stackrel{\text { O}}{2} \end{aligned}$ |  | $\begin{aligned} & \text { ロ } \\ & \text { O } \\ & \text { İ } \end{aligned}$ | $\begin{aligned} & \circ \\ & \text { ® } \\ & \text { İ } \end{aligned}$ | $\begin{aligned} & \circ \\ & \text { ® } \\ & \text { İ } \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{\circ}{\infty} \\ & \stackrel{\text { O}}{0} \end{aligned}$ | $\begin{aligned} & \circ \\ & \text { ® } \\ & \text { ( } \end{aligned}$ | $\begin{aligned} & \text { ơ } \\ & \underset{\sim}{0} \end{aligned}$ | $\begin{aligned} & \circ \\ & \infty \\ & \text { © } \\ & \text { İ } \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{0}{1} \\ & \text { © } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \stackrel{0}{+} \\ & \text { O } \end{aligned}$ | $\begin{aligned} & \circ \\ & \text { ö } \\ & \text { O } \end{aligned}$ |
| ＝ | $=$ |  |  | $=$ | $=$ |  |  | － |  | $=$ | $\begin{aligned} & N \\ & \sum_{n}^{v} \\ & \stackrel{N}{N} \\ & \bar{\sim} \\ & \end{aligned}$ | $=$ |  | $=$ | $=$ |  | $=$ | $=$ | $\begin{aligned} & \text { m } \\ & \stackrel{\times}{2} \\ & \stackrel{O}{\#} \\ & \underset{\sim}{\prime} \end{aligned}$ | $=$ | $=$ |  | $=$ |  |  |


|  | $\begin{aligned} & \frac{\mathfrak{T}}{\underline{W}} \\ & \frac{\tilde{W}}{\mathbb{\alpha}} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
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| $\begin{aligned} & \infty \\ & \stackrel{\infty}{\sim} \\ & \underset{\sim}{2} \end{aligned}$ |  | $\begin{aligned} & \hat{m} \\ & \text { O} \\ & \text { O} \end{aligned}$ | $\begin{aligned} & \tilde{\sim} \\ & \underset{\sim}{7} \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{\circ}{9} \\ & \hline \end{aligned}$ | $\begin{aligned} & 0 \\ & \underset{\sim}{N} \\ & \underset{\sim}{n} \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & \hat{\circ} \\ & \text { Öन } \end{aligned}$ | $\begin{aligned} & N \\ & \underset{\sim}{J} \end{aligned}$ | $\begin{aligned} & \text { N } \\ & \underset{N}{\prime} \end{aligned}$ | $\underset{\infty}{\stackrel{\sim}{\infty}}$ | $\begin{aligned} & \text { m} \\ & \underset{7}{1} \end{aligned}$ | $\begin{aligned} & \text { J } \\ & \text { O } \end{aligned}$ | $\begin{aligned} & \text { I } \\ & \text { I } \end{aligned}$ | $\underset{\sim}{\sim}$ | $\begin{aligned} & \text { İ } \\ & \text { ন } \end{aligned}$ | $\begin{aligned} & \infty \\ & \stackrel{\infty}{6} \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \stackrel{-1}{\infty} \\ & \infty \\ & \end{aligned}$ | $\begin{aligned} & \text { 几o } \\ & \text { O } \end{aligned}$ | $\begin{aligned} & \text { H్م几 } \\ & \text { م } \end{aligned}$ | $\begin{aligned} & \stackrel{9}{7} \\ & \stackrel{0}{7} \end{aligned}$ | $\begin{aligned} & \text { d } \\ & \stackrel{y}{n} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \text { İ } \\ & \text { of } \end{aligned}$ | $\begin{aligned} & \underset{N}{N} \\ & \underset{\sim}{N} \end{aligned}$ | $\begin{aligned} & \overrightarrow{7} \\ & \underset{\sim}{7} \\ & \underset{\sim}{\infty} \\ & \underset{\sim}{\infty} \end{aligned}$ | $\begin{array}{ll} \tilde{\infty} & \tilde{\sim} \\ \sim \\ \sim \\ \sim \\ \sim \\ \sim \end{array}$ |
| － | $\bigcirc$ |  | － |  | － |  | － |  | － |  |  |  |  |  |  |  |  |  |  | － | $\bigcirc$ | － | $\bigcirc$ | － 0 | － 0 |
| $\begin{aligned} & \text { ò } \\ & \infty \\ & \text { in } \end{aligned}$ |  |  | $\begin{aligned} & \text { oे } \\ & \text { ì } \end{aligned}$ |  | $\begin{aligned} & \text { oి } \\ & \text { in } \end{aligned}$ |  | $\begin{aligned} & \text { oे } \\ & \stackrel{0}{i} \end{aligned}$ |  | $\begin{aligned} & \text { oి } \\ & \text { ì } \end{aligned}$ |  |  |  |  |  |  |  |  |  |  | $\stackrel{\text { O}}{\stackrel{\circ}{4}}$ | $\begin{aligned} & \text { ồ } \\ & \stackrel{1}{\mathrm{~N}} \end{aligned}$ | $\begin{aligned} & \text { oे̀ } \\ & \text { ò } \end{aligned}$ | $\begin{aligned} & \text { Ò } \\ & \text { ণi } \end{aligned}$ |  | $\begin{aligned} & \stackrel{\rightharpoonup}{\circ} \\ & \underset{\sim}{\circ} \\ & \underset{\sim}{\circ} \\ & \hline \end{aligned}$ |
| $\circ$ 0 0 0 0 | $\begin{aligned} & \text { Ò } \\ & \text { İ } \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |  |  |  | $\begin{aligned} & \circ \\ & \stackrel{\circ}{\infty} \\ & \text { Mn } \end{aligned}$ |  | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \stackrel{0}{\infty} \\ & \end{aligned}$ |  | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \stackrel{\circ}{\infty} \\ & \text { ले } \end{aligned}$ |  |  |  | $\begin{aligned} & \text { Ò } \\ & 0 \\ & \text { on } \end{aligned}$ |  | $\begin{aligned} & \circ \stackrel{\circ}{\circ} \\ & \stackrel{\circ}{\circ} \\ & \underset{A}{-1} \end{aligned}$ |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | $\begin{aligned} & \text { O} \\ & \stackrel{y}{\Sigma} \end{aligned}$ | $\begin{array}{ll} 0 & 0 \\ & 0 \\ \stackrel{\rightharpoonup}{\Sigma} & \underset{~}{\Sigma} \\ \stackrel{\Sigma}{\Sigma} \end{array}$ |  |
| $\stackrel{\infty}{\sim}$ | $\stackrel{\rightharpoonup}{\circ}$ | $\stackrel{\circ}{\circ}$ | $\stackrel{\llcorner }{\mathrm{m}}$ | $\stackrel{\leftrightarrow}{\mathrm{m}}$ | $\stackrel{\llcorner }{\text { ®ٌ }}$ | $\underset{\sim}{7}$ | $\underset{\sim}{7}$ | $\stackrel{\infty}{\infty}_{\infty}^{\infty}$ | $\stackrel{\infty}{\infty}_{\infty}^{\infty}$ | $\stackrel{N}{\substack{n}}$ | $\stackrel{10}{+}$ |  | $\xrightarrow[\substack{\text { On } \\ 0}]{ }$ | $\stackrel{\sim}{0}$ | $\stackrel{\leftrightarrow}{0}$ | $\underset{\infty}{\stackrel{\circ}{\infty}}$ | $\begin{aligned} & \text { O} \\ & \infty \\ & \infty \end{aligned}$ | $\stackrel{\infty}{\infty}$ | $\stackrel{\sim}{0}_{\infty}^{\infty}$ | $\underset{\sim}{\sim}$ | $\underset{\sim}{N}$ | $\stackrel{\sim}{N}$ | No | $\begin{array}{cc} N \\ \text { No } \\ \text { No } \end{array}$ | No |
| 음 | O. | $\stackrel{8}{N}$ | $\stackrel{\circ}{\wedge}$ | $\stackrel{\mathrm{O}}{\mathrm{~N}}$ | $\stackrel{\text { ® }}{\stackrel{1}{2}}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\stackrel{8}{\sim}$ | $\stackrel{\mathrm{O}}{\mathrm{~N}}$ | $\stackrel{\otimes}{\mathrm{N}}$ | ৪ | $\begin{aligned} & \circ \\ & \stackrel{\circ}{\circ} \end{aligned}$ | $\underset{\sim}{\mathrm{N}}$ | $\stackrel{8}{\circ}$ | $\begin{aligned} & \mathrm{O} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \stackrel{8}{\sigma} \\ & \hline \end{aligned}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\stackrel{\stackrel{\rightharpoonup}{\circ}}{\stackrel{1}{2}}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{寸} \\ & \hline \end{aligned}$ | $\stackrel{\circ}{\text { ® }}$ | $\stackrel{8}{\sim}$ | $\stackrel{\stackrel{\rightharpoonup}{\mathrm{o}}}{\mathrm{Z}}$ | $\stackrel{\circ}{\circ}$ | 옷 옷 |  |
| $\begin{aligned} & \text { Oin } \\ & \hline \end{aligned}$ | $\begin{aligned} & \circ \stackrel{0}{0} \\ & \stackrel{y}{2} \end{aligned}$ | $\stackrel{\circ}{\circ}$ |  | O |  | ৪ |  | $\underset{\text { ¢ }}{\stackrel{\circ}{4}}$ |  | $\stackrel{\text { NN }}{\text { N }}$ |  | $\stackrel{\stackrel{\rightharpoonup}{m}}{(1)}$ | N్లి | $\underset{\sim}{N}$ | O్ల | $\underset{\sim}{\mathbf{N}}$ | $\stackrel{\stackrel{\sim}{\mathrm{N}}}{\mathbf{N}}$ | $\stackrel{\circ}{\infty}$ | $\stackrel{0}{0}$ | $\begin{aligned} & \text { in } \\ & \stackrel{\sim}{0} \end{aligned}$ | $\stackrel{\circ}{\mathrm{O}}$ |  | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \stackrel{7}{2} \end{aligned}$ | $\stackrel{\circ}{\sim} \stackrel{\sim}{\sim}$ | $\stackrel{\circ}{\circ}$ |
| $\begin{aligned} & \text { U } \\ & \text { 足 } \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \\ & 0 \\ & \text { O } \\ & \text { 足 } \end{aligned}$ | ¢ | $\begin{aligned} & 0 \\ & \frac{0}{4} \end{aligned}$ | $\stackrel{\square}{8}$ | $\begin{aligned} & 0 \\ & \frac{0}{<} \end{aligned}$ | $\frac{\square}{4}$ | $\begin{aligned} & 0 \\ & \frac{0}{4} \end{aligned}$ | $\begin{aligned} & 0 \\ & \frac{0}{4} \end{aligned}$ | $\begin{aligned} & 0 \\ & \frac{0}{4} \end{aligned}$ | $\frac{\square}{4}$ | U | $\stackrel{\square}{4}$ | $\begin{aligned} & 0 \\ & \frac{0}{4} \end{aligned}$ | $\stackrel{\square}{8}$ | U | ¢ | U | 咎 | － | ¢ | U | 0 | $\begin{aligned} & \text { U } \\ & \text { O } \\ & \text { O } \\ & \text { 足 } \end{aligned}$ | $\begin{array}{ll} 0 & 0 \\ 0 & 0 \\ 0 & 0 \\ \alpha & 0 \end{array}$ | $\begin{array}{ll} 0 & 0 \\ \frac{0}{4} & 0 \\ 心 & \frac{0}{c} \end{array}$ |
| $\begin{aligned} & \mathrm{O} \\ & \text { SN } \end{aligned}$ |  | $\begin{aligned} & \mathrm{O} \\ & \text { Sin } \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{8}{1} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \stackrel{0}{0} \\ & \underset{\sim}{7} \end{aligned}$ | $\begin{aligned} & \stackrel{0}{0} \\ & \underset{\sim}{N} \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{8}{\mathrm{~N}} \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{8}{7} \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{\sim} \\ & \underset{\sim}{2} \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{\sim} \\ & \underset{\sim}{n} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \underset{\sim}{\circ} \end{aligned}$ | $\stackrel{\mathrm{O}}{\stackrel{\rightharpoonup}{\mathrm{~N}}}$ | $\begin{aligned} & \stackrel{\circ}{\mathrm{N}} \\ & \text {. } \end{aligned}$ | $\stackrel{\text { O}}{\stackrel{\sim}{7}}$ | $\begin{aligned} & \text { \& } \\ & \underset{\sim}{\prime} \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{寸} \\ & \underset{\sim}{2} \end{aligned}$ | $\begin{aligned} & \text { O- } \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \text { O- } \\ & \stackrel{\sim}{2} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \text { O- } \\ & \stackrel{\sim}{2} \end{aligned}$ | $\begin{aligned} & \circ \\ & \underset{子}{-} \end{aligned}$ | $\begin{array}{ll} \stackrel{\circ}{j} \\ \underset{子}{\mathrm{~F}} \end{array}$ | $\begin{array}{ll} \mathrm{O} \\ \stackrel{\mathrm{~F}}{\mathrm{~F}} \\ \hline \end{array}$ |
| $\begin{aligned} & \underset{\sim}{\tilde{\infty}} \\ & \underset{\infty}{\infty} \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { ì } \\ & \stackrel{1}{5} \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{0}{0} \\ & 0 \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 . \\ & 0 . \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{\rightharpoonup}{8} \\ & \stackrel{y}{6} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \stackrel{\oplus}{6} \end{aligned}$ |  | $\begin{aligned} & 8 \\ & \stackrel{\rightharpoonup}{\overleftarrow{~}} \end{aligned}$ | İ | $\begin{aligned} & \stackrel{\otimes}{\tilde{\infty}} \\ & \underset{\sim}{\tilde{N}} \end{aligned}$ | $\begin{aligned} & 0 \\ & 00 \\ & 00 \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 . \\ & 0 . \end{aligned}$ |  | $$ | $\begin{aligned} & \text { N } \\ & \text { H్రిㅇ } \\ & \text { n } \end{aligned}$ | $\begin{aligned} & \infty 0 \\ & \stackrel{0}{\circ} \\ & \text { ¢ } \end{aligned}$ | $\begin{aligned} & \text { J } \\ & \text { ì } \end{aligned}$ | $\begin{aligned} & \text { İ } \\ & \text { I } \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \text { ® } \\ & \underset{\sim}{N} \end{aligned}$ | $\begin{aligned} & \text { \& } \\ & \text { ※̈ } \\ & \text { í } \end{aligned}$ | $\begin{gathered} \text { No } \\ \underset{\sim}{\infty} \end{gathered}$ | $\begin{gathered} \text { No } \\ \underset{\sim}{\infty} \end{gathered}$ | $\begin{aligned} & \text { N } \\ & \underset{\infty}{\infty} \\ & \underset{\infty}{2} \end{aligned}$ | $\begin{aligned} & \mathbb{N} \\ & \underset{\sim}{\circ} \end{aligned}$ |  |  |
| $\begin{aligned} & \text { ® } \\ & \text { L్. } \\ & \text { - } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { İ } \end{aligned}$ | $\begin{aligned} & \infty \\ & \stackrel{\infty}{\infty} \\ & \stackrel{\sim}{N} \end{aligned}$ | $\begin{aligned} & \text { m } \\ & \underset{\sim}{-} \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{0} \\ & \stackrel{y}{*} \\ & \stackrel{N}{0} \end{aligned}$ | $\stackrel{m}{\sim}$ | $\begin{aligned} & \infty \\ & \stackrel{\infty}{\circ} \\ & \stackrel{N}{N} \end{aligned}$ | $\begin{aligned} & \text { m} \\ & \underset{\sim}{7} \end{aligned}$ | $\begin{aligned} & \infty \\ & \stackrel{\infty}{\circ} \\ & \underset{N}{N} \end{aligned}$ | $\begin{aligned} & \text { m} \\ & \underset{\sim}{7} \end{aligned}$ | $\begin{aligned} & \stackrel{g}{+} \\ & \underset{7}{7} \end{aligned}$ | $\begin{aligned} & \text { J } \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \text { ণ} \\ & \underset{7}{7} \end{aligned}$ | $\begin{aligned} & \text { G} \\ & \underset{7}{\prime} \end{aligned}$ | $\begin{aligned} & \text { g} \\ & \underset{7}{7} \end{aligned}$ | $\begin{aligned} & \text { J } \\ & \text { A } \end{aligned}$ | $\begin{aligned} & \text { 잋 } \\ & \underset{7}{2} \end{aligned}$ | $\begin{aligned} & \text { H } \\ & \underset{\sim}{7} \end{aligned}$ | $\begin{aligned} & \text { ơ } \\ & \text { ન̈ } \end{aligned}$ | $\begin{aligned} & \text { む } \\ & \underset{\sim}{\prime} \end{aligned}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{\mathrm{m}} \\ & \underset{7}{2} \end{aligned}$ | $\begin{aligned} & \text { d } \\ & \stackrel{y}{7} \end{aligned}$ | $\begin{aligned} & \text { む } \\ & \underset{\sim}{\prime} \end{aligned}$ | $\begin{aligned} & \text { J } \\ & \underset{\sim}{\prime} \end{aligned}$ | $\begin{array}{ll} \dot{y} \\ \underset{~}{~} \\ \vec{~} \end{array}$ |  |
| $\begin{aligned} & \circ \\ & \text { O } \\ & \text { İ } \end{aligned}$ | $\begin{aligned} & \text { o } \\ & \text { } \\ & \text { O} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { 先 } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { 热 } \end{aligned}$ | $\begin{aligned} & \text { 8 } \\ & \text { + } \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \stackrel{8}{+} \\ & \stackrel{\text { N }}{N} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { NN } \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{8}{4} \\ & \stackrel{1}{N} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { NN } \end{aligned}$ | $\begin{aligned} & \text { Q } \\ & \text { 寂 } \end{aligned}$ | $\begin{aligned} & \text { N} \\ & \underset{\sim}{N} \end{aligned}$ | $\begin{aligned} & \text { N} \\ & \text { N్N } \end{aligned}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{N} \\ & \stackrel{\sim}{N} \end{aligned}$ | $\begin{aligned} & \stackrel{\text { N}}{\mathrm{N}} \\ & \stackrel{0}{2} \end{aligned}$ | $\stackrel{\stackrel{N}{N}}{\underset{\sim}{N}}$ | $\begin{aligned} & \stackrel{\text { N}}{N} \\ & \stackrel{\sim}{N} \end{aligned}$ | $\stackrel{\stackrel{\rightharpoonup}{\mathrm{N}}}{\underset{\sim}{2}}$ | $\stackrel{\stackrel{\rightharpoonup}{N}}{\stackrel{N}{N}}$ | $\begin{aligned} & \text { N} \\ & \text { Ni } \end{aligned}$ | $\begin{aligned} & \text { N} \\ & \underset{\sim}{\sim} \end{aligned}$ | $\begin{aligned} & \stackrel{N}{N} \\ & \stackrel{\sim}{\sim} \end{aligned}$ | $\stackrel{\text { NiN }}{\stackrel{N}{N}}$ | $\begin{gathered} \stackrel{\rightharpoonup}{N} \\ \stackrel{N}{N} \end{gathered}$ | $\stackrel{\text { N}}{\text { N}}$ | $\begin{gathered} \stackrel{N}{\tilde{N}} \\ \underset{\sim}{N} \\ \underset{\sim}{N} \end{gathered}$ | $\begin{array}{cc} \stackrel{N}{N} \\ \underset{\sim}{\sim} & \stackrel{\sim}{\sim} \end{array}$ |


| 12＂／50 Mk． 7 |
| :---: |
| 12＂／50 Mk． 8 |
| 10＂／30 Mk． 1 |
| ＂ |
| 10＂／34 Mk．1／2 |
| ＂ |
| 10＂／35 Mk． 2 |
| ＂ |
| 10＂／40 Mk． 3 |
| ＂ |
| 8＂／30 Mks． 1 \＆ 2 |
| ＂ |
| 8＂／35 Mk． 3 |
| ＂ |
| 8＂／40 Mk．3／3 |
| ＂ |
| 8＂／35 Mk． 4 |
| ＂ |
| 8＂／40 Mk． 5 |
| ＂ |
| 8＂／45 Mk． 6 |
| ＂ |
| ＂ |
| 8＂／55 Mk． 9 |
| ＂ |
| ＂ |
| ＂ |
|  |


| 8"/55 Mk. 12 | 203,20 | 151,96 | 762,00 | 41,00 | APCBC | 4,50 | 9,00 | 8.23 | Mk 21 | 19,80\% | 1,50\% | D | 27478 | Baltimore |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| " | 203,20 | 117,94 | 853,44 | 41,00 | SAPC | 4,50 | 7,00 |  | Mk 17 S C | 7,70\% | 3,99\% | D | 28582 |  |
| 7"/45 Mk. 2 | 177,80 | 74,84 | 822,96 | 15,00 | Common |  | 2,00 | 5.11 |  |  |  | BT |  | Connecticut, Mississippi |
| " | 177,80 | 74,84 | 822,96 | 15,00 | APC | 3,17 | 2,00 | 5.11 | $\begin{gathered} \text { APC Mk I } \\ \text { \& VIII } \end{gathered}$ |  |  | BT | 11860 |  |
|  | 177,80 | 74,84 | 822,96 | 15,00 | APC | 3,22 | 2,00 | 5.11 | APC Mk II APC Mk |  |  | BT | 11773 |  |
|  | 177,80 | 74,84 | 822,96 | 15,00 | APC | 3,28 | 4,00 | 5.11 | IV \& IX |  |  | D |  |  |
|  | 177,80 | 74,84 | 822,96 | 15,00 | APC | 3,38 | 5,00 | 5.11 | APC Mk. VI | 8,80\% | 2,61\% | D |  |  |
|  | 177,80 | 74,84 | 822,96 | 15,00 | APCBC | 3,39 | 7,00 | 5.11 | APC Mk. 10 | 8,80\% | 2,61\% | D | 15087 |  |
|  | 177,80 | 74,84 | 822,96 | 15,00 | APCBC | 3,38 | 7,00 | 5.11 | APC Mk. XII |  | 2,42\% | D | 15087 |  |
| 6"/30 Mks. 1, 2 \& 3/0 | 152,40 | 45,36 | 609,60 | 12,00 | AP | 2,88 | 2,00 | 3.96 | Steel |  | 1,25\% | BP | 7087 | Atlanta, Chicago, Charleston, San Francisco, Yorktown, Indiana, Maine |
| " | 152,40 | 45,36 | 609,60 | 12,00 | AP | 3,27 | 2,00 | 3.96 | Steel |  | 4,87\% | BP | 7087 |  |
| " | 152,40 | 45,36 | 609,60 | 12,00 | CP | 3,44 | 2,00 | 3.96 | Cast Iron |  | 4,75\% | BP | 7087 |  |
| " | 152,40 | 45,36 | 609,60 | 12,00 | Common | 3,61 | 2,00 | 3.96 | Cast Steel Johnson |  | 9,81\% | BP | 7087 |  |
| " | 152,40 | 47,13 | 634,00 | 12,00 | APC |  | 2,00 |  | Cap | 4,81\% |  |  | 7441 |  |
| 6"/35 Mk. 3/1 | 152,40 | 45,36 | 634,00 | 12,00 | AP | 2,88 | 2,00 | 4.11 | Steel |  | 1,25\% | BP | 7370 | Texas, Minneapolis |
| " | 152,40 | 45,36 | 634,00 | 12,00 | AP | 3,27 | 2,00 | 4.11 | Steel |  | 4,87\% | BP | 7370 |  |
| " | 152,40 | 45,36 | 634,00 | 12,00 | CP | 3,44 | 2,00 | 4.11 | Cast Iron |  | 4,75\% | BP | 7370 |  |
| " | 152,40 | 45,36 | 634,00 | 12,00 | Common | 3,61 | 2,00 | 4.11 | Cast Steel Johnson |  | 9,81\% | BP | 7370 |  |
| " | 152,40 | 47,13 | 655,32 | 12,00 | APC |  | 2,00 |  | Cap | 4,81\% |  |  | 7696 |  |
| $6 \mathrm{~F} / 40 \mathrm{Mks} 3 /$.2 \& 4 | 152,40 | 45,36 | 655,32 | 12,00 | AP | 2,88 | 2,00 | 4.11 | Steel |  | 1,25\% | BP | 7621 | Columbia, Cincinnati |
| " | 152,40 | 45,36 | 655,32 | 12,00 | AP | 3,27 | 2,00 | 4.11 | Steel |  | 4,87\% | BP | 7621 |  |
| " | 152,40 | 45,36 | 655,32 | 12,00 | CP | 3,44 | 2,00 | 4.11 | Cast Iron |  | 4,75\% | BP | 7621 |  |
| " | 152,40 | 45,36 | 655,32 | 12,00 | Common | 3,61 | 2,00 | 4.11 | Cast Steel Johnson |  | 9,81\% | BP | 7621 |  |
| " | 152,40 | 47,13 | 731,52 | 12,00 | APC | 3,20 | 2,00 | 4.11 |  | 4,81\% |  |  | 8595 |  |
| " | 152,40 | 47,63 | 731,52 | 12,00 | APC |  | 4,00 | 4.11 |  |  |  |  | 10571 |  |
| 6"/48 Mk. 6 | 152,40 | 47,13 | 792,48 | 15,00 | APC | 3,20 | 2,00 | 4.57 | Johnson Cap | 4,81\% |  |  | 10389 | Maine |
| " | 152,40 | 47,63 | 822,96 | 15,00 | APC |  | 4,00 |  |  |  | 2,48\% | D | 13716 |  |


| 152,40 | 47,63 | 853,44 | 15,00 | APC |  | 5,00 |  |  |  |  |  | 14630 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 152,40 | 47,63 | 822,96 | 15,00 | CP |  | 4,00 |  |  |  | 6,00\% | D | 13716 |  |
| 152,40 | 47,63 | 853,44 | 15,00 | CP |  | 5,00 |  | Comm. Mk. Johnson |  | 6,74\% | D | 14630 |  |
| 152,40 | 47,13 | 731,52 | 15,00 | APC |  | 2,00 | 4.65 | Cap | 4,81\% |  |  | 11340 | Illinois |
| 152,40 | 47,63 | 731,52 | 15,00 | APC |  | 4,00 |  |  |  | 2,48\% | D | 11915 |  |
| 152,40 | 47,63 | 853,44 | 15,00 | APC |  | 5,00 | 5.03 |  |  | 2,29\% | D | 14630 | Pennsylvania, Tennessee, St. Louis, Virginia |
| 152,40 | 47,63 | 853,44 | 15,00 | CP |  | 4,00 |  |  |  | 6,00\% | D | 14299 |  |
| 152,40 | 47,63 | 853,44 | 15,00 | CP | 3,78 | 5,00 |  | Comm. Mk. |  | 3,81\% | D | 14630 |  |
| 152,40 | 47,63 | 914,40 | 30,00 | APCBC | 3,80 | 7,00 | 5.64 |  |  | 2,48\% | D | 23134 | Omaha turrets |
| 152,40 | 47,63 | 914,40 | 30,00 | SAPC | 4,50 | 5,25 | 5.64 | $\begin{gathered} \mathrm{Sp} \\ \text { ComMk } 27 \end{gathered}$ | 9,10\% | 2,10\% | D | 21580 |  |
| 152,40 | 47,63 | 914,40 | 20,00 | APCBC | 3,80 | 7,00 | 5.64 |  |  | 2,48\% | D | 19294 | Omaha casemates |
| 152,40 | 47,63 | 914,40 | 20,00 | SAPC | 4,50 | 5,25 | 5.64 | Mk. 27 | 9,10\% | 2,10\% | D | 18105 |  |
| 152,40 | 47,63 | 914,40 | 25,00 | APCBC | 3,80 | 7,00 | 7,47 |  |  | 2,48\% | D | 21306 | Lexington, South Dakota |
| 152,40 | 47,63 | 914,40 | 25,00 | CPC | 4,50 | 5,25 | 7,47 | Mk. 24 |  | 6,74\% | D | 19998 |  |
| 152,40 | 58,97 | 762,00 | 40,00 | APCBC | 4,50 | 9,00 | 8.23 | Mk 35 | 18,40\% | 1,54\% | D | 23317 | Cleveland |
| 152,40 | 47,63 | 853,44 | 40,00 | APCBC | 3,80 | 7,00 |  |  |  |  | D | 21543 |  |
| 152,40 | 47,63 | 847,35 | 40,00 | SAPC | 4,50 | 5,25 |  | Mk 28 | 8,00\% | 5,45\% | D | 21401 |  |
| 152,40 | 47,63 | 914,40 | 20,00 | APCBC | 3,80 | 7,00 | 8.23 |  |  |  |  | 18105 | Erie |
| 152,40 | 47,63 | 914,40 | 20,00 | SAPC | 4,50 | 5,25 |  | Mk 28 | 8,00\% | 5,45\% | D | 17817 |  |
| 127,00 | 22,68 | 609,60 | 15,00 | AP | 2,90 | 2,00 | 3.96 |  |  |  |  | 7155 | Chicago |
| 127,00 | 22,68 | 609,60 | 15,00 | Common | 3,10 | 2,00 |  |  |  |  |  | 7155 |  |
| 127,00 | 22,68 | 701,04 | 15,00 | CP | 3,40 | 4,00 |  | Mk. 15 ['05] |  | 3,46\% | BT | 9574 |  |
| 127,00 | 22,68 | 701,04 | 15,00 | AP |  | 4,00 |  |  |  |  |  | 9574 |  |
| 127,00 | 22,68 | 685,80 | 15,00 | AP | 2,90 | 2,00 | 4.57 |  |  |  |  | 7891 | Olympia, Brooklyn, Cincinnati, Montgomery |
| 127,00 | 22,68 | 685,80 | 15,00 | CP |  |  |  |  |  |  |  | 7891 |  |
| 127,00 | 22,68 | 701,04 | 15,00 | CP | 3,40 | 4,00 |  | Mk. 15 ['05] |  | 3,46\% | BT | 9574 |  |
| 127,00 | 22,68 | 701,04 | 15,00 | AP |  | 4,00 |  |  |  |  |  | 9574 |  |
| 127,00 | 22,68 | 701,04 | 15,00 | AP | 2,90 | 2,00 | 5.11 |  |  |  |  | 8038 | Kearsarge |
| 127,00 | 22,68 | 701,04 | 15,00 | CP |  |  |  |  |  |  |  | 8038 |  |


| " | 127,00 | 22,68 | 807,72 | 15,00 | CP | 3,40 | 4,00 | 5.11 | Mk. 15 ['05] |  | 3,46\% | BT | 9960 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| " | 127,00 | 22,68 | 807,72 | 15,00 | AP |  | 4,00 |  |  |  |  |  | 9960 |  |
| 5"/50 Mk. 5 | 127,00 | 22,68 | 914,40 | 15,00 | APC | 3,30 | 4,00 | 3.58 |  |  | 3,40\% | D | 12344 | Delaware |
| " | 127,00 | 22,68 | 914,40 | 15,00 | CP | 3,40 |  |  | Mk. 15 ['05] |  | 3,46\% | BT | 12212 |  |
| 5"/50 Mk. 6 | 127,00 | 22,68 | 914,40 | 15,00 | APC | 3,30 | 4,00 | 5.87 |  |  | 3,40\% | D | 12344 | Denver |
| " | 127,00 | 22,68 | 914,40 | 15,00 | CP | 3,40 |  |  | Mk. 15 ['05] |  | 3,46\% | BT | 12217 |  |
| 5"/51 Mk. 7 | 127,00 | 22,68 | 960,12 | 20,00 | APC | 3,30 | 4,00 | 3.66 |  |  | 3,40\% | D | 14493 | Florida, Wyoming, New York, Nevada, Pennsylvania, <br> New Mexico, |
| " | 127,00 | 22,68 | 960,12 | 20,00 | CP | 3,40 |  |  | Mk. 15 ['05] |  | 3,46\% | BT | 14479 | Tennessee, Colorado |
| 5"/25 Mk. 10 | 127,00 | 25,03 | 634,00 | 85,00 | SAPC | 4,15 | 5,25 | 6.93 | Mk 38 S C | 14,00\% | 3,70\% | D | 13282 |  |
| " | 127,00 | 22,68 | 666,00 | 85,00 | APC | 3,30 | 4,00 | 6.93 |  |  |  |  | 13103 |  |
| " | 127,00 | 24,49 | 641,61 | 85,00 | CPBC | 4,15 | 5,25 | 6.93 | Mk 32 | 8,00\% | 4,60\% | D | 13250 |  |
| 5"/38 Mk. 12 | 127,00 | 25,03 | 798,58 | 85,00 | SAPC | 4,15 | 5,25 | 4.42 | Mk 38 S C | 14,00\% | 3,70\% | D | 16797 |  |
| " | 127,00 | 24,49 | 798,58 | 85,00 | CPBC | 4,15 | 5,25 | 4,42 | Mk 32 | 8,00\% | 4,78\% | D | 16555 |  |
| " | 127,00 | 22,68 | 838,20 | 85,00 | APC | 3,30 | 4,00 | 4,42 |  |  | 3,40\% | D | 16075 |  |
| 4"/40 Mks. 1-6 | 101,60 | 14,97 | 609,60 | 20,00 | AP | 3,20 | 2,00 | 5.11 |  |  |  |  | 9180 | New York, lowa |
| " | 101,60 | 14,97 | 609,60 | 20,00 | CP | 4,00 | 2,00 | 5.11 |  |  |  |  | 9180 |  |
| " | 101,60 | 14,97 | 701,04 | 20,00 | CPC | 3,20 | 3,00 | 5.11 |  |  |  |  | 9528 |  |
| 4"/50 Mk. 7 | 101,60 | 14,97 | 762,00 | 20,00 | SAPC | 4,90 | 3,00 | 3.66 |  |  | 3,33\% | BP | 10108 |  |
| " | 101,60 | 14,97 | 853,44 | 20,00 | CP | 3,95 | 7,00 | 3.66 | Mk 6 ('15) | 0,00\% | 4,21\% | BT | 14329 |  |
| " | 101,60 | 14,97 | 853,44 | 20,00 | SAPC | 4,38 | 7,00 | 3.66 | Mk 16 S C | 8,60\% | 3,51\% | D | 14329 |  |
| 4"/50 Mk. 9 | 101,60 | 14,97 | 883,92 | 20,00 | SAPC | 4,38 | 5,25 | 3.66 | Mk 16 S C | 8,60\% | 3,51\% | D | 14813 |  |
| " | 101,60 | 14,97 | 883,92 | 20,00 | CP | 3,95 | 2,00 | 3.66 | Mk 6 ('15) | 0,00\% | 4,21\% | BT | 14813 |  |
| 3"/50 Mk. 2 | 76,20 | 5,94 | 640,08 | 15,00 | AP | 4,05 | 2,00 | 4.65 | $\begin{aligned} & \text { Mk } 29 \\ & \text { Mk } 3 \end{aligned}$ |  | 2,29\% | D | 6400 |  |
| " | 76,20 | 5,90 | 640,08 | 15,00 | CP | 3,35 | 2,00 | 4.65 | Common | 0,00\% | 2,15\% | BT | 6400 |  |
| " | 76,20 | 5,94 | 822,96 | 15,00 | AP | 4,05 | 5,00 |  | Mk 29 |  | 2,29\% | D | 9418 |  |
| " | 76,20 | 5,90 | 822,96 | 15,00 | CP | 4,04 | 5,00 |  | Common |  | 9,76\% | BT | 9418 |  |
| $3 \mathrm{l} / 50 \mathrm{Mks}$. 3 \& 6 | 76,20 | 5,94 | 822,96 | 15,00 | AP | 4,05 | 5,00 |  | Mk 29 |  | 2,29\% | D | 9418 |  |
| " | 76,20 | 5,90 | 822,96 | 15,00 | CP | 4,04 | 5,00 |  | Common |  | 9,76\% | BT | 9418 |  |
| 3"/50 Mk. 10 | 76,20 | 5,90 | 822,96 | 85,00 | AP | 4,05 | 5,00 |  | Mk 29 |  | 2,31\% | D | 13341 |  |


|  | 76,20 | 5,90 | 822,96 | 85,00 | CP | 4,04 | 5,00 |  | $\begin{aligned} & \text { Common } \\ & \text { Mk } 3 \end{aligned}$ |  | 9,76\% | BT | 13341 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3"/23.5 Mk. 14 | 76,20 | 5,90 | 502,92 | 75,00 | CP | 3,35 | 2,00 | 4.65 | Common | 0,00\% | 2,15\% | BT | 8046 |
| " | 76,20 | 5,90 | 502,92 | 75,00 | CP | 4,04 | 5,00 |  | Common |  | 9,76\% | BT | 9235 |
| CIVIL WAR |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $\begin{aligned} & 20 \text {-in Dahlgren SB } \\ & 200 \# \end{aligned}$ | 508,00 | 486,26 | 417,58 | 25,00 | Cored | 1,00 | 1,00 | 1,98 |  |  |  |  | 5632 |
| 15-in Columbiad 40\# | 381,00 | 199,58 | 485,55 | 10,00 | Solid | 1,00 | 1,00 | 2,53 |  |  |  |  | 4285 |
| 60\# | 381,00 | 199,58 | 508,10 | 10,00 | Solid | 1,00 | 1,00 | 2,53 |  |  |  |  | 4478 |
| 15-in Dahlgren SB (short) $50 \#$ | 381,00 | 199,58 | 370,64 | 10,00 | Solid | 1,00 | 1,00 | 1,98 | cast iron |  |  |  |  |
| 50\# | 381,00 | 181,44 | 388,93 | 10,00 | Cored | 1,00 | 1,00 | 1,98 |  |  |  |  |  |
| 15-in Dahlgren SB (long) $60 \#$ | 381,00 | 199,58 | 430,07 | 10,00 | Solid | 1,00 | 1,00 | 2,53 | cast iron |  |  |  |  |
| 60\# | 381,00 | 181,44 | 451,10 | 10,00 | Cored | 1,00 | 1,00 | 2,53 |  |  |  |  |  |
| 11-in Dahlgren SB |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 30\# | 279,40 | 75,30 | 430,38 | 10,00 | Solid | 1,00 | 1,00 | 1,98 | cast iron wrought |  |  |  |  |
| 30\# | 279,40 | 84,37 | 405,38 | 10,00 | Solid | 1,00 | 1,00 | 1,98 | iron |  |  |  |  |
| 10-in Dahlgren SB |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 40\# <br> 10-in Columbiad SB | 254,00 | 56,25 | 557,79 | 10,00 | Solid | 1,00 | 1,00 | 2,53 |  |  |  |  | 3404 |
| 18\# <br> 9 -in Dahlgren SB | 254,00 | 56,20 | 508,41 | 10,00 | Solid | 1,00 | 1,00 | 2,53 |  |  |  |  | 3191 |
| 28.5\# <br> 8 -in Columbiad SB | 228,60 | 40,96 | 526,09 | 10,00 | Solid | 1,00 | 1,00 | 2,53 |  |  |  |  | 3074 |
| 10\# | 203,20 | 29,48 | 440,74 | 10,00 | Solid | 1,00 | 1,00 | 2,53 |  |  |  |  | 2604 |
| 20\# | 203,20 | 29,48 | 525,48 | 10,00 | Solid | 1,00 | 1,00 | 2,53 |  |  |  |  | 2927 |
| 8 -in 65 cwt SB 20\# | 203,20 | 29,48 | 491,95 | 10,00 | Solid | 1,00 | 1,00 | 2,53 |  |  |  |  | 2805 |
| 8 -in 63cwt SB 20\# | 203,20 | 29,48 | 502,01 | 10,00 | Solid | 1,00 | 1,00 | 2,53 |  |  |  |  | 2842 |
| 8 -in 55 cwt SB 20\# | 203,20 | 29,48 | 489,81 | 10,00 | Solid | 1,00 | 1,00 | 2,53 |  |  |  |  | 2797 |
| 42-pdr SB 10.5\# | 177,80 | 19,37 | 540,41 | 10,00 | Solid | 1,00 | 1,00 | 2,53 |  |  |  |  | 2482 |
| 32-pdr 72cwt SB 8\# | 162,56 | 14,79 | 545,59 | 10,00 | Solid | 1,00 | 1,00 | 2,53 |  |  |  |  | 2657 |


| 2579 |  |
| :--- | :--- |
| 2341 |  |
| 2154 |  |
| 2056 |  |
| 2446 |  |
| 2179 |  |
| 2444 |  |
| 3166 |  |
| 2534 |  |
| 2030 |  |
| 3036 |  |
| 2792 |  |
|  | Tennessee，Trenton， |
| 5075 | Shenondoah，et．al |
| 4842 | Tennessee |
| 5473 | Shenondoah，Ticonde－ |
| roga，Kearsarge，et．al． |  |
|  |  |
| 4936 |  |
| 5292 |  |
| 4406 |  |
| 4850 |  |
| 4962 |  |
| 5092 |  |


|  |  |  |  |  |  |  |  |  |  |  |  | $\begin{aligned} & \overline{\text { 凶े }} \\ & \text { 挙 } \end{aligned}$ |  |  |  |  |  |  | $\begin{aligned} & \text { 을 } \\ & \frac{\pi}{4} \end{aligned}$ |  |  |  | $\begin{aligned} & \text { 르 } \\ & \text { 은 } \\ & \text { 을 } \\ & \text { 휸 } \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\stackrel{N}{N}$ | $\stackrel{\sim}{N} \stackrel{N}{N}$ | $\stackrel{\sim}{\sim} \stackrel{\sim}{N}$ | $\stackrel{\sim}{N}$ | $\stackrel{N}{N}$ | $\stackrel{\sim}{\sim}$ | $\stackrel{N}{N}$ | $\stackrel{N}{N}$ | $\stackrel{N}{N}$ | $\stackrel{N}{N}$ | $\stackrel{N}{N}$ | $\stackrel{\sim}{\sim}$ | $\stackrel{\sim}{N}$ | $\stackrel{\sim}{\sim}$ | $\stackrel{N}{N}$ | $\stackrel{N}{\sim}$ | $\stackrel{N}{\sim}$ | $\stackrel{N}{N}$ | $\stackrel{N}{N}$ | $\stackrel{N}{\sim}$ | $\stackrel{N}{N}$ | $\stackrel{N}{N}$ | $\stackrel{N}{\sim}$ | $\stackrel{\sim}{\sim}$ | $\stackrel{\sim}{\sim}$ |
| $\underset{\sim}{8}$ | $8$ | $8 \text { O }$ | $\underset{\sim}{\mathrm{i}}$ | $\stackrel{\mathrm{r}}{\mathrm{r}}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\stackrel{8}{\mathrm{~N}}$ | $\stackrel{\circ}{\circ}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\underset{\sim}{\mathrm{N}}$ | $\underset{\sim}{\mathrm{N}}$ | $\underset{\sim}{\mathrm{N}}$ | $\stackrel{\stackrel{\rightharpoonup}{N}}{ }$ | $\stackrel{\circ}{\mathrm{N}}$ | $\stackrel{\stackrel{\rightharpoonup}{\mathrm{N}}}{ }$ | $\stackrel{\circ}{\mathrm{N}}$ | $\stackrel{\text { ® }}{\text { N }}$ | $\underset{\sim}{\mathrm{N}}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\underset{\sim}{\mathrm{N}}$ | $\underset{\sim}{\mathrm{N}}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\stackrel{\text { O}}{\text { i }}$ | － |
| $\stackrel{\circ}{\mathrm{i}}$ | $\underset{\sim}{8} \underset{\sim}{8}$ | $\underset{i}{\circ} \underset{\sim}{\circ}$ | $\underset{\sim}{\mathrm{O}}$ | $\stackrel{8}{i}$ | $\xrightarrow{3}$ | $\stackrel{0}{N}$ | $\underset{\sim}{\underset{\sim}{j}}$ | $\stackrel{\circ}{\text { in }}$ | $\stackrel{M}{N}$ | N | $\stackrel{\leftrightarrow}{\sim}$ | $\stackrel{\cong}{i}$ | $\stackrel{\circ}{\circ}$ | $\underset{i}{\text { ה }}$ | $\underset{\sim}{\infty}$ | $\underset{\sim}{i}$ | $\stackrel{\infty}{\infty}$ | $\stackrel{\rightharpoonup}{i}$ | $\xrightarrow{-1}$ | $\xrightarrow{\sim}$ | $\stackrel{8}{-}$ | $\underset{\sim}{N}$ | $\stackrel{\circ}{N}$ | $\stackrel{\text { O }}{\sim}$ |
| 믕 | $\begin{aligned} & \text { 흥 흫 } \\ & i \end{aligned}$ | $\begin{array}{ll} \text { 흧 흫 } \\ \text { in } \end{array}$ | 믛 | $\frac{\bar{ㅡ}}{0}$ | $\frac{8}{4}$ | $\frac{\square}{4}$ | $\stackrel{\square}{8}$ | $\frac{\square}{4}$ | 足 | ¢ | 号 | $\frac{\square}{8}$ | $\frac{\overline{ }}{\overline{0}}$ | $\begin{aligned} & \text { 를 } \\ & \text { 후 } \end{aligned}$ | $\frac{\text { 믕 }}{i}$ | $\begin{aligned} & \text { 3 } \\ & \text { 음 } \\ & \text { 응 } \end{aligned}$ | $\frac{\text { 흐 }}{i}$ | $\begin{aligned} & \text { 를 } \\ & \text { 흠 } \end{aligned}$ | \％ | $\stackrel{\square}{\circ}$ | \％ | 흥 | $\frac{\ddot{0}}{\omega}$ | 흥 |
| $\begin{aligned} & \circ \\ & \hline- \\ & \hline- \end{aligned}$ | $\begin{array}{ll} 8 & 0 \\ 0 & 0 \\ -1 & \end{array}$ | $\begin{array}{ll} \hline 0 \\ 0 & 0 \\ 0 & 0 \end{array}$ | $\begin{aligned} & \circ \\ & \hline- \\ & \hline- \end{aligned}$ | $\begin{aligned} & \circ \\ & \hline-\mathrm{O} \\ & \hline \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 \\ & \hline- \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \circ \\ & \hline-\mathrm{A} \\ & \hline \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \hline-1 \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \stackrel{\sim}{0} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \stackrel{0}{\mathrm{~N}} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { Sin } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { Nin } \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{8}{\mathrm{~N}} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \stackrel{0}{0} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { in } \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{8}{7} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \stackrel{1}{\mathrm{I}} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \stackrel{1}{7} \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{\circ}{\mathrm{H}} \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{8}{7} \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { B } \\ & \stackrel{y}{n} \end{aligned}$ | $\begin{array}{ll} 8 \\ \stackrel{\circ}{-} \\ \text { Ni } \end{array}$ |
| $\begin{aligned} & 0 \\ & 0 \\ & 0 \\ & \end{aligned}$ | $\begin{array}{lc} \stackrel{\sim}{\mathrm{N}} \\ \stackrel{\rightharpoonup}{\mathrm{~F}} \\ \underset{\sim}{\infty} \end{array}$ |  | $\begin{aligned} & \text { O} \\ & \text { Nì } \end{aligned}$ | $\begin{aligned} & \stackrel{\sim}{n} \\ & \stackrel{\sim}{\sim} \end{aligned}$ | $\begin{aligned} & \text { N్ } \\ & \text { N్ల } \end{aligned}$ | $\begin{aligned} & \infty_{0}^{\prime} \\ & \underset{\sim}{\circ} \end{aligned}$ | N్N్ | $\begin{aligned} & \text { O- } \\ & \underset{\sim}{\circ} \end{aligned}$ |  | $\begin{aligned} & \circ \\ & \stackrel{-}{F} \end{aligned}$ | $\begin{aligned} & \text { ద } \\ & \infty \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \infty \\ & \underset{\sim}{\circ} \\ & \hline \end{aligned}$ | $\begin{aligned} & \hat{\sim} \\ & \underset{\sim}{\circ} \end{aligned}$ | $\begin{aligned} & \text { N } \\ & \underset{\sim}{\sim} \end{aligned}$ | $\begin{aligned} & \underset{\sim}{G} \\ & \stackrel{\sim}{m} \end{aligned}$ | $\begin{aligned} & \text { P} \\ & \text { oip } \end{aligned}$ | $\begin{aligned} & \stackrel{0}{0} \\ & \stackrel{0}{0} \end{aligned}$ | $\begin{aligned} & \infty \\ & \underset{7}{7} \\ & \end{aligned}$ |  | $\begin{aligned} & \text { N } \\ & \text { ָ̄ } \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{\circ}{寸} \end{aligned}$ | $\begin{aligned} & \mathbb{Z} \\ & \mathbb{N} \\ & \hline \end{aligned}$ | $\begin{gathered} \underset{\sim}{\circ} \\ \underset{\sim}{\circ} \end{gathered}$ |  |
| $\stackrel{\Im}{\underset{\sim}{\sim}}$ | $\begin{array}{ll} N & 0 \\ \underset{\sim}{7} & \underset{\sim}{4} \end{array}$ |  | $\underset{\infty}{\infty}$ | $\stackrel{\infty}{\text { in }}$ |  | $\begin{aligned} & \text { Ǹ } \\ & \text { ©్ల } \end{aligned}$ | $\begin{aligned} & \infty \\ & \stackrel{\infty}{N} \end{aligned}$ | $\begin{aligned} & \hat{o}_{2} \\ & \hat{o}^{2} \end{aligned}$ | $\stackrel{\dddot{c}}{5}$ | $\begin{aligned} & \text { ®o } \\ & \underset{\infty}{\circ} \end{aligned}$ | $\underset{\substack{\text { Nop } \\ \hline}}{ }$ | $\begin{aligned} & \text { U } \\ & \text { ì } \end{aligned}$ | $\begin{aligned} & \underset{\sim}{\underset{\sim}{0}} \end{aligned}$ | $\begin{aligned} & \dot{9} \\ & \underset{7}{7} \end{aligned}$ | $\begin{aligned} & \underset{\sim}{N} \\ & \underset{\sim}{\sim} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \underset{7}{7} \end{aligned}$ | $\begin{aligned} & \infty \\ & \underset{\sim}{N} \\ & \underset{\sim}{n} \end{aligned}$ | $\underset{\infty}{\mathrm{O}_{0}}$ | $\stackrel{8}{\stackrel{0}{0}}$ | $\begin{aligned} & \stackrel{\circ}{0} \\ & \stackrel{0}{0} \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{+} \\ & \stackrel{y}{\circ} \end{aligned}$ | $\begin{aligned} & J_{\infty}^{\prime} \\ & 0 \end{aligned}$ | $\begin{gathered} \text { N } \\ \underset{\sim}{\mathrm{N}} \end{gathered}$ | $\begin{array}{cc} \substack{0 \\ \sim \\ \sim \\ \hline} \\ \hline \end{array}$ |
| $\begin{aligned} & \text { O} \\ & 0 \\ & 0 \\ & \hline \end{aligned}$ |  |  | $\begin{aligned} & \underset{\sim}{\tilde{N}} \\ & \stackrel{\rightharpoonup}{\mathrm{~N}} \end{aligned}$ | $\begin{aligned} & \text { N } \\ & \underset{\sim}{7} \end{aligned}$ | $\begin{aligned} & \text { ® } \\ & \stackrel{N}{\mathrm{~N}} \end{aligned}$ | $$ | $\begin{aligned} & \text { H } \\ & \text { N్స } \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \\ & i \end{aligned}$ | $\begin{aligned} & \text { 毋 } \\ & \infty \\ & \infty \end{aligned}$ | $\begin{aligned} & \stackrel{N}{N} \\ & \stackrel{\sim}{\sim} \end{aligned}$ | $\begin{aligned} & 0 \\ & \stackrel{0}{O} \\ & \end{aligned}$ | $\begin{aligned} & \underset{\sim}{0} \\ & \underset{\sim}{\mathrm{~N}} \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{H}{\sim} \end{aligned}$ | $\begin{aligned} & \text { B } \\ & \stackrel{+}{\sim} \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{y}{\sim} \\ & \stackrel{1}{N} \end{aligned}$ | $\begin{aligned} & \stackrel{8}{+} \\ & \stackrel{\text { N }}{N} \end{aligned}$ | $\stackrel{\text { Ni}}{\stackrel{N}{N}}$ | $\begin{gathered} \stackrel{\rightharpoonup}{N} \\ \stackrel{\sim}{N} \end{gathered}$ | $\begin{aligned} & \stackrel{N}{N} \\ & \underset{\sim}{2} \end{aligned}$ | $\stackrel{\stackrel{N}{N}}{\stackrel{N}{N}}$ | $\begin{gathered} \stackrel{N}{N} \\ \stackrel{N}{N} \end{gathered}$ | $\begin{aligned} & \stackrel{N}{0} \\ & \stackrel{N}{N} \end{aligned}$ | $\begin{aligned} & 0 \\ & \stackrel{0}{\mathrm{O}} \\ & \end{aligned}$ | $\begin{array}{ll} \circ \\ 0 \\ 0 \\ 0 & 0 \\ \end{array}$ |
|  | 苦 <br> $\infty$ © <br> 烒 <br> 훔 흠 <br> ジ～～ | 等昔 <br> ゅ $\omega$ <br> 苞 <br> N <br> 훈 훔 <br> ジ ̇ㅜ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | $=$ |  |  |  |  |


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100-pdr MLR (/23.4)

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7-in Brooke
bands) 20\#
8-in Brooke MLR (2 bands)

8 -in Brooke SB ( 2
bands)
10-in Brooke SB (2

bands) 11 -in Brooke SB (2
bands)
8 -in $150-\mathrm{pdr}$
8-in 200-pdr
Blakely [conversion] 7-
in 110-pdr
9-in MLR 250-pdr
4.5-in MLR
Blakely 6-in
[conversion] MLR
Blakely [contract] 32-
pdr SB
Blakely [contract] 68-
pdr SB
Blakely [conversion]
32-pdr MLR
Blakely [conversion]
6.3-in MLR
7-in MLR 120-pdr
8-in MLR 200-pdr

Armstrong
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AUSTRALIAN AND NEW ZEALAND COLONIES
Victoria
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Coast Defense
（Australia）
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皆 233，68 $\stackrel{\infty}{\sim}$ $\stackrel{\infty}{\sim}$
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| $\begin{aligned} & \text { त्ते } \\ & \frac{\stackrel{\rightharpoonup}{0}}{\omega} \end{aligned}$ | $\begin{aligned} & \mathrm{N} \\ & \stackrel{N}{0} \end{aligned}$ | $\begin{aligned} & \text { 들 } \\ & \frac{y}{W} \\ & \frac{\sqrt{W}}{2} \end{aligned}$ | ․ㅡㄴ 亭 |  |  | 늘 咅 W |  | 든 $\stackrel{y}{4}$ | $\stackrel{\text { M }}{\text { 른 }}$ |
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| Elswick | " | 127,00 | 22,68 | 605,64 | 15,00 | CP |  | 2,00 | 3,05 |  |  |  |  | 7071 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 12-pdr 8cwt BLR | 76,20 | 5,10 | 377,65 | 15,00 | Common |  | 2,00 | 3,05 |  |  | 4,45\% | BP | 4105 | Victoria |
| Elswick | 9 -pdr 6cwt BLR | 76,20 | 3,88 | 321,56 | 15,00 | Common |  | 2,00 | 3,05 |  |  | 4,38\% | BP | 3291 | Albert |
|  | JAPANESE |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 45-cal Type $548-\mathrm{cm}$ gun | 480,00 | 1550,00 | 800,00 | 30,00 | APC | 3,58 | 4,00 | 9.3 | No. 5 |  |  |  | 33210 | Coast Defence |
|  |  | 480,00 | 1750,00 | 750,00 | 30,00 | APCBC | 4,29 | 6,00 | 9.3 | Type 91 | 18,50\% | 1,60\% | TN | 33875 |  |
|  | 45-cal Type $546-\mathrm{cm}$ gun | 460,00 | 1375,00 | 800,00 | 30,00 | APC | 3,61 | 4,00 | 9.3 | No. 5 |  |  |  | 32715 | \#13 |
|  | 45-cal Type 9446 -cm | 460,00 | 1460,00 | 770,00 | 43,00 | APCBC | 4,25 | 6,00 | 9.3 | Type 91 <br> Type 91 |  |  |  | 39550 |  |
|  | gun | 460,00 | 1460,00 | 780,00 | 45,00 | APCBC | 4,25 | 6,00 | 8.8 | No. 0 <br> Type 91 | 18,50\% | 2,32\% | TN | 40800 | Yamato |
|  | 45-al " ${ }^{\text {c }}$ | 460,00 | 1460,00 | 780,00 | 45,00 | APCBC | 4,47 | 6,00 | 8.8 | No. 1 |  | 2,32\% | TN | 42030 |  |
|  | 45-cal Type 341 -cm gun | 409,00 | 1000,00 | 780,00 | 30,00 | APCBC | 3,60 | 3,00 | 6.3 | No. 5 |  |  |  | 30200 | Nagato, Kaga, Amagi, Kii |
|  | " | 409,00 | 1000,00 | 780,00 | 30,00 | APCBC | 3,66 | 4,00 | 6.3 | Type 88 |  |  |  | 30200 |  |
|  | " | 409,00 | 1020,00 | 780,00 | 43,00 | APCBC | 4,25 | 6,00 | 6.3 | Type 91 | 15,50\% | 1,46\% | TN | 38300 |  |
|  | 45-cal Type $4136-\mathrm{cm}$ gun | 355,60 | 635,04 | 770,00 | 25,00 | APC | 3,30 | 3,00 | 6.5 | No. 1 w/ Type 1 |  |  |  | 21870 | Kongo, Fuso, Ise |
|  | gr |  |  |  |  |  |  |  |  | No. 1 w/ |  |  |  |  |  |
|  | " | 355,60 | 635,04 | 770,00 | 25,00 | CPC |  | 3,00 | 6.5 | Type 1 <br> No. 2 w/ |  |  |  | 21870 |  |
|  | " | 355,60 | 635,04 | 770,00 | 25,00 | APC |  | 4,00 | 6.3 | Type 3 No. 2 w/ |  |  |  | 23970 |  |
|  | " | 355,60 | 635,04 | 770,00 | 25,00 | CPC |  | 4,00 | 6.3 | Type 3 No. 2 w/ |  |  |  | 23970 |  |
|  | " | 355,60 | 635,04 | 770,00 | 33,00 | APC |  | 4,00 | 6.3 | Type 3 No. 2 w/ |  |  |  | 27340 |  |
|  | " | 355,60 | 635,04 | 770,00 | 33,00 | CPC |  | 4,00 | 6.3 | Type 3 No. 5 |  |  |  | 27340 |  |
|  | " | 355,60 | 635,04 | 770,00 | 33,00 | APC | 3,61 | 4,00 | 6.2 | w/Type 5 No. 6 w/ |  |  |  | 28600 |  |
|  | " | 355,60 | 635,04 | 770,00 | 33,00 | APC | 3,61 | 4,00 | 6.2 | Type 88 |  |  |  | 28600 |  |
|  | " | 355,60 | 673,50 | 770,00 | 43,00 | APCBC | 4,30 | 6,00 | 6.3 | Type 91 | 15,50\% | 1,65\% | TN | 35450 |  |
| Canet | $32 \mathrm{~cm} / 38$ (M.1887) | 320,00 | 450,00 | 700,00 | 30,00 | AP | 3,50 | 2,00 | 7.5 |  |  | 2,26\% | BP | 18000 | Matsushima |
|  | " | 320,00 | 350,00 | 610,00 | 30,00 | Com |  | 2,00 | 7.5 |  |  |  |  | 15500 |  |
| Krupp | 30.5 cm RKL $25 \mathrm{C} / 80$ | 305,00 | 329,00 | 500,00 | 13,00 | AP | 2,70 | 2,00 | 5.5 | Steel C/81 |  | 1,06\% | BP | 7288 | Chinyen |




Ibuki

Furutaka，Aoba，Nachi

＇A＇Type cruisers
Fuso，re－armed Ryujo，
Kaimon，
Katsuragi
Kongo
Ryujo，re－armed
Adzuma
Mogami，Yamato，
Oyodo




$\left.\begin{array}{lllllllll}\text { 악 } & \circ & \circ & \circ & \circ & \circ & \circ & \circ & \circ \\ \hline\end{array}\right)$ ๗్ळ $\stackrel{\circ}{\circ}$ $\stackrel{\infty}{\infty} \stackrel{\circ}{N}$



| $\begin{aligned} & \text { N } \\ & \stackrel{0}{2} \\ & \stackrel{\rightharpoonup}{3} \end{aligned}$ | $\begin{aligned} & N \\ & \stackrel{N}{N} \\ & \stackrel{N}{3} \end{aligned}$ | $\begin{aligned} & \text { m } \\ & 0 \\ & \stackrel{0}{\lambda} \\ & \stackrel{N}{3} \end{aligned}$ | $\begin{aligned} & \text { m } \\ & \stackrel{\otimes}{2} \\ & \stackrel{\rightharpoonup}{3} \end{aligned}$ | $\begin{aligned} & \text { m } \\ & 0 \\ & \\ & \vdots \\ & 3 \end{aligned}$ |  |  |  | ન |  |  |  |  |  |  | $\begin{aligned} & \stackrel{\rightharpoonup}{\circ} \\ & \stackrel{\rightharpoonup}{2} \\ & \stackrel{\rightharpoonup}{\imath} \end{aligned}$ |  |  |  | $\begin{aligned} & \text { 흐 } \\ & \text { ָٓ } \\ & \text { Ü } \end{aligned}$ | $\begin{aligned} & \bar{\Phi} \\ & \stackrel{\otimes}{\omega} \end{aligned}$ |  |  |  |  | $\begin{aligned} & \text { N } \\ & \dot{z} \end{aligned}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{\otimes} \\ & \stackrel{\rightharpoonup}{\wedge} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\stackrel{\infty}{\odot}$ | $\stackrel{\infty}{\circ}$ | $\stackrel{\infty}{\infty}$ | $\stackrel{\infty}{\circ}$ | $\stackrel{\infty}{\circ}$ | $\stackrel{\infty}{\circ}$ | － | $\stackrel{\sim}{\circ}$ | คั | ल | ल | $\widehat{\sim}$ | $\widehat{\sim}$ | $\stackrel{\circ}{\sim}$ | $\stackrel{\circ}{\sim}$ | กู่ | $\stackrel{\rightharpoonup}{\mathrm{m}}$ | $\stackrel{-1}{n}$ | $\stackrel{-}{\text { ¢ }}$ | $\cdots$ | $\stackrel{-}{\sim}$ | $\stackrel{\rightharpoonup}{\mathrm{m}}$ | $\stackrel{-}{\text { ¢ }}$ | $\stackrel{\rightharpoonup}{\text { m }}$ | กั | ベ | N |
| $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\stackrel{\circ}{\circ}$ | $\stackrel{\circ}{-}$ | $\stackrel{\stackrel{\rightharpoonup}{\circ}}{\stackrel{1}{2}}$ | $\stackrel{\circ}{\circ}$ | $\stackrel{\circ}{\circ}$ | $\begin{aligned} & \circ \\ & \stackrel{\circ}{\sigma} \end{aligned}$ | $\stackrel{\circ}{\circ}$ | $\stackrel{8}{N}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\stackrel{8}{\mathrm{~N}}$ | $\begin{aligned} & \text { O} \\ & \text { in } \end{aligned}$ | $\stackrel{\circ}{\mathrm{N}}$ | ৪ | $\begin{aligned} & 8 \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { N } \end{aligned}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\begin{aligned} & \mathrm{O} \\ & \text { i } \end{aligned}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\stackrel{\mathrm{O}}{\mathrm{~N}}$ | $\stackrel{\stackrel{\rightharpoonup}{\sigma}}{\stackrel{1}{2}}$ | $\stackrel{\circ}{\square}$ | $\underset{\sim}{\mathrm{N}} \underset{\mathrm{~N}}{\mathbf{N}}$ |
|  |  |  |  |  |  | $\stackrel{\rightharpoonup}{\infty}$ | $\stackrel{\rightharpoonup}{\infty}$ | $\stackrel{\circ}{\dot{\sim}}$ | $\underset{\sim}{\underset{\sim}{7}}$ | $\stackrel{\text { N}}{\underset{\sim}{n}}$ | $\underset{\sim}{7}$ | $\stackrel{\text { N }}{\stackrel{1}{\sim}}$ | $\stackrel{\infty}{\sim}$ | $\stackrel{\text { N}}{\mathrm{N}}$ | $\stackrel{\widehat{\sim}}{\underset{\sim}{2}}$ | $\stackrel{\circ}{\circ}$ | $\underset{\sim}{N}$ | $\stackrel{\rightharpoonup}{6}$ | $\underset{\sim}{\underset{\sim}{*}}$ | $\underset{\sim}{N}$ | $\stackrel{\infty}{\infty}$ | $\stackrel{\circ}{\circ}$ | $\underset{\sim}{\mathrm{N}}$ | $\stackrel{\circ}{\circ}$ |  | $\underset{\sim}{b} \underset{\sim}{N}$ |
| $\begin{aligned} & 0 \\ & \frac{0}{4} \end{aligned}$ | $\begin{aligned} & \text { u } \\ & \text { O } \end{aligned}$ | $\begin{aligned} & 0 \\ & \frac{0}{4} \end{aligned}$ | 00 ì | $\begin{aligned} & 0 \\ & \frac{0}{4} \end{aligned}$ | O | $\begin{aligned} & U \\ & 0 \\ & \text { U } \\ & \text { ¢ } \end{aligned}$ | $\begin{aligned} & 00 \\ & \text { 足 } \end{aligned}$ | $\begin{aligned} & \text { U } \\ & \text { D } \\ & \text { 花 } \end{aligned}$ | ¢ | $\begin{aligned} & \text { б} \\ & 0 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | $\stackrel{\square}{4}$ |  | ¢ |  | $\begin{aligned} & \text { U } \\ & \text { D } \\ & \text { ¢ } \\ & \text { 心 } \end{aligned}$ |  | ¢ |  | 0 | $\frac{\square}{4}$ | $\frac{\square}{4}$ |  | ¢ | U | $\begin{aligned} & 0 \\ & \frac{0}{4} \end{aligned}$ | $\begin{aligned} & \text { 들 } \\ & \text { हु응 } \end{aligned}$ |
| $\begin{aligned} & \stackrel{\circ}{0} \\ & \underset{\sim}{n} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{0} \\ & \stackrel{-}{0} \end{aligned}$ | $\begin{aligned} & \circ \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { O- } \end{aligned}$ | $\begin{aligned} & \circ \\ & \hline 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { O- } \\ & \text { O- } \end{aligned}$ | $\begin{aligned} & \text { O- } \\ & \text { ó } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \circ \\ & \hline \end{aligned}$ | $\begin{aligned} & 8 \\ & \underset{\sim}{\mathrm{H}} \end{aligned}$ | $\begin{aligned} & 8 \\ & \underset{-}{\prime} \end{aligned}$ | $\begin{aligned} & \circ \\ & \underset{-}{\prime} \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{\rightharpoonup}{\text { an }} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \stackrel{\sim}{n} \end{aligned}$ | $$ | $\begin{aligned} & 8 \\ & \stackrel{8}{\mathrm{~N}} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { !ి } \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{\circ}{0} \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{8}{7} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \stackrel{\rightharpoonup}{\mathrm{~N}} \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{0} \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{0} \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \stackrel{\text { N }}{1} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { ñ } \end{aligned}$ | $\begin{array}{ll} 8 \\ 8 \\ \stackrel{0}{7} \\ \hline 1 \end{array}$ |
| $\begin{aligned} & \circ \\ & 0 \\ & \text { © } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { o. } \\ & \text { 。 } \end{aligned}$ | $\begin{aligned} & \circ \\ & \hline 8 \\ & \text { o } \end{aligned}$ | - |  |  | $\begin{aligned} & 8 \\ & \stackrel{8}{\circ} \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \hline \text { D } \\ & \hline \infty \end{aligned}$ | 8 <br> - <br>  | $\begin{aligned} & \stackrel{8}{\mathrm{~N}} \\ & \stackrel{y}{2} \end{aligned}$ | $$ | 8 | $\begin{aligned} & \text { ৪ } \\ & \text { ì } \end{aligned}$ | $\begin{aligned} & \text { O. } \\ & \underset{\sim}{\sim} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \substack{0 \\ \hline} \end{aligned}$ | $\begin{aligned} & \text { B. } \\ & \text { ू} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \text { } \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \text { İ } \\ & \text { İ } \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{0}{0} \\ & 0 \end{aligned}$ | $\begin{aligned} & \bullet \\ & \stackrel{0}{0} \\ & \stackrel{0}{6} \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{0}{0} \\ & \stackrel{0}{0} \end{aligned}$ | 8 $\stackrel{8}{0}$ 0 | $\begin{aligned} & 8 \\ & \text { Oi } \\ & \text { O} \end{aligned}$ | $\begin{aligned} & \text { B } \\ & \text { ̈ㅜㄴ } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & 0 . \\ & 0 \end{aligned}$ | 8 | $\begin{array}{ll} 8 & 8 \\ 0 & 0 \\ 0 & 0 \\ \infty & 0 \end{array}$ |
| $\begin{aligned} & \text { O} \\ & \underset{\sim}{7} \end{aligned}$ | $\begin{aligned} & \text { oj } \\ & \underset{7}{7} \end{aligned}$ | $\begin{aligned} & 0 \\ & \underset{\sim}{0} \\ & \text { N్ర } \end{aligned}$ |  |  | $\begin{aligned} & 0 \\ & \text { N్ర } \\ & \text { In } \end{aligned}$ | $\begin{aligned} & \circ \\ & 0 . \\ & \text { O } \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 . \\ & \text { I- } \end{aligned}$ | $\begin{aligned} & \text { م } \\ & \text { N్స } \\ & \text { N్ } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { in } \\ & \text { 仿 } \end{aligned}$ | $\begin{gathered} 8 \\ \text { in } \end{gathered}$ | $\begin{aligned} & \text { B } \\ & \stackrel{\circ}{\circ} \end{aligned}$ | $\begin{gathered} 8 \\ \text { in } \end{gathered}$ | No | $\begin{aligned} & \infty \\ & \stackrel{\circ}{\mathrm{m}} \end{aligned}$ | $\begin{aligned} & \hat{\infty} \\ & \hat{0} \\ & \text { Non } \end{aligned}$ | $\begin{aligned} & \infty \\ & \text { en } \\ & \text { 年 } \end{aligned}$ |  | $\begin{aligned} & \text { O} \\ & \underset{\sim}{2} \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { e } \\ & \text { § } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \underset{\sim}{2} \\ & \end{aligned}$ |  |  |  | $\begin{aligned} & \text { è } \\ & \text { fí } \end{aligned}$ | $\begin{aligned} & \infty \\ & \text { ๗゙ } \\ & \text { fin } \end{aligned}$ | $\begin{array}{lll} \circ & 0 \\ 0 & 0 \\ \text { By } & \text { Kin } \end{array}$ |
| $\begin{aligned} & \stackrel{\rightharpoonup}{\tilde{N}} \\ & \stackrel{\sim}{1} \end{aligned}$ | 씄 | NiN NiN | $\stackrel{\stackrel{N}{N}}{\text { N }}$ | $\stackrel{\text { N}}{\stackrel{N}{N}}$ | $\stackrel{\text { N}}{\text { N }}$ | $\circ$ <br> - <br> － <br> － | $\begin{aligned} & 8 \\ & 0 . \\ & \hline 0 \end{aligned}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{N} \\ & \stackrel{\sim}{N} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{0}{N} \\ & \underset{\sim}{1} \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{N} \\ & \underset{\sim}{1} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { O} \\ & \text { O- } \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{0} \\ & \underset{\sim}{1} \end{aligned}$ | $\begin{aligned} & \text { B } \\ & \stackrel{i}{n} \end{aligned}$ | $\begin{aligned} & \stackrel{\text { O}}{N} \\ & \underset{\sim}{\sim} \end{aligned}$ | $$ | $$ | $$ | $\begin{aligned} & \text { O} \\ & \text { Nin } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { N్స } \end{aligned}$ | $$ | $\begin{aligned} & \mathrm{O} \\ & \mathbb{N} \end{aligned}$ | $\begin{aligned} & \stackrel{y}{N} \\ & \underset{\sim}{\sim} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { ÑN } \end{aligned}$ |  |


|  |  |  |  |  |  |  |  |  |  |  |  | 읃 |  |  |  |  |  | $\stackrel{\overline{5}}{n}$ $\stackrel{3}{3}$ $\stackrel{3}{3}$ $\stackrel{\rightharpoonup}{b}$ |  |  |  | $\begin{aligned} & \stackrel{\pi}{\approx} \\ & \stackrel{\pi}{\widetilde{N}} \\ & \stackrel{\pi}{\tau} \end{aligned}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{array}{ll} \stackrel{\circ}{\lambda} & \text { g } \\ \sigma & \text { I } \end{array}$ | $\begin{aligned} & \text { og } \\ & -7 \end{aligned}$ | $$ | $\begin{aligned} & \text { 원 } \\ & \text { 기 } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { I } \end{aligned}$ | $\begin{aligned} & \circ \\ & \hline 0 \\ & \text { J } \end{aligned}$ | $\infty$ $\infty$ $\infty$ $\sim$ $\sim$ | $\begin{aligned} & N \\ & \underset{N}{N} \end{aligned}$ | － | ¢ | $\begin{aligned} & \mathrm{O} \\ & \stackrel{\circ}{\circ} \end{aligned}$ | $\begin{aligned} & \underset{7}{7} \\ & \text { م } \end{aligned}$ | － | ¢ | $\begin{aligned} & \circ \\ & 0 \\ & 0 \\ & \text { Non } \end{aligned}$ | ） | $\begin{aligned} & \circ \\ & \stackrel{\circ}{\mathrm{O}} \\ & \text { à } \end{aligned}$ | $\stackrel{\circ}{\circ}$ | N | $\stackrel{\text { N }}{\sim}$ | $\stackrel{\ominus}{\square}$ | $\stackrel{0}{\mathrm{~m}} \stackrel{1}{\sim}$ | $\stackrel{\text { 읏 }}{\text { N}}$ | $\stackrel{\otimes}{\circ} \stackrel{\circ}{\sim} \stackrel{\sim}{\sim}$ |
| 戸 | ら エ | む |  | ¢ | ড |  |  | あ | 0 | 0 | ¢ | 0 | ¢ | 0 | 而 | 历 | む | 0 | 0） | 0 | ¢ | 0） | － | ¢ 0 |
| $\begin{aligned} & \text { 人̀ } \\ & \infty \\ & \infty \\ & \infty \end{aligned}$ | $\begin{array}{ll} \stackrel{\circ}{\circ} & \stackrel{\rightharpoonup}{\circ} \\ 0 \\ \underset{\sim}{\circ} & \infty \\ \hline \end{array}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{0} \\ & \stackrel{0}{\sigma} \\ & \hline \end{aligned}$ |  |  | $\begin{aligned} & \stackrel{\circ}{0} \\ & \stackrel{e}{\sigma} \end{aligned}$ |  |  | $\begin{aligned} & \text { O} \\ & \text { © } \\ & \text { م) } \end{aligned}$ | 僉 | $\begin{gathered} \circ \\ \stackrel{\rightharpoonup}{\mathrm{N}} \\ \stackrel{y}{*} \end{gathered}$ | $\stackrel{\stackrel{\rightharpoonup}{7}}{\stackrel{\rightharpoonup}{7}}$ | 추N | $\begin{aligned} & \text { ⿳亠二口斤口⿱二小刂 } \end{aligned}$ | Nิํ | $\circ$ $\stackrel{\circ}{\mathrm{N}}$ in | $\begin{aligned} & \text { O} \\ & \text { ì } \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{\circ} \\ & \stackrel{\infty}{0} \\ & \hline \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \stackrel{y}{\circ} \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \text { oి } \\ & \text { O- } \end{aligned}$ | $\begin{aligned} & \text { ஃे̀ } \\ & \text { ले } \end{aligned}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{\circ} \\ & \text { Mo } \\ & \text { No } \end{aligned}$ | $\begin{aligned} & \text { Ò } \\ & \text { O- } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { O } \\ & 0 \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \text { ò } \\ & \text { Ni } \\ & \text { Ji } \end{aligned}$ |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | － | io |  |  |  |  |  |  |  |  |
|  | $\xrightarrow{+}$ | $\begin{gathered} \underset{\sim}{c} \\ \stackrel{\rightharpoonup}{z} \end{gathered}$ |  | $\begin{aligned} & \overrightarrow{-} \\ & \dot{c} \end{aligned}$ | $\begin{aligned} & \text { r } \\ & \dot{8} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  | $\begin{aligned} & -1 \\ & \sum_{3}^{0} \\ & \sum_{3}^{\infty} \end{aligned}$ | $\begin{gathered} \stackrel{\sim}{\otimes} \\ \stackrel{\rightharpoonup}{2} \end{gathered}$ |  |  |  |  |  |  |  |
| $\stackrel{\rightharpoonup}{\text { ¢ }}$ | ¢゙ | กั | ベ | ก | ก | $\stackrel{3}{5}$ | $\stackrel{-1}{5}$ | $\stackrel{\text { ¢ }}{ }$ | $\stackrel{\sim}{\square}$ | $\stackrel{\sim}{\square}$ | $\hat{\sim}$ | $\hat{\sim}$ | $\underset{\sim}{\underset{\sim}{N}}$ | $\underset{\sim}{N}$ | $\stackrel{\bigcirc}{\bigcirc}$ | $\stackrel{\bigcirc}{\bigcirc}$ | $\stackrel{\bigcirc}{\bigcirc}$ | ＋ | $\stackrel{\sim}{\sim}$ | $\stackrel{\sim}{\sim}$ | $\stackrel{\sim}{\sim}$ | $\stackrel{\sim}{0}$ | $\stackrel{\sim}{n}$ | $\bigcirc$ |
| $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\begin{array}{ll} \mathrm{O} & \mathrm{O} \\ \text { N } \end{array}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\begin{array}{ll} \stackrel{\circ}{\square} & 8 \\ \underset{\sim}{2} \end{array}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\stackrel{\circ}{-}$ | $\stackrel{\circ}{\circ}$ | $\begin{aligned} & \mathrm{O} \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\underset{\sim}{\mathrm{N}}$ | $\stackrel{8}{i}$ | $\underset{\sim}{\mathrm{N}}$ | $\stackrel{\mathrm{O}}{\mathrm{~N}}$ | $\stackrel{\stackrel{\rightharpoonup}{\mathrm{F}}}{\mathrm{\sigma}}$ | $\stackrel{\circ}{\mathrm{O}}$ | $\stackrel{8}{\circ}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\stackrel{\stackrel{\rightharpoonup}{\mathrm{N}}}{\mathrm{i}}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\stackrel{8}{\mathrm{~N}}$ | － | $\underset{\sim}{\mathrm{N}} \underset{\mathrm{~N}}{\mathbf{N}} \underset{\sim}{\mathrm{~N}}$ |
| $\stackrel{\circ}{\circ}$ | $\begin{array}{ll} \stackrel{\rightharpoonup}{N} \\ \text { ले } \end{array}$ | $\underset{\sim}{N}$ |  | $\begin{aligned} & \overrightarrow{0} \\ & \text { min } \end{aligned}$ | $\underset{\sim}{N}$ |  | $\underset{\sim}{\stackrel{N}{N}}$ |  | ${\underset{\sim}{n}}_{\infty}^{n}$ | $\stackrel{\circ}{\circ}$ | $\underset{N}{N}$ | $\begin{aligned} & \circ \\ & \stackrel{\circ}{\sim} \end{aligned}$ | $\underset{N}{N}$ | $\begin{aligned} & \circ \\ & \stackrel{\circ}{\top} \end{aligned}$ | $\stackrel{\infty}{\infty}$ | $\underset{\sim}{\aleph}$ | $\stackrel{\circ}{-}$ | $\stackrel{\sim}{\sim}$ | $\stackrel{\infty}{\stackrel{\circ}{\sim}}$ | $\stackrel{\bullet}{\circ}$ | $\stackrel{\infty}{\infty}$ | $\begin{aligned} & \text { O응 } \\ & \text { N } \end{aligned}$ | $\stackrel{\stackrel{1}{+}}{+}$ | NัN |
|  |  | 呆 | $\begin{array}{lll} 0 & 0 \\ \text { Q } & 0 \\ \hline \end{array}$ |  | $\frac{\square}{4}$ | $\begin{aligned} & \text { O } \\ & \text { 足 } \end{aligned}$ | $\begin{aligned} & \text { u } \\ & \text { O } \end{aligned}$ | U0 | $\stackrel{\square}{4}$ |  | $\stackrel{\square}{4}$ |  | $\stackrel{\square}{8}$ |  | $\begin{aligned} & 0 \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & \text { U } \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | U |  | $\stackrel{\square}{4}$ |  |  | $\stackrel{\square}{4}$ | ¢ | ¢ |
| $\begin{aligned} & \circ \\ & \stackrel{\circ}{0} \end{aligned}$ |  | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \underset{\sim}{\circ} \end{aligned}$ | $\begin{array}{ll} 8 & 8 \\ \underset{\sim}{\infty} & 0 \\ 0 \end{array}$ | $\begin{aligned} & \mathrm{O} \\ & \stackrel{0}{\circ} \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \infty \\ & 0 \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{\infty} \\ & \text { - } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { ö } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { Si } \end{aligned}$ | ৪ì | $\begin{aligned} & \text { O} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{0} \\ & \text { In } \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{0} \\ & \text { N} \end{aligned}$ | $\stackrel{\underset{\sim}{7}}{\stackrel{\rightharpoonup}{2}}$ | $\begin{aligned} & \text { O} \\ & \underset{\sim}{9} \end{aligned}$ | － | $\begin{aligned} & \text { O} \\ & \text { O- } \end{aligned}$ | $\begin{aligned} & \text { O- } \\ & \text { - } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \underset{\sim}{\mathrm{I}} \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{8}{0} \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { in } \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{8}{n} \end{aligned}$ | $\begin{aligned} & \text { O-} \\ & \text { ஸి } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { in } \end{aligned}$ | $\begin{array}{ll} 8 \\ \stackrel{8}{0} \\ \text { nin } \end{array}$ |
| $\begin{aligned} & \text { O} \\ & \text { Ni } \\ & \text { in } \end{aligned}$ |  | $\begin{aligned} & 8 \\ & \text { Bion } \\ & \hline \infty \end{aligned}$ | $\begin{array}{ll} 8 & 8 \\ \text { in } \\ \text { in } & 0 \\ \hline 0 \end{array}$ | $\begin{aligned} & \text { O} \\ & \text { O } \\ & 0 \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { in } \\ & 0 \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { in } \\ & \hline \infty \end{aligned}$ | $\begin{aligned} & 8 \\ & \hline 0 . \\ & 0.0 \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { in } \\ & 0 \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { O} \\ & \text { గin } \end{aligned}$ |  |  | $\begin{aligned} & \stackrel{\circ}{\top} \\ & \text { N } \\ & \text { O} \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 . \\ & 0 \\ & 8 \end{aligned}$ | $\begin{aligned} & \text { \& } \\ & \stackrel{0}{\circ} \\ & \stackrel{\circ}{\circ} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { Oi } \\ & \hline 0 \end{aligned}$ | $$ | $\begin{aligned} & 8 \\ & \hline 0 . \\ & 0.0 \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{0}{\circ} \\ & \text { O } \end{aligned}$ | $\begin{aligned} & \stackrel{8}{-} \\ & \stackrel{\text { N}}{-} \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{8}{2} \\ & \stackrel{5}{2} \end{aligned}$ | $\begin{aligned} & 8 \\ & \hline 8 \\ & \hline 8 \end{aligned}$ | $\begin{aligned} & \mathrm{B} \\ & \text { O- } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { O- } \\ & \text { in } \end{aligned}$ | $\begin{array}{ll} 88 \\ \hline 8 \\ \stackrel{H}{0} & \stackrel{H}{0} \end{array}$ |
|  |  |  |  | $\begin{aligned} & \text { O} \\ & \text { O } \\ & \text { \& } \end{aligned}$ |  | $\begin{aligned} & \text { O} \\ & \underset{\sim}{0} \\ & \stackrel{y}{2} \end{aligned}$ | $\begin{aligned} & \stackrel{0}{0} \\ & \text { \& } \end{aligned}$ | $\begin{aligned} & \text { e } \\ & \text { O } \\ & \text { \& } \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { İ } \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \text { Oin } \\ & \text { Non } \end{aligned}$ | $\stackrel{\circ}{\mathrm{N}}$ | $\begin{aligned} & \text { On } \\ & \text { Nin } \end{aligned}$ | $\stackrel{\circ}{\text { N }}$ | $\begin{aligned} & \text { O. } \\ & \text { öల } \end{aligned}$ | $\stackrel{\otimes}{\infty}$ | $\begin{aligned} & \stackrel{\circ}{\circ} \\ & \text { on } \end{aligned}$ | $\begin{aligned} & \underset{\sim}{\underset{\sim}{*}} \end{aligned}$ | $\stackrel{8}{\mathrm{~N}}$ | $$ | $\begin{aligned} & \text { M } \\ & \underset{\sim}{0} \end{aligned}$ | $\begin{aligned} & \stackrel{8}{\circ} \\ & \stackrel{\circ}{\circ} \end{aligned}$ | $\begin{aligned} & \stackrel{8}{\circ} \\ & \stackrel{0}{\circ} \end{aligned}$ |  |
| $$ |  | $$ |  | $\begin{aligned} & \dot{j} \\ & \tilde{N} \end{aligned}$ | $\begin{aligned} & \text { 아N } \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \mathfrak{g} \\ & \tilde{N} \end{aligned}$ | $$ | $\begin{aligned} & \mathfrak{g} \\ & \underset{\sim}{N} \end{aligned}$ | $\begin{aligned} & 0 \\ & \stackrel{\rightharpoonup}{0} \\ & \stackrel{0}{寸} \end{aligned}$ | $\begin{aligned} & 0 \\ & \stackrel{0}{7} \\ & \underset{\sim}{7} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { oे } \\ & \text { In } \end{aligned}$ | $\begin{aligned} & \stackrel{O}{7} \\ & \stackrel{\rightharpoonup}{g} \\ & \hline \end{aligned}$ | $\begin{aligned} & \stackrel{O}{1} \\ & \stackrel{\rightharpoonup}{7} \end{aligned}$ | $\begin{aligned} & 0 \\ & \underset{7}{9} \\ & \stackrel{\rightharpoonup}{7} \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 \\ & \text { O} \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{0}{0} \\ & \text { O } \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{-} \\ & \stackrel{-}{-} \end{aligned}$ | $\begin{aligned} & \stackrel{0}{-} \\ & \stackrel{\sim}{\mathrm{O}} \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { N- } \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \text { B } \\ & \text { N్స } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { N- } \end{aligned}$ | $\begin{aligned} & \text { O- } \\ & \text { N- } \end{aligned}$ | － | $\begin{array}{ll} 8 & 8 \\ \stackrel{-}{N} & \stackrel{1}{7} \end{array}$ |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | $\begin{aligned} & \infty \\ & \stackrel{\infty}{U} \\ & \stackrel{\sim}{2} \\ & \underset{y}{x} \\ & \underset{\sim}{x} \\ & \underset{\sim}{y} \\ & \hline \end{aligned}$ | $=$ |  |  | $=$ | ธ <br>  $\begin{aligned} & \text { y} \\ & \underset{\sim}{4} \end{aligned}$ <br>  |
| O. |  |  |  |  |  |  |  |  | $\begin{aligned} & \text { 을 } \\ & \text { 르N } \end{aligned}$ |  | $\begin{aligned} & \frac{2}{2} \\ & \frac{2}{2} \end{aligned}$ |  | $\begin{aligned} & \text { 을 } \\ & \text { 르N } \end{aligned}$ |  |  |  |  |  | $\begin{aligned} & \text { 을 } \\ & \frac{3}{3} \end{aligned}$ |  | O. | $\begin{aligned} & \text { 을 } \\ & \text { 立 } \end{aligned}$ |  | O |



|  | 1914 | 304,80 | 385,55 | 894,00 | 15,00 | APC | 3,28 | 4,00 | 6,9 | Vickers |  | 2,71\% | L | 20300 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1914 | 304,80 | 385,55 | 894,00 | 15,00 | SAPC | 3,79 | 4,00 | 6,9 | Vickers |  | 7,76\% | L | 20300 |  |
|  | 1914 | 304,80 | 385,55 | 894,00 | 15,00 | CP | 4,16 | 4,00 | 6,9 | Vickers Bofors |  | 8,45\% | BP | 20300 |  |
|  | " | 304,80 | 385,55 | 894,00 | 15,00 | APC | 3,35 | 4,00 | 6,9 | M/17-21 Bofors | 6,02\% | 2,89\% | T | 21500 |  |
|  | " | 304,80 | 385,55 | 894,00 | 15,00 | SAPC | 3,80 | 4,00 | 6,9 | $\begin{gathered} \mathrm{M} / 17-21 \\ \mathrm{La} \end{gathered}$ | 6,02\% | 8,39\% | T | 21500 |  |
|  | C. A. de 30.5 cm (No. | 304,80 | 385,55 | 894,00 | 15,00 | CP | 4,20 | 4,00 | 6,9 | Carraca |  | 8,45\% | BP | 21500 |  |
| Armstrong | 1) $L / 25.5$ <br> C. A. de 30.5 cm (No. | 304,80 | 323,87 | 547,00 | 22,50 | AP | 2,64 | 2,00 | 8.0 |  |  |  |  | 11500 |  |
| Armstrong | 2) $L / 25.5$ <br> C. H. de 28 cm molelo Barrios | 304,80 280,00 | 323,87 88,00 | 577,00 | 22,50 | AP Ball | 2,64 1,00 | 2,00 1,00 | 8.0 8.0 |  |  |  |  | 12200 |  |
| Krupp | $28 \mathrm{~cm} \mathrm{RKL/22} \mathrm{C/74}$ | 283,00 | 240,00 | 490,00 | 24,00 | AP | 2,45 | 2,00 | 8.0 |  |  | 1,46\% | BP | 10200 | Coast Defence |
|  | " | 283,00 | 240,00 | 490,00 | 24,00 | Common | 2,96 | 2,00 | 8.0 |  |  |  |  | 10200 |  |
| Hontoria | 280mm/35 M1883 | 280,00 | 315,00 | 620,00 | 13,50 | AP | 3,36 | 2,00 | 7.5 |  |  | 1,59\% | BP | 10400 | Pelayo, Infanta Maria Teresa, Emperador |
|  | " | 280,00 | 265,60 | 663,00 | 13,50 | Common | 3,40 | 2,00 | 7.5 |  |  | 5,27\% | BP | 10590 | Carlos V |
|  | " | 280,00 | 263,11 | 666,00 | 13,50 | SAP | 3,31 | 3,00 | 7.5 |  |  | 4,56\% | BP | 10600 |  |
| Krupp | $26 \mathrm{~cm} \mathrm{RKL} / 35 \mathrm{C} / 83$ | 263,00 | 275,00 | 530,00 | 22,00 | AP | 3,50 | 2,00 | 8.0 |  |  | 1,16\% | BP | 11400 | Coast Defence |
|  | " | 263,00 | 275,00 | 530,00 | 22,00 | Common | 4,00 | 2,00 | 8.0 |  |  | 3,82\% | BP | 11400 | Coast Defence |
|  | " | 263,00 | 275,00 | 530,00 | 22,00 | APC | 3,50 | 3,00 | 8.0 | C/01 |  |  |  | 12200 | Coast Defence |
|  | " | 263,00 | 275,00 | 530,00 | 22,00 | SAP | 4,00 | 3,00 | 8.0 |  |  |  |  | 12200 | Coast Defence <br> Numancia, Vitoria, Sa- |
| Armstrong | 10" 300-pdr MLR | 254,00 | 131,50 | 414,00 | 10,00 | Bolt | 1,59 | 2,00 | 3.51 |  |  |  |  | 4142 | dez Nunez |
|  | 10" 300 | 254,00 | 133,80 | 410,00 | 10,00 | Common | 2,24 | 2,00 | 3.51 |  |  |  |  | 4171 |  |
| Parrott | 10" 300-pdr MLR (14.4) | 254,00 | 154,22 | 356,62 | 15,00 | Solid | 1,86 | 2,00 | 8.0 |  |  |  |  | 5002 | Coast Defence |
|  | " | 254,00 | 113,40 | 416,05 | 15,00 | Hollow | 1,71 | 2,00 | 8.0 |  |  |  |  | 5453 |  |
| Armstrong | C.A. de 254 mm Pattern '83 L/26 | 254,00 | 204,11 | 586,00 | 23,00 | AP | 2,88 | 2,00 | 8.0 | Palliser |  | 1,11\% | BP | 12200 | Coast Defence |
|  | " | 254,00 | 181,44 | 606,00 | 23,00 | Comm |  | 2,00 | 8.0 |  |  | 1,75\% | BP | 12040 |  |
| Hontoria | 240mm/35 M1883 | 240,00 | 199,00 | 620,00 | 14,00 | AP | 3,37 | 2,00 | 7.0 | Palliser |  |  |  | 10000 | Reina Regente |
|  | " | 240,00 | 168,00 | 674,00 | 14,00 | Common | 3,41 | 2,00 | 7.0 |  |  |  |  | 10290 |  |


| 1,52\% | BP | 10600 |  |
| :---: | :---: | :---: | :---: |
| 5,39\% | BP | 10890 |  |
| 4,49\% | BP | 10890 |  |
|  |  | 15770 | Princesa de Asturias |
|  |  | 15960 |  |
|  |  | 6000 | Coast Defence |
|  |  | 7500 | Coast Defence |
|  |  | 11000 | Coast Defence |
|  |  | 11000 | Coast Defence |
|  |  | 9000 | Coast Defence |
|  | T | 11320 | Coast Defence <br> Vitoria, Zaragosa, Sa- |
| 0,88\% | BP | 4197 | (1874?) |
| 7,40\% | BP | 4197 |  |
|  |  | 10500 | Coast Defence |
|  |  | 10500 | Coast Defence |
|  |  | 10000 | Coast Defence |
| 6,23\% | BP | 5000 | Coast Defence |
| 6,23\% | BP | 5000 | Coast Defence |
|  |  | 4103 | Numancia, Vitoria, Arapiles, Mendez Nunez, |
| 5,39\% | BP | 4103 | Aragon class |
|  |  | 5464 | Coast Defence |
|  |  | 5621 | Coast Defence |
|  |  | 4711 | Coast Defence |
|  |  | 4922 | Coast Defence |
|  |  | 9900 | Coast Defence |


|  | " | 240,00 | 198,00 | 647,10 | 14,00 | AP | 3,30 | 2,00 | 7.0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | " | 240,00 | 167,00 | 704,00 | 14,00 | Common | 3,31 | 2,00 | 7.0 |
|  | " | 240,00 | 167,00 | 704,00 | 14,00 | SAP | 3,31 | 2,00 | 7.0 |
| Guillen | 240mm/42 M1896 | 240,00 | 150,00 | 800,00 | 25,00 | AP | 2,50 | 2,00 |  |
|  | C' ${ }^{\text {" }}$ | 240,00 | 150,00 | 800,00 | 25,00 | APC |  | 3,00 |  |
| Ordonez | C.H.S. de 24 cm Mod. 1881 | 240,00 | 139,00 | 400,00 | 16,00 | AP |  | 2,00 | 8.0 |
| Ordonez | ${ }_{1884}$ c.i.S. de 24 cm Mod. | 240,00 | 139,00 | 445,00 | 19,00 | AP |  | 2,00 | 8.0 |
| Ordonez | C.H.S.E. de 24 cm Mod. 1891 L/35 | 240,00 | 195,00 | 540,00 | 20,00 | AP |  | 2,00 | 8.0 |
|  | nowiter " ${ }^{\text {c }} 1801$ de | 240,00 | 195,00 | 540,00 | 20,00 | Common |  | 2,00 | 8.0 |
| Ordonez | howitzer Mod. 1891 de 24 cm <br> howitzer Mod. 1916 de | 240,00 | 140,00 | 349,00 | 68,00 | AP |  | 2,00 | 8.0 |
| Ordonez | $24 \mathrm{~cm} \mathrm{L/16}$ | 240,00 | 200,00 | 430,00 | 55,00 | CP |  | 2,00 | 8.0 |
| Armstrong | $\begin{aligned} & \text { 9"/14-12-Ton MLR } \\ & \text { (250-pdr) } \end{aligned}$ | 228,60 | 113,40 | 408,13 | 10,00 | AP | 2,23 | 2,00 | 2.0 |
|  | " | 228,60 | 113,40 | 408,13 | 10,00 | Common | 2,60 | 2,00 | 2.0 |
|  | 22 cm modelo Barrios 22 cm MLR (conver- | 220,00 | 43,00 |  |  | Ball | 1,00 | 1,00 |  |
| Palliser | sion of 28 cm Barrios) C.H.S.E. de 21 cm | 220,00 |  |  |  |  |  |  |  |
| Ordonez | Mod. 1891 L35 | 210,00 | 130,00 | 520,00 | 25,00 | AP |  | 2,00 | 8.0 |
|  | howitzer Mod. 1894 de | 210,00 | 130,00 | 520,00 | 25,00 | Common |  | 2,00 | 8.0 |
| Ordonez | 21 cm <br> howitzer H.R.S. Mod. | 210,00 |  |  |  | AP |  | 2,00 | 8.0 |
|  | 1872 de 21cm mortar Mod. 1864/65 | 210,00 | 80,20 | 256,00 | 42,00 | Common |  | 2,00 | 8.0 |
|  | de 21 cm <br> 8"/14.75 9-Ton MLR | 210,00 | 80,20 | 256,00 | 42,00 | Common |  | 2,00 | 8.0 |
| Armstrong | (180-pdr) | 203,20 | 81,65 | 408,13 | 10,00 | AP | 2,29 | 2,00 | 3.05 |
|  | " | 203,20 | 81,65 | 408,13 | 10,00 | Common | 2,67 | 2,00 | 3.05 |
| Parrott | 200-pdr MLR (199.8) | 203,20 | 79,38 | 406,60 | 15,00 | Solid | 2,01 | 2,00 | 8.0 |
|  | " | 203,20 | 68,04 | 438,91 | 15,00 | Hollow | 1,87 | 2,00 | 8.0 |
| Parrott | 150-pdr MLR (117) | 203,20 | 79,38 | 350,52 | 15,00 | Solid | 2,01 | 2,00 | 8.0 |
|  | " | 203,20 | 68,04 | 378,56 | 15,00 | Hollow | 1,87 | 2,00 | 8.0 |
| Armstrong | 8"/26 BLR Pattern B | 203,20 | 81,65 | 615,70 | 21,00 | AP | 2,62 | 2,00 | 8.0 |




## $\pi$ $\pi$ $\pi$ $\pi$ $\pi$

Coast Defence




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$\begin{array}{ll}8 & 0 \\ 8 & 0 \\ \circ & 0 \\ 1 & 0\end{array}$ $\begin{array}{ll}\circ & 8 \\ -1 & 8 \\ 0 & 0 \\ -1 & -1\end{array}$ $\begin{array}{ll}\circ & 0 \\ & 6 \\ \cdots & 9\end{array}$


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| $\stackrel{\sim}{\sim}$ | $\stackrel{\sim}{n}$ | $\stackrel{\circ}{\mathrm{m}}$ | $\stackrel{\circ}{\forall}$ |  |  |  |  | $\stackrel{\bullet}{\dot{\sim}}$ |  |  |  |  |  |  |  |  | ${ }^{\circ} \dot{\infty}$ | ${ }_{\infty}^{\circ}$ |  | $\mathrm{O}_{\infty}^{\circ}$ | ${ }_{\infty}^{\circ}$ | $\bigcirc$ |  | ${ }_{\infty}^{\circ}$ | $\bigcirc$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\stackrel{\circ}{\mathrm{N}}$ | O | $\stackrel{\circ}{\mathrm{N}}$ | $\underset{\sim}{\mathrm{N}}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | O | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | O | $\begin{aligned} & \circ \\ & \text { O } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | O | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | O | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | O | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{~N} \end{aligned}$ | $\begin{aligned} & \circ \\ & \text { ले } \end{aligned}$ | - | ○ | － |
| $\begin{gathered} \text { o } \\ \text { in } \end{gathered}$ | O N | $\begin{aligned} & \circ \\ & \stackrel{\circ}{N} \end{aligned}$ |  |  |  |  |  |  | $\stackrel{N}{N}$ | $\underset{\sim}{\sim}$ | $\begin{aligned} & N \\ & \underset{N}{N} \end{aligned}$ | $\begin{gathered} \stackrel{+}{\mathrm{m}} \\ \text { N } \end{gathered}$ | $\begin{aligned} & -\mathbf{6} \\ & { }^{2} \end{aligned}$ | $\underset{\sim}{\ddagger}$ | N | $\begin{aligned} & \infty \\ & \infty \\ & \underset{\sim}{\infty} \end{aligned}$ |  |  |  |  |  | $\stackrel{\text { N }}{\text { N }}$ | $\stackrel{0}{\stackrel{0}{N}}$ | $\stackrel{\infty}{\stackrel{\infty}{-}}$ | $\stackrel{-1}{9}$ |


| $\begin{aligned} & \text { Co } \\ & \text { E } \\ & 0 \\ & 0 \end{aligned}$ | $\stackrel{\square}{4}$ |  | $\begin{aligned} & \text { ㄷ } \\ & \text { E } \\ & \text { EO } \end{aligned}$ | E | $\stackrel{\square}{4}$ | E | $\stackrel{\square}{4}$ | $\stackrel{\square}{4}$ | ÉO | $\begin{aligned} & \text { U } \\ & \text { O } \end{aligned}$ | $\stackrel{\square}{4}$ |  | $\stackrel{\square}{4}$ |  | ס 0 0 0 0 | 0 | $\stackrel{\square}{4}$ | ¢ | $\stackrel{\square}{4}$ | $\begin{aligned} & \text { ס } \\ & \text { E } \\ & \text { EO } \end{aligned}$ | $\begin{aligned} & \text { ㄷ } \\ & \text { E } \\ & 0 \\ & 0 \end{aligned}$ | 只 | $\begin{aligned} & \text { Co } \\ & \text { E } \\ & 0 \\ & \hline 0 . \end{aligned}$ | $\begin{aligned} & \text { O } \\ & \text { 只 } \end{aligned}$ | $\frac{0}{6}$ | $\begin{aligned} & \text { O } \\ & \text { 足 } \end{aligned}$ | U |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & 8 \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 0 \\ & \underset{\sim}{N} \\ & \end{aligned}$ | $\begin{aligned} & \stackrel{0}{\mathrm{~N}} \\ & \underset{\sim}{n} \end{aligned}$ | $$ | $\begin{aligned} & \mathrm{O} \\ & \underset{-}{\prime} \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 \\ & 0 \\ & i \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{8}{7} \\ & \stackrel{1}{2} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \stackrel{\rightharpoonup}{7} \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { N్ల } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \mathrm{i} \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { I- } \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { I- } \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { 극 } \end{aligned}$ | $\begin{aligned} & 8 \\ & 7 \\ & 7 \end{aligned}$ | $\begin{aligned} & 8 \\ & \underset{\sim}{7} \end{aligned}$ | $\begin{aligned} & \circ \\ & \text { 각 } \end{aligned}$ | $\begin{aligned} & 8 \\ & \text {-i } \end{aligned}$ | $\begin{aligned} & \text { M } \\ & \underset{\sim}{7} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \underset{\sim}{7} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { Ni } \end{aligned}$ | $\begin{aligned} & \mathrm{B} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { N} \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { 잉 } \end{aligned}$ | $\begin{aligned} & 8 \\ & \stackrel{8}{n} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \stackrel{1}{2} \end{aligned}$ | － |
| $\begin{aligned} & \text { O } \\ & \text { B } \\ & \text { ద̂ } \end{aligned}$ | $$ | $\begin{aligned} & 8 \\ & 0 \\ & \infty \\ & \hline-8 \end{aligned}$ | $\begin{aligned} & \circ \\ & \hline 0 \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \stackrel{0}{5} \\ & \stackrel{y}{2} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { స్ } \end{aligned}$ | $\begin{aligned} & 8 \\ & \underset{-}{-1} \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 . \\ & 0 . \\ & 0 \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { O. } \\ & \text { © } \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { N } \\ & \hline \end{aligned}$ | $\begin{aligned} & \circ \\ & \hline 0 \\ & \hline 8 \end{aligned}$ | $\begin{aligned} & \text { @ } \\ & \stackrel{y}{\circ} \\ & \stackrel{\infty}{\circ} \end{aligned}$ | $\begin{aligned} & \text { J } \\ & -7 \end{aligned}$ |  | $$ | $J$ | $\begin{aligned} & \text { J } \\ & \text { O} \\ & 6 \end{aligned}$ | $\begin{aligned} & \text { J } \\ & \text { ö } \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { d } \\ & \text { O} \\ & 0 \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { M } \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{\circ}{\sim} \\ & \stackrel{N}{2} \end{aligned}$ | $\begin{aligned} & \stackrel{8}{\circ} \\ & \stackrel{N}{\gamma} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { N} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & 8 \\ & 8 \\ & 0 \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \circ \\ & \hline 8 \\ & \hline 0 \end{aligned}$ | $\begin{aligned} & 8 \\ & \hline 0 \\ & 0 . \\ & 0 . \end{aligned}$ | $\begin{aligned} & \text { O} \\ & 0 \\ & \text { ì } \end{aligned}$ | － |
| $\begin{aligned} & \circ \\ & \text { O- } \\ & \text { of } \end{aligned}$ | $$ | $\begin{aligned} & \text { O} \\ & \infty \\ & \infty \\ & \hline \end{aligned}$ | $\begin{aligned} & \circ \\ & \text { ó } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { - } \end{aligned}$ | $\begin{aligned} & 8 \\ & 8 \\ & 8 \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { Bi } \end{aligned}$ | $\begin{aligned} & 8 \\ & \hline-7 \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { in } \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { Oin } \end{aligned}$ | $\begin{aligned} & \text { ழ } \\ & \underset{\sim}{6} \end{aligned}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{N} \\ & \stackrel{\text { N}}{ } \end{aligned}$ | $\begin{aligned} & \text { N } \\ & \underset{\sim}{N} \\ & \hline \end{aligned}$ | $\begin{aligned} & 0 \\ & \mathrm{M} \\ & \text { \& } \end{aligned}$ | $\begin{aligned} & \dot{0} \\ & \underset{\sim}{0} \end{aligned}$ | $\begin{aligned} & 0 \\ & \mathrm{~N}^{-} \end{aligned}$ | $\begin{aligned} & \text { ழ } \\ & \underset{\sim}{\circ} \\ & \underset{\sim}{n} \end{aligned}$ |  | $\begin{aligned} & \text { ๒ } \\ & \text { if } \end{aligned}$ | $\begin{aligned} & \stackrel{N}{N} \\ & \underset{\sim}{\prime} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \underset{N}{N} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { N- } \\ & \text { N } \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 . \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \circ \\ & \text { O- } \\ & \text { of } \end{aligned}$ | $\begin{aligned} & \text { M } \\ & \text { No } \end{aligned}$ | $\begin{aligned} & \text { O- } \\ & \text { Hi } \end{aligned}$ | － | 160,00


| 8 | 8 |
| :--- | :--- |
| 0 | 0 |
| 0 | 0 |
|  |  |


| Hontoria | $160 \mathrm{~mm} / 17 \mathrm{M} 1879$ <br> No． 2 |
| :---: | :---: |
|  | ＂ |
|  | ＂ |
|  | 160mm／18 M 1879 |
| Hontoria | No． 3 |
| Hontoria | $160 \mathrm{~mm} / 35 \mathrm{M} 1883$ |
|  | ＂ |
|  | ＂ |
|  | QFC |
|  | QFC |
| Vickers | 6＂／50 Mks．T，U |
| Armstrong | 15cm／26．1 Pattern＇81 |
|  | ＂ |
| Armstrong | $15 \mathrm{~cm} / 32$ Pattern＇83 |
|  | ＂ |
|  | ＂ |
|  | ＂ |
|  | ＂ |
|  | ＂ |
| Palliser | 150mm／Mod． 1885 |
|  | C．H．S．de 15 cm Mod． |
| Ordonez | 1878 |
|  | ＂ |
|  | canon H．S．E．Mod． |
| Ordonez | 1885 de 15 cm |
|  | ＂ |
| Rueda | 150mm／48．3 |
|  | ＂ |
|  | C．Ac．De 15 cm Tr． |
| Trubia | Mod． 1903 L／45 |




| $1,30 \%$ | BP | 8330 | Tordenskjold |
| ---: | :--- | ---: | :--- |
| $2,40 \%$ | BP | 8330 |  |
| $4,95 \%$ | BP | 8330 |  |
| $2,77 \%$ | T | 15855 | Niels luel (plan) |
| $12,61 \%$ | T | 15855 |  |
| $1,37 \%$ | BP | 6920 | Helgoland |
| $5,25 \%$ | BP | 7200 |  |
| $2,55 \%$ | BP | 7400 |  |
| $5,47 \%$ | BP | 7400 |  |
| $1,95 \%$ | BP | 12500 | Iver Hvitfeldt |
| $5,61 \%$ | BP | 12500 |  |
| $1,95 \%$ | BP | 12600 | Iver Hvitfeldt |
| $5,61 \%$ | BP | 12600 |  |
| $1,32 \%$ | BP | 6100 | Helgoland |
| $5,35 \%$ | BP | 6350 |  |
| $2,54 \%$ | BP | 6550 |  |
| $5,12 \%$ | BP | 6550 |  |
| $1,10 \%$ | BP | 3400 | Gorm |
| $6,61 \%$ | BP | 3400 |  |
| $1,10 \%$ | BP | 3400 | Odin |
| $6,61 \%$ | BP | 3400 |  |


|  |  | 37,00 | 0,47 | 405,00 |  | CP |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Maxim | $37 \mathrm{~mm} / 26.5$ | 37,00 | 0,42 | 549,00 |  | AP |  |  |  |  |
|  |  | 37,00 | 0,42 | 549,00 |  | CP |  |  |  |  |
|  | 70mm/15 M. 1879 |  |  |  |  |  |  |  |  |  |
| Hontoria | [ PFC ] ${ }^{\text {d }}$ | 66,00 | 3,85 |  |  | CP |  |  |  |  |
|  | [BL] | 66,00 | 2,70 | 315,00 |  | CP |  |  |  |  |
|  | DENMARK |  |  |  |  |  |  |  |  |  |
| Krupp | 35.5 cm RKL/25 C/80 | 355,00 | 525,00 | 537,00 | 13,00 | AP | 2,71 | 2,00 | 4.0 | Gruson |
|  | " | 355,00 | 525,00 | 537,00 | 13,00 | AP | 2,71 | 2,00 | 4.0 |  |
|  | " | 355,00 | 525,00 | 537,00 | 13,00 | Common | 3,29 | 2,00 | 4.0 |  |
| Krupp | 30.5 cm SKL/45 C/07 | 305,00 | 390,00 | 855,00 | 13,50 | APC | 3,20 | 3,00 | 5.5 | M. 1908 |
|  | " | 305,00 | 333,00 | 925,00 | 13,50 | CP | 3,44 | 3,00 | 5.5 | M. 1908 |
| Krupp | $30.5 \mathrm{~cm} \mathrm{RKL} / 22 \mathrm{C} / 78$ | 305,00 | 329,00 | 475,00 | 13,00 | AP | 2,68 | 2,00 | 4.5 | Gruson Chilled |
|  | " | 305,00 | 282,00 | 510,00 | 13,00 | Common | 2,70 | 2,00 | 4.5 |  |
|  | " | 305,00 | 329,00 | 510,00 | 13,00 | AP | 2,68 | 2,00 | 4.5 | C/81 Steel |
|  | " | 305,00 | 329,00 | 510,00 | 13,00 | Common | 3,25 | 2,00 | 4.5 |  |
| Krupp | 26cm MRKU $35 \mathrm{C} / 86$ | 263,00 | 205,00 | 610,00 | 25,00 | AP | 2,61 | 2,00 | 5.0 |  |
|  | " | 263,00 | 205,00 | 610,00 | 25,00 | Common | 3,16 | 2,00 | 5.0 |  |
|  | " | 263,00 | 205,00 | 615,00 | 25,00 | AP | 2,61 | 2,00 | 5.0 |  |
|  | " | 263,00 | 205,00 | 615,00 | 25,00 | Common | 3,15 | 2,00 | 5.0 |  |
| Krupp | 26cm RKL/22 C/76 | 263,00 | 205,00 | 475,00 | 12,00 | AP | 2,61 | 2,00 | 4.7 | Gruson Chilled |
|  | " | 263,00 | 177,50 | 510,00 | 12,00 | Common | 3,16 | 2,00 | 4.7 |  |
|  | " | 263,00 | 205,00 | 500,00 | 12,00 | AP | 2,60 | 2,00 | 4.7 | Steel |
|  | " | 263,00 | 205,00 | 500,00 | 12,00 | Common | 3,10 | 2,00 | 4.7 |  |
|  | 10"/14 18-Ton MLR |  |  |  |  |  |  |  |  |  |
| Armstrong | M. 1870 | 254,00 | 181,44 | 417,00 | 7,00 | AP | 2,56 | 2,00 | 3.35 | Palliser |
|  | " | 254,00 | 181,44 | 417,00 | 7,00 | Common | 3,03 | 2,00 | 3.35 |  |
|  | 10"/14.5 18.5-Ton |  |  |  |  |  |  |  |  |  |
| Armstrong | MLR M. 1874 | 254,00 | 181,44 | 417,00 | 7,00 | AP | 2,56 | 2,00 | 3.35 | Palliser |
|  |  | 254,00 | 181,44 | 417,00 | 7,00 | Common | 3,03 | 2,00 | 3.35 |  |



| Finspong | $\begin{aligned} & \text { 15cm.K./18.9 MLR } \\ & \text { M. } 1868 \end{aligned}$ | 153,50 | 25,00 | 328,00 | 7,00 | Common |  | 2,00 |  |  | 7,60\% | BP | 2155 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Bofors | $15 \mathrm{~cm} . \mathrm{K} . / 45 \mathrm{M} / 22$ | 149,10 | 46,70 | 825,00 | 30,00 | SAPBC | 4,40 | 8,50 | 4.2 |  |  |  | 19635 | Niels luel (1922) |
|  | " | 149,10 | 45,80 | 835,00 | 30,00 | APC |  | 4,00 |  |  |  |  | 17800 |  |
| Bofors | 15cm.K./50 M/06 | 149,10 | 51,00 | 820,00 | 30,00 | APC | 3,78 | 3,00 | 2.0 |  | 1,52\% | T | 16377 | Peder Skram |
|  | " | 149,10 | 51,00 | 820,00 | 30,00 | SAP | 4,10 | 3,00 | 2.0 | C/06 | 6,39\% | T | 16377 |  |
|  | " | 149,10 | 51,00 | 830,00 | 30,00 | APC | 3,78 | 3,00 | 2.0 |  | 1,52\% | T | 16542 |  |
|  | " | 149,10 | 51,00 | 830,00 | 30,00 | SAP | 4,10 | 3,00 | 2.0 | C/06 | 6,39\% | T | 16542 |  |
| Bofors | 15cm.K./43 M/01 | 149,10 | 51,00 | 700,00 | 30,00 | APC | 3,78 | 3,00 | 2.0 |  | 1,52\% | T | 14401 | Olfert Fischer |
|  | " | 149,10 | 51,00 | 700,00 | 30,00 | SAP | 4,10 | 3,00 | 2.0 | C/06 | 6,39\% | T | 14401 |  |
| Bofors | 15cm.K./43 M/96 | 149,10 | 51,00 | 700,00 | 30,00 | APC | 3,78 | 3,00 | 2.0 |  | 1,52\% | T | 14401 | Herluf Trolle |
|  | " | 149,10 | 51,00 | 700,00 | 30,00 | SAP | 4,10 | 3,00 | 2.0 | C/06 | 6,39\% | T | 14401 |  |
| Krupp | 15cm SKL/35 C/88 | 149,10 | 51,00 | 575,00 | 20,00 | AP | 3,35 | 2,00 | 4.0 |  | 1,33\% | BP | 9460 | Hekla |
|  | " | 149,10 | 51,00 | 575,00 | 20,00 | Common | 4,00 | 2,00 |  |  | 3,82\% | BP | 9460 |  |
| Krupp | 15cm RKL/35 C/80 | 149,10 | 51,00 | 560,00 | 20,00 | AP | 3,35 | 2,00 | 5.5 |  | 1,33\% | BP | 9250 | Fyen |
|  | " | 149,10 | 51,00 | 560,00 | 20,00 | Common | 4,00 | 2,00 |  |  | 3,82\% | BP | 9250 |  |
| Krupp | 15cm RKL/25 C/78 | 149,10 | 39,00 | 476,00 | 13,00 | AP | 2,72 | 2,00 | 2.6 | Gruson Chilled | 1,28\% | BP | 5580 | Fyen |
|  | " | 149,10 | 31,50 | 513,00 | 13,00 | Common | 2,66 | 2,00 | 2.6 |  | 6,03\% | BP | 5565 |  |
| Krupp | 15cm RKL/22 C/80 | 149,10 | 39,00 | 470,00 | 13,00 | AP | 2,72 | 2,00 | 2.6 | Gruson Chilled | 1,28\% | BP | 5515 |  |
|  |  | 149,10 | 31,50 | 515,00 | 13,00 | Common | 2,66 | 2,00 | 2.6 |  | 6,03\% | BP | 5585 |  |
| Finspong | 18-pdr MLR <br> (14cm/20.2) M. 1863 <br> 18-pdr MLR | 138,50 | 17,50 | 328,00 | 7,00 | Common | 2,34 | 2,00 | 2.0 |  | 5,71\% | BP | 2050 |  |
| Palliser-type | $\begin{aligned} & (13.85 \mathrm{~cm} / 17.2) \\ & \text { 12-pdr MLR } \end{aligned}$ | 138,50 | 17,50 | 328,00 | 7,00 | Common |  | 1,00 | 1,00 |  | 2,86\% | BP | 2050 |  |
| Bronze | ( $12.75 \mathrm{~cm} / 20$ ) 12-pdr MLR <br> (12.75cm/22.8) | 127,50 | 13,50 | 314,00 | 7,00 | Common |  | 1,00 | 1,00 |  | 2,96\% | BP | 1900 |  |
| Finspong | M. 1862 | 127,50 | 13,50 | 314,00 | 7,00 | Common |  | 1,00 | 1,00 |  | 2,96\% | BP | 1930 |  |
| Bofors | 12cm.K./40 M/32 | 120,00 | 20,00 | 770,00 | 20,00 | SAPBC | 3,85 | 8,50 | 3.0 |  |  |  | 12500 | Ingolf |
| Krupp | 12cm RKL/30 C/84 | 120,00 | 26,00 | 525,00 | 25,00 | AP |  | 2,00 | 3.5 | Steel | 2,88\% | BP | 8930 | Iver Hvitfeldt |
|  | " | 120,00 | 26,00 | 525,00 | 25,00 | Common |  | 2,00 | 3.5 |  | 6,54\% | BP | 8930 |  |
| Krupp | 12cm RKL/25 C/79 | 120,00 | 20,00 | 455,00 | 13,00 | AP |  | 2,00 | 4.0 | Gruson Chilled | 1,25\% | BP | 5000 | Helgoland, Tordenskjold |
|  | " | 120,00 | 20,00 | 455,00 | 13,00 | AP |  | 2,00 | 4.0 | Steel | 3,00\% | BP | 5000 |  |




| Krupp | " | 240,00 | 120,00 | 390,00 | 7,25 | Common |  | 2,00 |  | C/80 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 24 cm RK L/25 C/78 | 238,00 | 139,00 | 470,00 | 12,50 | AP | 3,50 | 2,00 |  |  |
|  | " | 238,00 | 139,00 | 470,00 | 12,50 | Common |  | 2,00 |  |  |
| Krupp | $24 \mathrm{~cm} \mathrm{RK} \mathrm{L} 30 \mathrm{C} / 80$ | 238,00 | 215,00 | 505,00 | 14,50 | AP |  | 2,00 |  |  |
|  | " | 238,00 | 195,00 | 530,00 | 14,50 | Common |  | 2,00 |  |  |
| Krupp | 24cm MRK L/35 C/88 | 238,00 | 215,00 | 550,00 | 17,50 | AP | 3,50 | 2,00 |  | C/80 |
|  | " | 238,00 | 215,00 | 550,00 | 17,50 | Common |  | 2,00 |  | C/80 |
| Krupp | $24 \mathrm{~cm} \mathrm{SK} \mathrm{L/40} \mathrm{C/97}$ | 238,00 | 170,00 | 780,00 | 20,00 | AP |  | 2,00 | 4.5 |  |
|  | 24cm SKL/40 C/99 | 238,00 | 170,00 | 780,00 | 20,00 | CP |  | 2,00 | 4.5 |  |
| Krupp | No. 1 | 238,00 | 170,00 | 820,00 | 20,00 | AP |  | 2,00 | 4.5 |  |
|  | 24cm SKL/40 C/01 | 238,00 | 170,00 | 820,00 | 20,00 | CP |  | 2,00 | 4.5 |  |
| Krupp | No. 2 | 238,00 | 170,00 | 850,00 | 20,00 | AP |  | 2,00 | 4.5 |  |
|  | " | 238,00 | 170,00 | 850,00 | 20,00 | CP |  | 1,00 | 4.5 |  |
| Armstrong | 9"/14 12.5-Ton MLR | 228,60 | 113,00 | 450,00 | 10,00 | AP | 2,23 | 2,00 | 2.0 | Palliser |
|  | 21cm MRKL35 C/86 | 228,60 | 119,00 | 438,50 | 10,00 | Common | 2,73 | 2,00 | 2.0 |  |
| Krupp | No. 1 | 209,30 | 140,00 | 530,00 | 13,00 | AP | 3,60 | 2,00 | 6.5 |  |
|  | " | 209,30 | 140,00 | 530,00 | 13,00 | Common |  | 2,00 | $6.5$ |  |
|  | " | 209,30 | 140,00 | 550,00 | 13,00 | AP | 3,60 | 2,00 | 6.5 |  |
|  | " | 209,30 | 140,00 | 550,00 | 13,00 | Common |  | 2,00 | 6.5 |  |
|  | " | 209,30 | 140,00 | 530,00 | 25,00 | AP | 3,60 | 2,00 | 6.5 |  |
|  | " | 209,30 | 140,00 | 530,00 | 25,00 | Common |  | 2,00 | 6.5 |  |
|  | " | 209,30 | 140,00 | 550,00 | 25,00 | AP | 3,60 | 2,00 | 6.5 |  |
|  | 21cm MRKL/35 C/92 | 209,30 | 140,00 | 550,00 | 25,00 | Common |  | 2,00 | 6.5 |  |
| Krupp | No. 2 | 209,30 | 140,00 | 580,00 | 25,00 | AP | 3,60 | 2,00 | 6.5 |  |
|  | " | 209,30 | 140,00 | 580,00 | 25,00 | Common |  | 2,00 | 6.5 |  |
|  | " | 209,30 | 140,00 | 580,00 | 14,00 | AP | 3,60 | 2,00 | 6.5 |  |
|  | " | 209,30 | 140,00 | 580,00 | 14,00 | Common |  | 2,00 | 6.5 |  |
| Armstrong | 7"/15.9 7.17-Ton MLR | 177,80 | 52,00 | 475,00 | 12,00 | AP | 2,17 | 2,00 | 2.0 | Palliser |
|  | " | 177,80 | 53,00 | 477,00 | 12,00 | Common | 2,59 | 2,00 | 2.0 |  |


| Gruson |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Chilled | 1,67\% | BP | 5200 | Atjeh |
|  | 5,88\% | BP | 5305 |  |
|  |  |  | 11700 | Reinier Claessen, Koningin Wilhelmina |
|  | 5,86\% | BP | 10904 |  |
|  |  |  |  | Amstel |
|  |  |  | 5036 | Watergeus, Marnix, Banda |
|  |  |  | 5111 |  |
| Gruson |  |  |  | Alkmaar, Sommelsdijk, |
| Chilled | 1,28\% | BP | 5980 | Java, Aruba, |
|  | 6,03\% | BP |  | Batavia, Suriname, Coast Defence |
|  | 6,03\% |  | 6090 | Coast Defence |
|  | 1,57\% | BP | 11360 |  |
|  | 4,51\% | BP | 11360 |  |
|  |  |  |  | Evertsen, Coast |
|  | 1,89\% | PA | 12200 | Defence |
|  | 8,80\% | PA | 12200 |  |
| C/01 | 7,56\% | T | 12500 |  |
|  | 9,76\% | $T$ | 12500 |  |
|  | 1,89\% | PA | 12650 | Holland, Coast Defence |
|  | 8,80\% | PA | 12650 |  |
| C/01 | 7,56\% | T | 13100 |  |
|  | 9,76\% | T | 13100 |  |
|  |  |  |  | Gelderland, Coast |
| C/01 | 7,56\% | T | 13100 | Defence |
|  | 9,76\% | T | 13100 |  |
|  |  |  |  | Koningin |
| C/01 | 7,56\% | T | 13350 | Regentes |
|  | 9,76\% | T | 13350 |  |
|  | 1,89\% | PA | 13660 | Coast Defence |
|  | 9,29\% | PA | 13660 |  |
|  | 7,56\% | T | 14700 | Tromp, Heemskerck, De Zeven Provincien, |


| Krupp | 17 cm RKL/25 C/72 | 172,60 | 60,00 | 475,00 | 11,00 | AP | 2,70 | 2,00 | 3.7 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | " | 172,60 | 51,00 | 515,00 | 11,00 | Common | 2,79 | 2,00 | 3.7 |
| Krupp | 17cm RKL/35 C/84 | 172,60 | 78,00 | 585,00 | 25,00 | AP | 3,50 | 2,00 | 5.5 |
|  | " | 172,60 | 51,20 | 720,00 | 25,00 | CP | 2,79 | 2,00 | 5.5 |
|  | $\begin{aligned} & \text { Canon-Obusier } 30 \\ & \text { (SB) } \end{aligned}$ | 164,70 | 15,30 | 538,70 | 12,00 | Ball | 1,00 | 1,00 | 2.5 |
| Armstrong | 70-pdr MLR | 162,60 | 32,52 | 453,10 | 15,00 | Bolt | 1,50 | 2,00 | 2.66 |
|  | " | 162,60 | 31,80 | 453,10 | 15,00 | Common | 2,30 | 2,00 | 2,66 |
|  | $15 \mathrm{~cm} \mathrm{RKL/25} \mathrm{C/75}$ |  |  |  |  |  |  |  |  |
| Krupp | No. 1 | 149,10 | 39,00 | 475,00 | 14,50 | AP | 2,72 | 2,00 | 2.6 |
|  | " | 149,10 | 31,50 | 528,00 | 14,50 | Common | 2,66 | 2,00 | 2.6 |
|  | 15 cm RKL/35 C/85 |  |  |  |  |  |  |  |  |
| Krupp | No. 2 | 149,10 | 51,00 | 610,00 | 25,00 | AP | 3,35 | 2,00 | 4.3 |
|  | " ${ }^{\text {" }}$ | 149,10 | 51,00 | 610,00 | 25,00 | Common | 4,00 | 2,00 | 4.3 |
|  | $15 \mathrm{~cm} \mathrm{SKL} / 35 \mathrm{C} / 88$ |  |  |  |  |  |  |  |  |
| Krupp | No. 1 | 149,10 | 45,50 | 650,00 | 30,00 | AP | 3,18 | 2,00 | 5.7 |
|  | " | 149,10 | 45,50 | 650,00 | 30,00 | Common | 3,84 | 2,00 | 5.7 |
|  | " | 149,10 | 41,00 | 680,00 | 30,00 | CP | 3,01 | 3,00 | 5.7 |
|  | " | 149,10 | 41,00 | 680,00 | 30,00 | HE | 3,39 | 3,00 | 5.7 |
|  | 15 cm SKL/40 C/92 |  |  |  |  |  |  |  |  |
| Krupp | No. 2 | 149,10 | 45,50 | 680,00 | 30,00 | AP | 3,18 | 2,00 | 5.6 |
|  | " | 149,10 | 45,50 | 680,00 | 30,00 | Common | 3,84 | 2,00 | 5.6 |
|  | " | 149,10 | 41,00 | 725,00 | 30,00 | CP | 3,01 | 3,00 | 5.6 |
|  | " | 149,10 | 41,00 | 725,00 | 30,00 | HE | 3,39 | 3,00 | 5.6 |
|  | $15 \mathrm{~cm} \mathrm{SKL} / 40 \mathrm{C} / 99$ |  |  |  |  |  |  |  |  |
| Krupp | No. 3 | 149,10 | 41,00 | 725,00 | 30,00 | CP | 3,01 | 3,00 | 5.6 |
|  | " | 149,10 | 41,00 | 725,00 | 30,00 | HE | 3,39 | 3,00 | 5.6 |
|  | $15 \mathrm{~cm} \mathrm{SKL/40} \mathrm{C/00}$ |  |  |  |  |  |  |  |  |
| Krupp | No. 4 | 149,10 | 41,00 | 745,00 | 30,00 | CP | 2,96 | 3,00 | 5.3 |
|  | " | 149,10 | 41,00 | 745,00 | 30,00 | HE | 3,31 | 3,00 | 5.3 |
|  | " | 149,10 | 45,50 | 750,00 | 30,00 | AP | 2,96 | 3,00 | 4,0 |
|  | " | 149,10 | 45,50 | 750,00 | 30,00 | CP | 3,39 | 3,00 | 4,0 |
|  | 15 cm SKL/40 C/05 |  |  |  |  |  |  |  |  |
| Krupp | No. 5 | 149,10 | 41,00 | 850,00 | 30,00 | CP | 2,96 | 3,00 | 5.3 |
|  | " | 149,10 | 41,00 | 850,00 | 30,00 | HE | 3,31 | 3,00 | 5.3 |
| Bofors | 15cm K. $/ 50 \mathrm{M} / 24 \mathrm{No}$. | 149,10 | 46,70 | 900,00 | 29,00 | SAPBC | 4,40 | 8,50 | 5.0 |



| 75,00 | 6,35 | 640,00 | 30,00 | SAP | 4,00 | 4,00 | 4.8 |  |  |  | 10120 | Heemskerck, Holland, Koningin Wilhelmina Fret, Sumatra, De Zeven |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 75,00 | 5,85 | 900,00 | 30,00 | APC | 3,30 | 4,00 | 3.5 | M. 1911 |  |  | 12380 | Provincien |
| 75,00 | 5,85 | 900,00 | 30,00 | SAP | 3,70 | 4,00 | 3.5 | M. 1911 |  |  | 12380 |  |
| 75,00 | 5,85 | 605,00 | 30,00 | SAP | 3,70 | 4,00 | 3.4 | M. 1911 |  |  | 9300 | 'G' \& 'Z' class TB |
| 267,00 | 174,50 | 395,00 | 7,50 | AP | 2,16 | 2,00 | 2.5 | Palliser |  |  | 3249 | Skorpionen, Thor |
| 267,00 | 143,50 | 373,00 | 7,50 | Common | 2,07 | 2,00 | 2.5 |  |  |  | 2923 |  |
| 267,00 | 178,50 | 440,00 | 10,00 | AP | 2,20 | 2,00 | 4.5 | Palliser |  |  | 4656 | Uller, Brage |
| 267,00 | 143,50 | 468,00 | 10,00 | Common | 2,07 | 2,00 | 4.5 |  |  |  | 4718 |  |
| 267,00 | 203,50 | 472,00 | 12,00 | AP | 2,51 | 2,00 | 4.5 | Palliser |  |  | 5957 | Vidar |
| 267,00 | 143,50 | 470,00 | 12,00 | Common | 2,07 | 2,00 | 4.5 | Gruson |  |  | 5375 |  |
| 263,00 | 205,00 | 480,00 | 16,50 | AP | 2,61 | 2,00 | 4.5 | Chilled |  |  | 7500 | Sleipner |
| 263,00 | 177,50 | 485,00 | 16,50 | Common | 2,66 | 2,00 | 4.5 | Gruson |  |  | 7250 |  |
| 263,00 | 275,00 | 525,00 | 12,00 | AP | 3,50 | 2,00 | 4.5 | Chilled | 1,16\% | BP | 8380 | Gor |
| 263,00 | 275,00 | 525,00 | 12,00 | Common | 3,95 | 2,00 | 4.5 |  | 3,82\% | BP | 8380 |  |
| 240,00 | 189,94 | 883,92 | 15,00 | APC | 3,25 | 4,00 | 4.88 |  |  |  | 17300 | Nidaros |
| 209,30 | 140,00 | 550,00 | 25,00 | AP | 3,60 | 2,00 | 5.5 |  | 1,50\% | BP | 11550 | Aegir |
| 209,30 | 140,00 | 550,00 | 25,00 | CP |  | 2,00 | 5.5 |  | 4,00\% | BP | 11550 |  |
| 209,00 | 142,00 | 700,00 | 15,00 | APC |  | 2,00 | 5.18 |  |  |  | 11370 | Harald Haarfagre, Norge |
| 200,00 | 75,00 | 420,00 | 12,00 | AP | 2,20 | 2,00 | 2.0 |  |  |  | 4700 |  |
| 200,00 | 60,00 | 375,00 | 12,00 | Common | 2,28 | 2,00 | 2.0 |  | 5,00\% | BP | 3990 |  |
| 167,00 | 49,80 | 405,00 | 12,00 | AP | 2,50 | 2,00 | 2.0 |  |  |  | 4500 |  |
| 167,00 | 37,50 | 436,00 | 12,00 | Common | 2,20 | 2,00 | 2.0 |  |  |  | 4460 |  |
| 155,00 | 26,80 | 340,00 | 12,00 | Common | 1,95 | 2,00 | 2.0 |  |  |  | 3400 |  |
| 155,00 | 25,00 | 360,00 | 12,00 | Com |  | 2,00 |  |  |  |  | 3600 |  |
| 149,10 | 39,00 | 480,00 | 13,00 | AP | 2,72 | 2,00 | 2.6 | Chilled | 1,28\% | BP | 5625 | Sleipner |


| Krupp | 7.5cm SKL55 C/10 |
| :---: | :---: |
|  |  |
| Krupp | 7.5 cm SKL/30 C/12 |
|  | NORWAY |
| Armstrong | 10.6"/12.5 18.2-Ton MLR No. 1 |
|  | " |
|  | 10.6"/13.8 19.7-Ton |
| Armstrong | MLR No. 2 |
|  | " |
|  | 10.6"/16.7 21.7-Ton |
| Armstrong | MLR No. 3 |
|  | " |
|  | $26 \mathrm{~cm} \mathrm{RKL/22} \mathrm{C/76}$ |
| Krupp | No. 1 |
|  | " |
| Krupp | $26 \mathrm{~cm} \mathrm{RKL} / 30 \mathrm{C} / 84$ |
|  | No. 2 |
|  | " |
| EOC | 9.45"/50 Pattern E |
| Krupp | 21cm MRKL/35 C/86 |
|  | " |
|  |  |
| Armstrong |  |
| Palliser | $\begin{aligned} & 20 \mathrm{~cm} / 13.1 \text { 8.66-Ton } \\ & \text { MLR } \end{aligned}$ |
|  | " |
| Palliser | 6.6"/17 4.9-Ton MLR |
|  | " |
| Palliser | 6.1 "/16.8 3.4-Ton |
|  | MLR |
|  | 24-pdr MLR |
| Finspong | ( $15.5 \mathrm{~cm} / 22$ ) |
| Krupp | $15 \mathrm{~cm} \mathrm{RKL} / 25 \mathrm{C} / 75$ |



| Krupp | " | 283,00 | 240,00 | 680,00 | 25,00 | SAP | 2,90 | 3,00 | 5.0 | M. 1901 | 7,75\% | 3,60\% | PA | 14940 | Torgud Reis |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 28 cm MRKL/40 C/90 | 283,00 | 240,00 | 745,00 | 25,00 | APC | 2,60 | 3,00 | 5.0 |  |  |  |  | 15678 |  |
|  | " | 283,00 | 240,00 | 745,00 | 25,00 | SAP | 2,90 | 3,00 | 5.0 |  |  |  |  | 15678 | Yavuz |
| Krupp | $28 \mathrm{~cm} \mathrm{SKL} / 50 \mathrm{C} / 09$ | 283,00 | 302,00 | 870,00 | 22,50 | APC | 3,20 | 4,00 | 6.5 | Palliser |  |  |  | 23260 |  |
|  | " | 283,00 | 302,00 | 870,00 | 22,50 | SAP | 3,50 | 4,00 | 6.5 |  |  |  |  | 23260 |  |
| Armstrong | 10"/15 18-Ton MLR | 254,00 | 181,44 | 415,58 | 10,00 | AP | 2,60 | 2,00 | 3.35 |  |  |  |  | 4513 | Messudieh |
|  | " | 254,00 | 180,53 | 416,66 | 10,00 | Common | 3,02 | 2,00 | 3.35 |  |  | 5,03\% | BP | 4523 |  |
| Krupp | 24cm MRK L/35 C/86 | 235,40 | 132,50 | 530,00 | 20,00 | AP |  | 2,00 | 5.0 |  |  | 2,26\% | PA | 9000 | Coast Defence, Osmanieh |
|  | ${ }^{\prime}$ | 235,40 | 119,50 | 490,00 | 20,00 | CP |  | 2,00 | 5.0 |  |  | 5,69\% | PA | 8090 |  |
|  | " | 235,40 | 160,00 | 630,00 | 20,00 | APC | 2,90 | 4,00 | 5.0 |  |  | 1,50\% | PA | 11700 |  |
| Vickers | 9.2"/46.7 Mk. T | 233,68 | 173,27 | 785,00 | 15,00 | AP | 3,00 | 2,00 |  | Palliser |  |  |  | 13380 | re-armed Messudieh |
|  | " ${ }^{\text {" }}$ | 233,68 | 172,37 | 785,00 | 15,00 | CP | 3,80 | 2,00 |  |  |  |  |  | 13380 |  |
|  | 9/13.9 12.5-Ton |  |  |  |  |  |  |  |  |  |  |  |  |  | Osmanieh, Assari Tewfik, Assari Sjevket, Avni Illah, Fetjo Bulend Idjalieh, Hamidieh |
| Armstrong | MLR | 228,60 | 116,12 | 438,91 | 10,00 | AP | 2,28 | 2,00 | 2.0 |  |  |  |  | 4569 |  |
|  | " | 228,60 | 113,40 | 432,64 | 10,00 | Common | 2,60 | 2,00 | 2.0 |  |  | 7,60\% | BP | 4468 |  |
| Krupp | $21 \mathrm{~cm} \mathrm{RKL/35} \mathrm{C/86}$ | 209,30 | 108,00 | 615,00 | 25,00 | AP | 2,70 | 2,00 | 6.5 |  |  |  |  | 11900 | Assari Tewfik |
|  | " | 209,30 | 108,00 | 615,00 | 25,00 | CP | 3,20 | 2,00 |  | Palliser |  | 5,37\% | BP | 11900 |  |
| Armstrong | 8"/14.75 9-Ton MLR | 203,20 | 81,65 | 408,13 | 10,00 | AP | 2,29 | 2,00 | 3.05 |  |  |  |  | 4103 | Osmanieh, Lufti Djelil |
|  | " | 203,20 | 81,65 | 316,08 | 10,00 | Common | 2,67 | 2,00 | 3.05 |  |  | 5,39\% | BP | 3007 |  |
| Armstrong | 7"/16 6.5-Ton MLR | 177,80 | 52,20 | 465,00 | 12,00 | AP | 2,18 | 2,00 | 2.0 | Palliser |  | 0,87\% | BP | 5095 | Assaor Sjevket, Lutfi Djelil, Idjalieh, |
|  | " | 177,80 | 52,60 | 463,00 | 12,00 | Common | 2,57 | 2,00 | 2.0 |  |  | 7,76\% | BP | 5078 | Messudieh |
| Krupp | 17cm RKL/25 C/74 | 172,60 | 60,00 | 475,00 | 11,00 | AP | 2,70 | 2,00 | 3.7 | Gruson Chilled |  | 1,67\% | BP | 5290 | Medjidieh |
|  | " | 172,60 | 51,00 | 515,00 | 11,00 | Common | 2,79 | 2,00 | 3.7 |  |  | 5,88\% | BP | 5415 |  |
| Bethlehem | 6"/44 | 152,40 | 47,63 | 685,80 | 20,00 | APC | 4,00 | 7,00 | 3.8 |  |  |  |  | 14369 | re-armed Messudieh |
| Vickers | 6"/45 Mk. | 152,40 | 45,36 | 762,00 | 15,00 | AP | 2,88 | 2,00 | 3.0 | Steel |  | 1,25\% | BP | 9986 |  |
|  | " | 152,40 | 45,36 | 762,00 | 15,00 | AP | 3,27 | 2,00 | 3.0 | Steel |  | 4,87\% | BP | 9986 |  |
|  | " | 152,40 | 45,36 | 762,00 | 15,00 | CP | 3,44 | 2,00 | 3.0 | Cast Iron |  | 4,75\% | BP | 9986 |  |
|  | " | 152,40 | 45,36 | 762,00 | 15,00 | Common | 3,61 | 2,00 | 3.0 | Cast Steel |  | 9,81\% | BP | 9986 |  |
| EOC | 6"/45 Pattern | 152,40 | 45,36 | 792,48 | 15,00 | AP | 2,88 | 2,00 | 4,57 | Steel |  | 1,25\% | BP | 10360 | Abdul Hamid |
|  | " | 152,40 | 45,36 | 792,48 | 15,00 | AP | 3,27 | 2,00 | 4,57 | Steel |  | 4,87\% | BP | 10360 |  |


|  | " | 152,40 | 45,36 | 792,48 | 15,00 | CP | 3,44 | 2,00 | 4,57 | Cast Iron | 4,75\% | BP | 10360 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | " | 152,40 | 45,36 | 792,48 | 15,00 | Common | 3,61 | 2,00 | 4,57 | Cast Steel | 9,81\% | BP | 10360 |  |
| EOC | 6"/50 Pattern | 152,40 | 45,36 | 844,30 | 20,00 | CPC |  | 3,00 | 6.09 |  | 8,66\% | BP | 12526 | Sultan Osman I |
| Vickers | 6"/50 Mk. M | 152,40 | 45,36 | 914,40 | 15,00 | CPC | 3,60 | 3,00 | 6.25 |  | 5,69\% | L | 13636 | Resadiye |
| Krupp | 15 cm RKL/22 C/ | 149,10 | 39,00 | 470,00 | 13,00 | AP | 2,72 | 2,00 | 2.6 | Gruson | 1,28\% | BP | 5615 |  |
|  | " | 149,10 | 31,50 | 515,00 | 13,00 | Common | 2,66 | 2,00 | 2.6 |  | 6,03\% | BP | 5705 |  |
| Krupp | 15cm RKL/25 C/75 | 149,10 | 39,00 | 495,00 | 13,00 | AP | 2,72 | 2,00 | 2.6 | Gruson Chilled | 1,28\% | BP | 5730 | Osmanieh, Hifzi Rahman |
|  | " | 149,10 | 31,50 | 536,00 | 13,00 | Common | 2,68 | 2,00 | 2.6 |  | 6,03\% | BP | 5890 |  |
| Krupp | 15 cm RKL/35 C/80 | 149,10 | 51,00 | 560,00 | 20,00 | AP | 3,35 | 2,00 | 5.5 |  | 1,33\% | BP | 9460 | Idjalieh |
|  | " | 149,10 | 51,00 | 560,00 | 20,00 | Common | 4,00 | 2,00 | 5.5 |  | 3,82\% | BP | 9460 |  |
| Krupp | 15cm SKL/40 C/06 | 149,10 | 41,00 | 840,00 | 30,00 | SAP | 3,01 | 3,00 | 3.8 |  | 7,56\% | T | 14570 | Assari Tewfik, Avni Illih, Fethi Bulend |
|  | " | 149,10 | 41,00 | 840,00 | 30,00 | HE | 3,39 | 3,00 | 3.8 |  | 9,76\% | T | 14570 |  |
| Krupp | 15 cm SKL/45 C/09 | 149,10 | 45,30 | 835,00 | 30,00 | APC | 3,70 | 4,00 | 4.0 |  |  | T | 18446 | Yavuz, Midilli |
|  | " | 149,10 | 45,30 | 835,00 | 30,00 | SAP | 4,10 | 4,00 | 4.0 |  |  | T | 18446 |  |
| Krupp | 12cm RKL/25 C/78 | 120,00 | 20,00 | 455,00 | 13,00 | AP | 2,68 | 2,00 | 4.0 | Gruson Chilled | 1,25\% | BP | 5090 | Hifzi Rahman |
|  | " | 120,00 | 20,00 | 455,00 | 13,00 | AP | 2,68 | 2,00 | 4.0 | Steel | 3,00\% | BP | 5090 |  |
|  | " | 120,00 | 16,40 | 495,00 | 13,00 | Common | 2,66 | 2,00 | 4.0 |  | 6,71\% | BP | 5120 |  |
| Krupp | $12 \mathrm{~cm} \mathrm{SKL/40} \mathrm{C/97}$ | 120,00 | 20,00 | 720,00 | 18,00 | SAP | 3,06 | 3,00 | 3.8 |  | 3,85\% | PA | 8860 | Assari Tewfik |
|  | " | 120,00 | 20,00 | 720,00 | 18,00 | CP | 3,05 | 3,00 | 3.8 |  | 6,35\% | PA | 8860 |  |
| Bethlehem | 4.7"/45 | 120,00 |  |  |  |  |  |  |  |  |  |  |  | Medjidieh |
| EOC | 4.7"/50 Pattern | 120,00 | 20,41 | 801,63 | 15,00 | AP | 3,02 | 2,00 | 4.57 | Cast Iron Palliser | 2,08\% | BP | 9178 | Abdul Hamid/Hamidieh |
|  | " | 120,00 | 20,41 | 801,63 | 15,00 | AP | 3,02 | 2,00 | 4.57 | Steel | 4,44\% | BP | 9178 |  |
|  | " | 120,00 | 20,41 | 801,63 | 15,00 | CP | 3,63 | 2,00 | 4.57 | Steel | 10,00\% | BP | 9178 |  |
| Krupp | $10.5 \mathrm{~cm} \mathrm{SKL} / 35 \mathrm{C} / 86$ | 105,00 | 18,20 | 580,00 | 25,00 | Common | 4,36 | 2,00 | 4.4 |  |  |  | 9475 | Osmanieh |
| Krupp | $10.5 \mathrm{~cm} \mathrm{SKL} / 35 \mathrm{C} / 91$ | 105,00 | 17,40 | 600,00 | 30,00 | SAP |  | 4,00 | 3.1 | M. 1907 | 2,30\% | PA | 11100 | Torgud Reis |
| Krupp | $10.5 \mathrm{~cm} \mathrm{SKL} / 40 \mathrm{C} / 97$ | 105,00 | 17,40 | 840,00 | 30,00 | SAP | 3,30 | 3,00 | 4.4 |  | 2,01\% | PA | 14060 | Berk I Satvet |
| Krupp | $10.5 \mathrm{~cm} \mathrm{SKL} / 45 \mathrm{C} / 12$ | 105,00 | 17,40 | 710,00 | 30,00 | SAP |  | 4,00 | 4.4 |  | 2,01\% | T | 13140 | Midilli |
| Canet | $100 \mathrm{~mm} / 50$ | 100,00 | 16,00 | 740,00 | 25,00 | SAPC | 3,20 | 2,00 | 3.7 |  |  |  | 10940 | Preveze |
| Krupp | $8.8 \mathrm{~cm} \mathrm{SKL} 30 \mathrm{C} / 89$ | 88,00 | 7,04 | 670,00 | 20,00 | SAP | 2,80 | 2,00 | 3.7 |  | 4,85\% | T | 7195 | Torgud Reis |

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\text { Veinticinco de Mayo } \\
\text { Almirante Brown } \\
\text { Buenos Aires, San } \\
\text { Martin } \\
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## 을 을 을 <br> 


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|  | " | 152,40 | 45,36 | 585,22 | 15,00 | CP | 3,44 | 2,00 | 4.57 | Cast Iron | 4,74\% | BP | 7700 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | " | 152,40 | 45,36 | 585,22 | 15,00 | AP | 2,88 | 2,00 | 4.57 | Steel | 1,25\% | BP | 7700 |  |
| Armstrong | 6"/40 Pattern | 152,40 | 45,36 | 670,30 | 15,00 | AP | 3,27 | 2,00 | 4.57 | Steel | 4,87\% | BP | 8737 | Nueve de Julio |
|  | " | 152,40 | 45,36 | 670,30 | 15,00 | AP | 2,88 | 2,00 | 4.57 | Steel | 1,25\% | BP | 8737 |  |
|  | " | 152,40 | 45,36 | 670,30 | 15,00 | CP | 3,44 | 2,00 | 4.57 | Cast Iron | 4,75\% | BP | 8737 |  |
|  | " | 152,40 | 45,36 | 670,30 | 15,00 | Common | 3,61 | 2,00 | 4.57 | Cast Steel | 9,81\% | BP | 8737 |  |
| Armstrong | 6"/45 Pattern | 152,40 | 45,36 | 792,48 | 15,00 | AP | 3,27 | 2,00 | 4.57 | Steel | 4,87\% | BP | 10198 | Buenos Aires, Garibaldi class |
|  | " | 152,40 | 45,36 | 792,48 | 15,00 | CP | 3,44 | 2,00 | 4.57 | Cast Iron | 4,75\% | BP | 10198 |  |
|  | " | 152,40 | 45,36 | 792,48 | 15,00 | Common | 3,61 | 2,00 | 4.57 | Cast Steel | 9,81\% | BP | 10198 |  |
|  | " | 152,40 | 45,36 | 792,48 | 15,00 | AP | 2,88 | 2,00 | 4.57 | Steel | 1,25\% | BP | 10198 |  |
| Bethlehem | 6"/50 | 152,40 | 47,63 | 853,44 | 15,00 | APCBC | 4,00 | 7,00 | 3.8 |  |  |  | 15498 | Rivadavia |
| Vickers | 6"/50 Mk. W | 152,40 | 45,36 | 900,00 | 45,00 | CPC |  | 6,00 | 5.3 |  |  |  | 23500 | Almirante Brown (rearmed) |
| Canet | 150mm/50 M. 1896 | 150,00 | 40,00 | 800,00 | 15,00 | AP | 2,70 | 2,00 | 4.57 |  |  |  | 10175 |  |
|  | " | 150,00 | 39,40 | 806,00 | 15,00 | CP | 3,30 | 2,00 | 4.57 |  |  |  | 10112 |  |
| Armstrong | 4.7"/23.5 BLR Pattern | 120,00 | 23,60 | 485,00 | 12,00 | SAP | 3,15 | 2,00 | 4.57 | Palliser | 4,45\% | BP | 5358 | Almirante Brown (rearmed) |
|  | " | 120,00 | 16,70 | 487,00 | 12,00 | Common | 2,96 | 2,00 | 4.57 |  | 5,99\% | BP | 4810 |  |
| Krupp | $12 \mathrm{~cm} \mathrm{SKL/40} \mathrm{C/88}$ | 120,00 | 23,80 | 680,00 | 30,00 | AP | 3,20 | 2,00 | 3.9 |  | 2,10\% | PA | 11400 | Veinticinco de Mayo |
|  | " | 120,00 | 23,80 | 680,00 | 30,00 | CP | 3,86 | 2,00 | 3.9 |  | 5,46\% | PA | 11400 |  |
| Canet | 120mm/50 M. 1896 | 120,00 | 22,00 | 840,00 | 15,00 | AP | 2,90 | 2,00 | 4.57 |  |  |  | 9633 | Almirante Brown (rearmed) |
|  | " | 120,00 | 22,00 | 840,00 | 15,00 | CP | 3,60 | 2,00 | 4.57 |  |  |  | 9633 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  | Independencia, Nueve de Julio, Garibaldi class, |
| EOC | 4.7"/40 Pattern P | 120,00 | 20,41 | 544,37 | 15,00 | AP | 3,02 | 2,00 | 4.57 | Steel Cast Iron | 4,44\% | BP | 6469 | Patria |
|  | " | 120,00 | 20,41 | 544,37 | 15,00 | AP | 3,02 | 2,00 | 4.57 | Palliser | 2,08\% | BP | 6469 |  |
|  | " | 120,00 | 20,41 | 544,37 | 15,00 | CP | 3,63 | 2,00 | 4.57 | Cast Steel | 10,00\% | BP | 6469 |  |
|  | " | 120,00 | 20,41 | 647,70 | 15,00 | AP | 3,02 | 2,00 | 4.57 | SteelCast Iron Palliser | 4,44\% | BP | 7465 |  |
|  | " | 120,00 | 20,41 | 647,70 | 15,00 | AP | 3,02 | 2,00 | 4.57 |  | 2,08\% | BP | 7465 |  |
|  | " | 120,00 | 20,41 | 647,70 | 15,00 | CP | 3,63 | 2,00 | 4.57 | Cast Steel | 10,00\% | BP | 7465 |  |
| EOC | 4.7"/45 Pattern $Y$ | 120,00 | 20,41 | 783,34 | 20,00 | AP | 3,02 | 2,00 | 4,11 | Steel Cast Iron Palliser | 4,44\% | BP | 9974 | Buenos Aires |
|  | " | 120,00 | 20,41 | 783,34 | 20,00 | AP | 3,02 | 2,00 | 4,11 |  | 2,08\% | BP | 9974 |  |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|c|c|}
\hline 120,00 \& 20,41 \& 783,34 \& 20,00 \& CP \& 3,63 \& 2,00 \& 4,11 \& Cast Steel \& \& 10,00\% \& BP \& 9974 \& <br>
\hline 120,00
101,60 \& 22,00
15,00 \& 850,00
853,44 \& 35,00

20,00 \& CPC
APC \& 3,70
3,40 \& 4,00
4,00 \& 4.0
7.6 \& \& \& \& \& 16689
12887 \& Mendoza, Corrientes Rivadavia, Catamarca, La Plata, San Luis, Mendoza <br>
\hline 101,60 \& 15,00 \& 853,44 \& 20,00 \& SAP \& 3,80 \& 4,00 \& 7.6 \& \& \& \& \& \& <br>
\hline 101,60 \& 15,00 \& 853,44 \& 20,00 \& CP \& 4,00 \& 2,00 \& 7.6 \& \& \& \& \& 10907 \& <br>
\hline 101,60 \& 14,06 \& 914,40 \& 90,00 \& CP \& 3,80 \& 6,00 \& 8.3 \& \& \& \& \& 18200 \& La Argentina <br>
\hline 101,60 \& 13,75 \& 875,00 \& 85,00 \& CP \& \& 3,00 \& 7.5 \& \& \& \& \& 14611 \& Almirante Brown <br>
\hline 76,20 \& 5,67 \& 673,61 \& 20,00 \& CP \& 3,72 \& 2,00 \& 2.59 \& \& \& 9,15\% \& BP \& 7245 \& <br>
\hline 381,00 \& 884,97 \& 762,00 \& 20,00 \& APC \& 3,94 \& 4,00 \& 7.62 \& \& 8,13\% \& 2,03\% \& T \& 22970 \& Riachuelo (Plan) <br>
\hline 381,00 \& 884,97 \& 762,00 \& 20,00 \& CPC \& 4,94 \& 4,00 \& 7.62 \& \& \& \& \& 22970 \& <br>
\hline 355,60 \& 635,04 \& 800,10 \& 20,00 \& APC \& 3,30 \& 3,00 \& 6.84 \& \& \& \& \& 21498 \& Rio de Janeiro (Plan) <br>
\hline 355,60 \& 635,04 \& 800,10 \& 20,00 \& CPC \& \& 3,00 \& 6.84 \& \& \& \& \& 21498 \& <br>
\hline 305,00 \& 445,00 \& 865,00 \& 12,00 \& APC \& \& 3,00 \& 8,0 \& 1908 \& \& \& \& 19000 \& Coast Defence <br>
\hline 305,00 \& 445,00 \& 865,00 \& 12,00 \& CP \& \& 3,00 \& 8,0 \& 1908 \& \& \& \& 19000 \& <br>
\hline 304,80 \& 317,52 \& 492,05 \& 14,00 \& AP \& 2,64 \& 2,00 \& 5.11 \& Palliser \& \& \& \& 7365 \& Independencia <br>
\hline 304,80 \& 278,96 \& 524,04 \& 14,00 \& Common \& 2,70 \& 2,00 \& 5.11 \& \& \& 6,50\% \& BP \& 7617 \& <br>
\hline 304,80 \& 385,56 \& 853,44 \& 18,00 \& APC \& 3,30 \& 2,00 \& 6.55 \& \& 3,33\% \& \& \& 18022 \& Minas Gerais <br>
\hline 304,80 \& 385,56 \& 853,44 \& 18,00 \& AP \& 3,16 \& 2,00 \& 6.55 \& \& \& \& \& 18109 \& <br>
\hline 304,80 \& 385,56 \& 822,96 \& 13,50 \& APC \& 3,30 \& 4,00 \& 7.54 \& \& \& \& \& 17035 \& Rio de Janeiro <br>
\hline 304,80 \& 385,56 \& 822,96 \& 13,50 \& CPC \& 3,90 \& 4,00 \& 7.54 \& \& \& \& \& 17035 \& <br>
\hline 254,00 \& 334,75 \& 373,38 \& 14,00 \& AP \& 3,36 \& 5,00 \& 3,0 \& \& \& 4,74\% \& BP \& 6954 \& Javary <br>
\hline 254,00 \& 199,13 \& 464,21 \& 14,00 \& Common \& 3,47 \& 5,00 \& 3,0 \& \& \& 5,47\% \& BP \& 9326 \& <br>
\hline 233,68 \& 172,37 \& 640,08 \& 15,00 \& AP \& 3,12 \& 2,00 \& 4.72 \& \& \& \& \& 10301 \& Riachuelo <br>
\hline 233,68 \& 172,37 \& 640,08 \& 15,00 \& CP \& 4,11 \& 2,00 \& 4.72 \& \& \& 8,68\% \& BP \& 10301 \& <br>
\hline 233,68 \& 172,37 \& 629,41 \& 15,00 \& AP \& 3,12 \& 2,00 \& 4.72 \& \& \& \& \& 10106 \& Aquidaban <br>
\hline 233,68 \& 172,37 \& 629,41 \& 15,00 \& CP \& 3,80 \& 2,00 \& 4.72 \& \& \& 8,68\% \& BP \& 10106 \& <br>
\hline
\end{tabular}

| Whitworth | 9" 14.7-Ton MLR | 228,60 | 243,13 | 347,17 | 10,00 | AP | 3,34 | 5,00 | 3,0 |  |  | 4,66\% | BP | 3906 | Sete de Setembro |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | " | 228,60 | 145,15 | 430,99 | 10,00 | Common | 3,47 | 5,00 | 3,0 |  |  | 5,63\% | BP | 5033 |  |
| Whitworth | 8" MLR | 203,20 |  |  |  |  |  |  |  |  |  |  |  |  | Independencia Barrozo, Brasi;, Lima Barros, Bahia, Mariz e |
| Whitworth | 7"L/17.5 7.5-Ton MLR | 177,80 | 68,04 | 363,93 | 10,00 | Common | 3,46 | 5,00 | 3,0 |  |  | 7,07\% | BP | 3863 | Barros |
|  | " | 177,80 | 86,18 | 380,70 | 10,00 | AP Shell | 2,52 | 5,00 | 3,0 |  |  |  |  | 4204 |  |
|  | " | 177,80 | 68,40 | 427,33 | 10,00 | Shot | 2,58 | 5,00 | 3,0 |  |  |  |  | 4735 |  |
| Whitworth | 120-pdr L/22.5 MLR | 162,56 | 49,90 | 423,37 | 10,00 | Common | 3,32 | 5,00 | 3,0 |  |  |  |  | 4556 |  |
|  | " | 162,56 | 68,49 | 379,78 | 10,00 | AP Shell | 2,62 | 5,00 | 3,0 |  |  |  |  | 4165 |  |
|  | " | 162,56 | 53,30 | 430,38 | 10,00 | Shot | 2,63 | 5,00 | 3,0 |  |  |  |  | 4714 |  |
| Armstrong | 6"/32 Pattern M | 152,40 | 45,36 | 597,41 | 15,00 | AP | 3,27 | 2,00 | 4.57 | Steel |  | 4,87\% | BP | 7850 | Almirante Tamandare, Benjamin Constant |
|  | " | 152,40 | 45,36 | 597,41 | 15,00 | AP | 2,88 | 2,00 | 4.57 | Steel |  | 1,25\% | BP | 7850 |  |
|  | " | 152,40 | 45,36 | 597,41 | 15,00 | CP | 3,44 | 2,00 | 4.57 | Cast Iron |  | 4,75\% | BP | 7850 |  |
|  | " | 152,40 | 45,36 | 597,41 | 15,00 | Common | 3,61 | 2,00 | 4.57 | Cast Steel |  | 9,81\% | BP | 7850 |  |
| EOC | 6"/50 Pattern DD | 152,40 | 45,36 | 792,48 | 20,00 | AP | 3,27 | 2,00 | 4.57 | Steel |  | 4,87\% | BP | 11688 | Barrozo |
|  | " | 152,40 | 45,36 | 792,48 | 20,00 | CP | 3,44 | 2,00 | 4.57 | Cast Iron |  | 4,75\% | BP | 11688 |  |
|  | " | 152,40 | 45,36 | 792,48 | 20,00 | Common | 3,61 | 2,00 | 4.57 | Cast Steel |  | 9,81\% | BP | 11688 |  |
|  | " | 152,40 | 45,36 | 792,48 | 20,00 | AP | 2,88 | 2,00 | 4.57 | Steel |  | 1,25\% | BP | 11688 |  |
| EOC | 6"/50 Pattern | 152,40 | 45,36 | 844,30 | 15,00 | APC |  | 3,00 | 6.09 |  |  |  |  | 12321 | Rio de Janerio, Riachuelo |
|  | " | 152,40 | 45,36 | 844,30 | 15,00 | CPC |  | 3,00 | 6.09 |  |  | 8,66\% | BP | 12321 |  |
| Vickers | 6"/50 Mk. S | 152,40 | 45,36 | 883,92 | 15,00 | APC |  | 3,00 | 3.05 |  |  |  |  | 12920 | Javary |
|  | " | 152,40 | 45,36 | 883,92 | 15,00 | CPC |  | 3,00 | 3.05 |  |  | 7,50\% | BP | 12920 |  |
| Armstrong | 5.5"/ Pattern | 139,70 |  |  |  |  |  | 2,00 | 4.72 |  |  |  |  |  | Riachuelo, Aquidaban Tamandare, |
| Whitworth | 70-pdr L/23.6 MLR | 127,00 | 22,79 | 405,23 | 10,00 | Common | 3,18 | 5,00 | 3,0 |  |  |  |  | 4075 | Silvado, Cabral |
|  | " | 127,00 | 36,74 | 332,84 | 10,00 | AP Shell | 2,95 | 5,00 | 3,0 |  |  |  |  | 3491 |  |
|  | " | 127,00 | 22,29 | 422,48 | 10,00 | Shot | 2,31 | 5,00 | 3,0 |  |  |  |  | 4240 |  |
|  | " | 127,00 | 31,75 | 358,14 | 10,00 | Shot | 3,29 | 5,00 | 3,0 |  |  |  |  | 3750 |  |
| Bethlehem | 5"/38 Mk. 12 | 127,00 | 25,03 | 790,96 | 85,00 | SAPC | 4,15 | 5,25 | 4.42 | Mk. 38 S C | 14,00\% | 3,70\% | D | 16474 | Marcilio Dias, Acre |
|  | " | 127,00 | 24,49 | 800,10 | 85,00 | CPBC |  |  | 4.42 | Mk. 32 S C | 8,00\% | 4,60\% | D | 16507 |  |
|  | " | 127,00 | 22,68 | 830,58 | 85,00 | APC | 3,30 | 4,00 | 4.42 |  |  |  |  | 15995 |  |


| Armstrong | 40-pdr 1.32-Ton BLR <br> (/22) | 120,65 | 18,37 | 480,06 | 12,00 | CP | 3,25 | 2,00 | 2.44 |  | 5,86\% | BP | 4799 | Almirante Barrozo |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Armstrong | 4.7"/32 Pattern M | 120,00 | 16,33 | 590,50 | 15,00 | CP | 2,88 | 2,00 | 4.57 |  |  |  | 6208 | Almirante Tamandare, Benjamin Constant |
| Armstrong | 4.7"/40 Pattern P | 120,00 | 20,41 | 544,37 | 20,00 | AP | 3,02 | 2,00 | 4.57 | Steel Cast Iron Palliser | 4,44\% | BP | 7694 | Republica, Tiradentes |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | " | 120,00 | 20,41 | 544,37 | 20,00 | AP | 3,02 | 2,00 | 4.57 |  | 2,08\% | BP | 7694 |  |
|  | " | 120,00 | 20,41 | 544,38 | 20,00 | CP | 3,63 | 2,00 | 4.57 | Steel | 10,00\% | BP | 7694 |  |
|  | " | 120,00 | 20,41 | 647,70 | 20,00 | AP | 3,02 | 2,00 | 4.57 | Steel Cast Iron Palliser | 4,44\% | BP | 8773 |  |
|  | " | 120,00 | 20,41 | 647,70 | 20,00 | AP | 3,02 | 2,00 | 4.57 |  | 2,08\% | BP | 8773 |  |
|  | " | 120,00 | 20,41 | 647,70 | 20,00 | CP | 3,63 | 2,00 | 4.57 | Steel | 10,00\% | BP | 8773 |  |
| EOC | 4.7"/50 Pattern AA | 120,00 | 20,41 | 801,63 | 15,00 | AP | 3,02 | 2,00 | 4.57 | Steel Cast Iron Palliser | 4,44\% | BP | 10315 | Barrozo |
|  | " | 120,00 | 20,41 | 801,63 | 15,00 | AP | 3,02 | 2,00 | 4.57 |  | 2,08\% | BP | 10315 |  |
|  | " | 120,00 | 20,41 | 801,63 | 15,00 | CP | 3,63 | 2,00 | 4.57 | Steel | 10,00\% | BP | 10315 |  |
| EOC | 4.7"/50 Pattern CC | 120,00 | 20,41 | 914,40 | 15,00 | AP | 3,02 | 2,00 | 4.57 |  | 4,44\% | BP | 10055 | Minas Gerais, Bahia |
|  | " | 120,00 | 20,41 | 914,40 | 15,00 | CP | 3,63 | 2,00 | 4.57 |  | 10,00\% | BP | 10055 |  |
| Vickers | 4"/40 Mk. M | 101,60 | 14,06 | 676,66 | 30,00 | CPC | 3,80 | 3,00 | 4.0 |  |  |  | 11162 | Para class |
| Vickers | 4"/45 Mk. N | 101,60 | 14,06 | 853,44 | 40,00 | CPC | 3,80 | 3,00 | 4.0 |  |  |  | 14545 | Carioca |
| Whitworth | 32-pdr L/24 MLR | 91,44 | 9,07 | 356,01 | 10,00 | Common | 3,39 | 5,00 | 3,0 |  |  |  | 3391 | Barrozo |
|  |  | 91,44 | 11,79 | 325,53 | 10,00 | Shot | 3,29 | 5,00 | 3,0 |  |  |  | 3185 |  |
| Armstrong | 3.5"/40 Pattern | 88,90 | 9,07 | 594,36 | 20,00 | CP | 2,98 | 2,00 | 2.66 |  |  |  | 7270 | Sampaio |
|  | 12-pdr ${ }^{\text {" }}$ " 3 " 140 | 88,90 | 9,07 | 737,62 | 20,00 | CP | 3,73 | 2,00 | 2.66 |  |  |  | 8400 |  |
| EOC | $\begin{aligned} & \text { 12-pdr QF (3"/40 } \\ & \text { Pattern N) } \end{aligned}$ | 76,20 | 5,67 | 673,61 | 20,00 | CP | 3,72 | 2,00 | 2.59 |  |  |  | 7353 |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | CHILE |  |  |  |  |  |  |  |  |  |  |  |  |  |
| EOC | 14"/45 Pattern A | 355,60 | 719,40 | 754,38 | 20,00 | APC |  | 4,00 | 7.32 | Mk. la | 3,87\% | L | 21891 | Almirante Latorre |
|  | " | 355,60 | 719,40 | 754,38 | 20,00 | CPC |  | 4,00 | 7.32 |  | 6,57\% | BP | 21891 |  |
|  | " | 355,60 | 719,40 | 754,38 | 20,00 | CPC |  | 4,00 | 7.32 |  | 6,64\% | BP | 21900 |  |
|  | " ${ }^{\text {" }}$ | 355,60 | 723,49 | 754,38 | 20,00 | APC |  | 4,00 | 7,32 | Mk. IIIa | 2,35\% | S | 21900 |  |
|  | 10"/26 25-Ton BLR Pattern | 254,00 |  | 579,12 |  |  | 2,88 | 2,00 | 4.57 | Palliser | 1,58\% | BP | 7230 |  |
| Armstrong | Patter | 254,00 | 181,44 | 614,17 | 10,00 | Common | 2,88 3,57 | 2,00 2,00 | 4.57 |  |  |  | 7480 | Arturo Prat |


| Armstrong | $10^{\prime \prime} / 30$ Patterns F \& G | 254,00 | 204,11 | 627,89 | 12,00 | AP | 2,88 | 2,00 | 4.11 | Palliser | 1,58\% | BP | 8975 | Esmeralda |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | " | 254,00 | 181,44 | 665,84 | 12,00 | Common | 3,57 | 2,00 | 4.11 |  |  |  | 9186 |  |
|  | (cordite) | 254,00 | 204,11 | 624,84 | 12,00 | AP | 2,88 | 2,00 | 4.11 | Palliser | 1,58\% | BP | 8921 |  |
| EOC \& VSM | 10"/45 Pattern S \& Mk. A | 254,00 | 226,80 | 792,48 | 13,50 | AP | 3,21 | 2,00 | 7.39 |  |  |  | 13196 | Constitucion |
|  | " | 254,00 | 226,80 | 792,48 | 13,50 | CP | 3,90 | 2,00 | 7.39 |  | 7,55\% | BP | 13196 |  |
| Canet | $240 \mathrm{~mm} / 36 \mathrm{M} .1887$ | 240,00 | 144,00 | 760,00 | 12,00 | AP | 2,40 | 2,00 | 5.4 |  |  |  | 10112 | Capitan Prat |
|  | " | 240,00 | 144,00 | 760,00 | 12,00 | CP | 2,90 | 2,00 | 5.4 |  |  |  | 10079 |  |
|  | " | 240,00 | 170,00 | 760,00 | 12,00 | APC | 2,70 | 2,00 | 5.4 |  | 1,41\% | M | 10388 |  |
|  | " | 240,00 | 170,00 | 760,00 | 12,00 | CPC | 3,00 | 2,00 | 5.4 |  | 6,65\% | M | 10368 |  |
| Armstrong | 9"/15.3 12-Ton MLR | 228,60 | 116,12 | 432,82 | 10,00 | AP | 2,28 | 2,00 | 2.0 | Palliser |  |  | 4785 | Almirante Cochrane |
|  | 8"/30 13.5-Ton BLR | 228,60 | 113,40 | 432,64 | 10,00 | Common | 2,60 | 2,00 | 2.0 |  | 7,40\% | BP | 4759 |  |
| Armstrong | Pattern L | 203,20 | 95,26 | 670,56 | 7,50 | AP | 2,62 | 2,00 | 2.74 |  |  |  | 6384 | Almirante Cochrane (re- armed) |
|  | " | 203,20 | 95,26 | 670,56 | 7,50 | Common | 3,31 | 2,00 | 2.74 |  |  |  | 6384 |  |
| Armstrong | 8"/25.6 Pattern E | 203,20 | 95,26 | 621,30 | 11,00 | AP | 2,62 | 2,00 | 2.74 |  |  |  | 7315 | re-armed Huascar |
|  | " | 203,20 | 95,26 | 621,30 | 11,00 | Common | 3,31 | 2,00 | 2.74 |  |  |  | 7315 |  |
| Armstrong | 8"/39.9 Pattern P | 203,20 | 95,26 | 744,32 | 15,00 | AP | 3,57 | 2,00 | 5.18 |  |  |  | 10473 | Blanco Encalada, Esmeralda |
|  | " | 203,20 | 95,26 | 744,32 | 15,00 | Common | 3,45 | 2,00 | 5.18 |  |  |  | 10473 |  |
|  | " | 203,20 | 113,40 | 612,04 | 15,00 | AP | 3,00 | 2,00 | 5.18 |  | 0,90\% | BP | 9273 |  |
|  | (cordite) | 203,20 | 95,26 | 783,34 | 15,00 | AP | 3,57 | 2,00 | 5.18 |  |  |  | 11013 |  |
|  | " | 203,20 | 95,26 | 783,34 | 15,00 | Common | 3,45 | 2,00 | 5.18 |  |  |  | 11013 |  |
|  | " | 203,20 | 113,40 | 722,07 | 15,00 | AP | 3,00 | 2,00 | 5.18 |  | 0,90\% | BP | 11071 |  |
| Armstrong | 8"/45 Pattern S | 203,20 | 95,26 | 858,62 | 15,00 | AP | 3,57 | 2,00 | 5.18 |  |  |  | 12044 | Chacabuco |
|  | " | 203,20 | 113,40 | 787,00 | 15,00 | AP | 3,00 | 2,00 | 5.18 |  | 0,90\% | BP | 12128 |  |
| Armstrong | 8"/45 Pattern T | 203,20 | 95,26 | 784,86 | 15,00 | AP | 3,57 | 2,00 | 6.8 |  |  |  | 11038 | O'Higgins |
|  | " | 203,20 | 95,26 | 784,86 | 15,00 | CP | 3,45 | 2,00 | 6.8 |  |  |  | 11038 |  |
|  | 促 | 203,20 | 113,40 | 743,71 | 15,00 | AP | 3,00 | 2,00 | 6.8 |  | 0,90\% | BP | 11429 |  |
| EOC \& VSM | 7.5"/50 Pattern A \& Mk. B | 190,50 | 90,72 | 822,63 | 15,00 | Shot | 2,90 | 2,00 | 4.11 |  |  |  | 12734 | Constitucion |
|  | " | 190,50 | 90,72 | 822,63 | 15,00 | AP | 3,70 | 2,00 | 4.11 |  | 4,37\% | BP | 12734 |  |
|  | " | 190,50 | 90,72 | 822,63 | 15,00 | APC | 2,90 | 2,00 | 4.11 |  | 4,37\% | BP | 12734 |  |
|  | " | 190,50 | 90,72 | 822,63 | 15,00 | CP | 3,70 | 2,00 | 4.11 |  | 8,25\% | BP | 12734 |  |


| Armstrong | RBL 70-pdr 69cwt | 162,60 | 32,52 | 424,70 | 15,00 | Bolt | 1,50 | 2,00 | 3.51 |  |  |  | 4805 | Abtao |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | " | 162,60 | 36,29 | 424,10 | 15,00 | AP | 1,98 | 2,00 | 3.51 | Palliser |  |  | 5070 |  |
|  | " | 162,60 | 31,80 | 453,10 | 15,00 | Common | 2,30 | 2,00 | 3.51 |  |  |  | 5025 |  |
| Armstrong | 6"/26.1 BLR 4-Ton Pattern B | 2,40 | 36,29 | 587,9 | 12,00 | AP | 2,32 | 2,00 | 4.57 | Palliser | 2,12 |  |  |  |
|  | " | 152,40 | 36,29 | 519,00 | 12,00 | Common | 2,53 | 2,00 | 4.57 |  | 6,25\% | BP | 5591 | Arturo Prat |
| Armstrong | 6"/30 Pattern I | 152,40 | 36,29 | 637,03 | 13,00 | Common | 3,12 | 2,00 | 4.57 |  | 6,25\% | BP | 6981 | Esmeralda |
|  | (cordite) | 152,40 | 36,29 | 697,99 | 13,00 | Common | 3,12 | 2,00 | 4.57 |  | 6,25\% | BP | 7570 |  |
| Armstrong | 6"/40 Patterns W \& Z | 152,40 | 45,36 | 762,00 | 15,00 | AP | 3,27 | 2,00 | 4.57 | Steel | 4,87\% | BP | 9838 | Blanco Encalada, O'Higgins, Esmeralda |
|  | " | 152,40 | 45,36 | 762,00 | 15,00 | CP | 3,44 | 2,00 | 4.57 | Cast Iron | 4,75\% | BP | 9838 |  |
|  | " | 152,40 | 45,36 | 762,00 | 15,00 | Common | 3,61 | 2,00 | 4.57 | Cast Steel | 9,81\% | BP | 9838 |  |
|  | " | 152,40 | 45,36 | 762,00 | 15,00 | AP | 2,88 | 2,00 | 4.57 | Steel | 1,25\% | BP | 9838 |  |
| Armstrong | 6"/50 Pattern DD | 152,40 | 45,36 | 792,48 | 20,00 | AP | 3,27 | 2,00 | 4.57 | Steel | 4,87\% | BP | 11688 | Ministro Zenteno |
|  | " | 152,40 | 45,36 | 792,48 | 20,00 | CP | 3,44 | 2,00 | 4.57 | Cast Iron | 4,75\% | BP | 11688 |  |
|  | " | 152,40 | 45,36 | 792,48 | 20,00 | Common | 3,61 | 2,00 | 4.57 | Cast Steel | 9,81\% | BP | 11688 |  |
|  | " | 152,40 | 45,36 | 792,48 | 20,00 | AP | 2,88 | 2,00 | 4.57 | Steel | 1,25\% | BP | 11688 |  |
| EOC | 6"/50 Pattern TT | 152,40 | 45,36 | 883,92 | 15,00 | CPC | 3,92 | 3,00 | 4,27 |  | 8,66\% | BP | 12924 | Almirante Latorre |
| Canet | 150mm/36 M. 1884 RBL 40-pdr 35cwt | 150,00 | 40,00 | 770,00 | 15,00 | AP | 3,00 | 2,00 | 5.75 |  |  |  | 9830 | Presidente Errazuriz |
| Armstrong | (/22.4) | 120,65 | 18,60 | 354,79 | 15,00 | Bolt | 2,17 | 2,00 | 2.59 |  |  |  | 4498 | Abtao |
|  | " | 120,65 | 20,40 | 338,60 | 15,00 | AP | 2,68 | 2,00 | 2.59 | Palliser |  |  | 42154344 |  |
|  | " | 120,65 | 18,37 | 359,66 | 15,00 | Common | 2,92 | 2,00 | 2.59 |  | 6,17\% | BP |  |  |
| Armstrong | 40-pdr MLR (/16) | 120,65 | 18,37 | 491,95 | 12,00 | Common | 2,87 | 2,00 | 2.5 |  | 8,18\% | BP | 4799 | Almirante Cochrane re-armed Huascar |
| Armstrong | 40-pdr 1.32-Ton BLR | 120,65 | 18,37 | 480,06 | 12,00 | Common | 3,25 | 2,00 | 2.44 |  |  |  | 4753 |  |
| Canet | 120mm/36 M. 1884 | 120,00 | 22,00 | 715,00 | 15,00 | AP | 3,00 | 2,00 | 5.75 |  |  |  | 8413 | Presidente Errazuriz |
|  |  | 120,00 | 22,00 | 715,00 | 15,00 | CP | 3,60 | 2,00 | 5.75 |  |  |  | 8332 |  |
| Canet | 120mm/45 M. 1887 | 120,00 | 22,00 | 850,00 | 15,00 | AP | 3,00 | 2,00 | 3.6 |  |  |  | 9726 | Capitan Prat |
|  | " | 120,00 | 22,00 | 850,00 | 15,00 | CP | 3,60 | 2,00 | 3.6 |  |  |  | 9621 |  |
|  |  |  |  |  |  |  |  |  |  | Steel Cast Iron Palliser |  |  |  | Chacabuco, Almirante Simpson |
| Armstrong | 4.7/40 Pattern P | 120,00 | 20,41 | 655,32 | 15,00 | AP | 3,02 | 2,00 | 4.57 |  | 4,44\% | BP | 7638 |  |
|  | " | 120,00 | 20,41 | 655,32 | 15,00 | AP | 3,02 | 2,00 | 4.57 |  | 2,08\% | BP | 7638 |  |
|  | " | 120,00 | 20,41 | 655,32 | 15,00 | CP | 3,63 | 2,00 | 4.57 | Steel | 10,00\% | BP | 7638 |  |


| Armstrong | 4.7"/43.9 Pattern $Y$ | 120,00 | 20,41 | 783,34 | 15,00 | AP | 3,02 | 2,00 | 4,11 | Steel Cast Iron | 4,44\% | BP | 8860 | O'Higgins |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 120,00 | 20,41 | 783,34 | 15,00 | AP | 3,02 | 2,00 | 4,11 | Palliser | 2,08\% | BP | 8860 |  |
|  |  | 120,00 | 20,41 | 783,34 | 15,00 | CP | 3,63 | 2,00 | 4,11 | Steel | 10,00\% | BP | 8860 |  |
| Vickers | 4.7"/45 Mk. E | 120,00 | 22,00 | 810,00 | 35,00 | CPC | 3,70 | 4,00 | 3.8 |  |  |  | 14877 | Serrano |
| EOC | 4:/40 Pattern S <br> 12-pdr QF Pattern N | 101,60 | 14,06 | 701,04 | 25,00 | CP |  | 3,00 | 3.66 |  |  |  | 10635 | Almirante Lynch |
| Armstrong | (3"/40) | 76,20 | 5,67 | 673,61 | 20,00 | CP | 3,72 | 2,00 | 2.59 |  | 9,15\% | BP | 7245 |  |
|  | CHINA |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Armstrong | 12.5"/16 38-Ton MLR | 317,50 | 362,88 | 412,09 | 12,00 | AP | 2,66 | 2,00 | 4.57 |  |  |  | 5331 | Fei Ting |
|  | " | 317,50 | 362,88 | 412,09 | 12,00 | Common | 3,11 | 2,00 | 4.57 |  |  |  | 5324 |  |
| Krupp | 30.5 cm RKL/25 C/80 | 305,00 | 329,00 | 500,00 | 13,00 | AP | 2,70 | 2,00 | 5.5 |  | 1,06\% | BP | 7250 | Ting Yuen |
|  | " | 305,00 | 329,00 | 500,00 | 13,00 | Common | 2,50 | 2,00 | 5.5 |  | 5,47\% | BP | 7250 |  |
| Vavasseur | 12-in MLR |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Armstrong | 11"/12 25-Ton MLR | 279,40 | 241,77 | 400,65 | 12,00 | AP | 2,61 | 2,00 | 4.57 |  | 2,81\% | BP | 5001 | Hoi Tung Hung |
| Armstrong | 11"/13 26.5-Ton MLR | 279,40 | 241,77 | 426,72 | 12,00 | AP | 2,61 | 2,00 | 4.57 |  | 2,81\% | BP | 5001 | Lung Hsiang Chen Tung, Chen |
| Armstrong | 11"/23 35-Ton MLR | 279,40 | 241,99 | 552,83 | 12,00 | AP | 2,62 | 2,00 | 4.57 |  | 0,83\% | BP | 7425 | Chung |
|  | " | 279,40 | 242,99 | 551,69 | 12,00 | Com |  | 2,00 | 4.57 |  | 5,36\% | BP | 7417 |  |
| Krupp | 26 cm RKL/22 C/76 | 263,00 | 205,00 | 500,00 | 13,00 | AP | 3,50 | 2,00 | 3.5 |  | 1,95\% | BP | 6908 | Ping Yuen |
|  | " | 263,00 | 205,00 | 500,00 | 13,00 | Common | 3,20 | 2,00 | 3.5 |  | 5,61\% | BP | 6908 |  |
| Armstrong | 10"/15 18-Ton MLR | 254,00 | 181,44 | 415,58 | 12,00 | AP | 2,60 | 2,00 | 3.35 |  |  |  | 5114 | Chien Sheng |
|  | 20" ${ }^{\text {" }}$ | 254,00 | 180,53 | 416,66 | 12,00 | Common | 3,02 | 2,00 | 3.35 |  | 6,66\% | BP | 5117 |  |
| Armstrong | 10"/26 25-Ton BLR Pattern | 254,00 | 204,11 | 579,12 | 10,00 | AP | 2,56 | 2,00 | 4.57 |  | 1,58\% | BP | 7161 | Chao Yung |
|  | " | 254,00 | 181,44 | 588,61 | 10,00 | Common | 3,57 | 2,00 | 4.57 |  | 7,87\% | BP | 7021 |  |
| Krupp | $21 \mathrm{~cm} \mathrm{RKL/30} \mathrm{C/84}$ | 209,30 | 140,00 | 545,00 | 13,00 | AP | 3,53 | 2,00 | 5.2 |  | 1,79\% | BP | 7780 | Chih Yuan |
|  | " | 209,30 | 140,00 | 545,00 | 13,00 | Common | 4,28 | 2,00 | 5.2 |  | 3,93\% | BP | 7780 |  |
| Krupp | 21cm RKL/22 C/72 | 209,30 | 89,00 | 450,00 | 13,00 | AP | 2,48 | 2,00 | 2.5 | Gruson Chilled | 1,91\% | BP | 5480 | Chi Yuan, Kai Che, King Yuan, Nan Thin |
|  | " | 209,30 | 78,00 | 425,00 | 13,00 | Common | 2,41 | 2,00 | 2.5 |  | 8,72\% | BP | 5000 |  |
| EOC | 8"/45 Pattern S | 203,20 | 95,26 | 858,62 | 15,00 | AP | 3,57 | 2,00 | 5.18 |  |  |  | 11848 | Hai Tien |


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|  | $\begin{aligned} & \text { og } \\ & \stackrel{N}{n} \end{aligned}$ | $\begin{aligned} & \text { N } \\ & \\ & \end{aligned}$ | $\stackrel{\infty}{\underset{\sim}{\sim}}$ |  | $\begin{aligned} & \text { O } \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{N} \\ & \underset{\sim}{n} \end{aligned}$ | $\underset{\text { m }}{\ddagger}$ | $\underset{m}{\ddagger}$ | $\stackrel{N}{N}$ | $\begin{aligned} & \infty \\ & \infty \\ & \underset{\sim}{\infty} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { ले } \end{aligned}$ | $\underset{\sim}{N}$ | $\begin{aligned} & \infty \\ & \infty \\ & \sim \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { ल } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \underset{\sim}{2} \end{aligned}$ | $\begin{aligned} & \text { N } \\ & \text { ल゙ } \end{aligned}$ | $\stackrel{8}{\mathrm{O}}$ | $\begin{aligned} & \dot{\circ} \\ & \text { ल } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \underset{\sim}{2} \end{aligned}$ | $\stackrel{\infty}{\underset{\sim}{\infty}}$ | $\begin{aligned} & \dot{\infty} \\ & \text { ल゙ } \end{aligned}$ | $\begin{aligned} & \infty \\ & \stackrel{\infty}{0} \\ & \text { N } \end{aligned}$ | $\stackrel{\llcorner }{\stackrel{N}{N}}$ | $\begin{aligned} & \text { On } \\ & \text { ले } \end{aligned}$ | $\underset{\underset{\sim}{\mathrm{N}}}{\stackrel{-}{2}}$ |  |  |
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| $\begin{aligned} & 8 \\ & \stackrel{0}{0} \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { ò } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { ò } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \underset{\sim}{1} \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { - } \end{aligned}$ | $\begin{aligned} & 8 \\ & \hline-\mathrm{F} \end{aligned}$ | $\begin{aligned} & \circ \\ & 0 \\ & i \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{0}{5} \\ & \end{aligned}$ | $\begin{aligned} & \text { O } \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \text { O } \\ & \text { Ni } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { - } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { N- } \end{aligned}$ | 응 | $\begin{aligned} & \text { O- } \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { N- } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { ले } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \underset{\sim}{7} \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 \\ & \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{0}{n} \\ & \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { O- } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { - } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { O. } \\ & \text { O} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { Nָ } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { Nin } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { Nin } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { - } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { B- } \end{aligned}$ |
| $\begin{aligned} & \text { N } \\ & \text { ó } \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { Oi } \\ & \infty \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { Oig } \\ & \text { م } \end{aligned}$ | $\begin{aligned} & \infty \\ & \infty \\ & \underset{\sim}{\sim} \end{aligned}$ | $\begin{aligned} & \infty \\ & \stackrel{\infty}{\sim} \\ & \underset{\sim}{2} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \stackrel{0}{N} \\ & \stackrel{y}{n} \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { On } \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \mathscr{0} \\ & 0 \\ & \stackrel{N}{N} \\ & \stackrel{n}{2} \end{aligned}$ | $\begin{aligned} & \circ \\ & 0 \\ & \stackrel{0}{N} \\ & \stackrel{0}{n} \end{aligned}$ | $\begin{aligned} & \underset{寸}{-} \\ & \underset{-}{6} \end{aligned}$ | $\begin{aligned} & \circ \\ & \underset{\sim}{-} \end{aligned}$ | $\begin{aligned} & \text { o} \\ & \underset{-}{-} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & -\underset{-}{-1} \end{aligned}$ | $\begin{aligned} & \text { o} \\ & \text { নु } \end{aligned}$ | $\begin{aligned} & \stackrel{+}{-} \\ & \underset{-1}{\prime} \end{aligned}$ | $\begin{aligned} & \underset{\sim}{\circ} \\ & \underset{\sim}{2} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { O} \\ & \text { H} \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { O- } \\ & \text { ద్ర } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { N్․ } \\ & \text { On } \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { N్ర } \\ & \text { Non } \end{aligned}$ | $\begin{aligned} & \text { O. } \\ & \text { on } \\ & \infty \end{aligned}$ | $\begin{aligned} & \text { O } \\ & \text { D } \\ & \infty \end{aligned}$ | $\begin{aligned} & \text { O } \\ & \text { O } \\ & \text { م } \end{aligned}$ | $\circ$ <br> - <br> － | $\begin{aligned} & \text { Q } \\ & \text { O} \\ & \text { Nin } \end{aligned}$ | $\begin{aligned} & \text { B } \\ & \text { - } \\ & \text { దn } \end{aligned}$ | $\begin{aligned} & \text { O } \\ & 0 \\ & \text { Din } \end{aligned}$ | 8 |
| $\begin{aligned} & \text { N } \\ & \text { ஸ⿵ } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \stackrel{1}{N} \\ & \underset{\sim}{2} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { N్స } \\ & \end{aligned}$ | $\begin{aligned} & \infty \\ & \stackrel{\infty}{0} \end{aligned}$ | $\begin{aligned} & \infty \\ & \underset{N}{N} \\ & \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 . \\ & 0 \end{aligned}$ | $\begin{aligned} & 8 \\ & 0.7 \end{aligned}$ | $\begin{aligned} & 0 \\ & \mathrm{~N}^{-} \end{aligned}$ |  | $\begin{aligned} & \text { è } \\ & \text { Hi } \end{aligned}$ | $\begin{aligned} & 0 \\ & \mathrm{~N}^{-} \\ & \mathrm{O}^{2} \end{aligned}$ | $\begin{aligned} & \text { e } \\ & \text { ஸ } \end{aligned}$ | $\begin{aligned} & \circ \\ & \mathrm{N}^{-} \\ & \stackrel{7}{2} \end{aligned}$ | $\begin{aligned} & \circ \\ & \underset{\sim}{\circ} \\ & \stackrel{y}{\circ} \end{aligned}$ | $\begin{aligned} & \text { e } \\ & \text { if } \\ & \text { in } \end{aligned}$ | $\begin{aligned} & \tilde{6} \\ & \underset{\sim}{\circ} \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { in } \\ & \hline \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { in } \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { 가 } \end{aligned}$ | $\begin{aligned} & 8 \\ & -7 \\ & i \end{aligned}$ | $\begin{aligned} & 0 \\ & \text { م } \\ & \text { fin } \end{aligned}$ | $$ | $\begin{aligned} & \mathrm{O} \\ & \text { ò } \\ & \text { M } \end{aligned}$ | $\begin{aligned} & \underset{-}{J} \\ & \underset{\sim}{1} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \stackrel{\rightharpoonup}{\mathrm{~N}} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \mathbf{N} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{0}{N} \\ & \text { N } \end{aligned}$ | N－ |
| $\begin{aligned} & \text { N} \\ & \text { N} \\ & \text { N} \end{aligned}$ | $\begin{aligned} & \text { ৪i } \\ & \text { Ni } \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \text { N్ } \end{aligned}$ | $\begin{aligned} & \text { o } \\ & \stackrel{N}{N} \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{0}{N} \\ & \stackrel{N}{-} \end{aligned}$ | $\begin{aligned} & 8 \\ & \underset{N}{N} \\ & - \end{aligned}$ | $\begin{aligned} & \circ \\ & \stackrel{0}{N} \\ & \text { N } \end{aligned}$ | $\begin{aligned} & \circ \\ & \underset{N}{N} \\ & \stackrel{0}{1} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \underset{\sim}{\mathrm{O}} \end{aligned}$ | $\begin{aligned} & \circ \\ & \underset{\sim}{N} \\ & \stackrel{\sim}{1} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \underset{N}{N} \\ & \underset{\sim}{n} \end{aligned}$ | $\begin{aligned} & \circ \\ & \underset{\sim}{7} \\ & \stackrel{\sim}{n} \end{aligned}$ | $\begin{aligned} & \text { o } \\ & \text { N } \\ & \end{aligned}$ | $\begin{aligned} & \stackrel{+}{N} \\ & \stackrel{N}{n} \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \underset{\sim}{0} \\ & \stackrel{1}{2} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \underset{\sim}{N} \\ & \underset{\sim}{n} \end{aligned}$ | $\begin{aligned} & 0 \\ & \underset{-}{7} \\ & \underset{-1}{ } \end{aligned}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{-} \\ & \underset{\sim}{\underset{\sim}{7}} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \underset{\sim}{7} \\ & \underset{-}{\prime} \end{aligned}$ | $\begin{aligned} & 0 \\ & \underset{-}{-} \\ & \underset{-}{-} \end{aligned}$ | $\begin{aligned} & \mathrm{O} \\ & \underset{\sim}{-} \\ & \underset{\sim}{4} \end{aligned}$ | $\begin{aligned} & 0 \\ & \underset{-}{9} \\ & \underset{-1}{ } \end{aligned}$ | $\begin{aligned} & 8 \\ & 0 \\ & \text { O } \\ & \text { - } \end{aligned}$ | $\begin{aligned} & \text { ๗} \\ & \text { - } \\ & \text { N్ } \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { ̇ㅡ﹎ } \end{aligned}$ | $\begin{aligned} & \text { O} \\ & \text { - } \\ & \text { I- } \end{aligned}$ | $\begin{aligned} & 8 \\ & \text { 음 } \end{aligned}$ | O － ते |


| Skoda | $20.3 \mathrm{~cm} / 50 \mathrm{~K} / 16$ |
| :---: | :---: |
|  | ＂ |
| Armstrong | 7＂／15．9 MLR |
|  | ＂ |
| Krupp | 17cm RKL／25 C／74 |
|  | ＂ |
| Armstrong | 6＂／26．1 BLR |
|  | ＂ |
|  | 6＂／50 Patterns NN \＆ WW |
| EOC | ＂ |
|  | ＂ |
| Vickers | 6＂／50 Mk．M |
|  | ＂ |
| Bethlehem | 6＂／50 |
| Krupp | 15cm RKL／35 C／80 |
|  | ＂ |
| Krupp | 15cm SKL／40 C／92 |
|  | ＂ |
| Krupp | 15cm SKL／40 C／97 |
|  | ＂ |
|  | 50－cal Type 3 14－cm gun |
| Vavasseur | 5．5－in MLR <br> 40－pdr 1．32－Ton BLR |
| Armstrong | (I22) |
| Krupp | 12cm RKL／35 C／80 |
|  | ＂ |
| Krupp | 12cm SK L35 C／87 |
|  | ＂ |


| Krupp | $12 \mathrm{~cm} \mathrm{SKL/40} \mathrm{C/88}$ | 120,00 | 23,80 | 680,00 | 30,00 | AP | 3,20 | 2,00 | 3.9 |  | 2,10\% | PA | 11400 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | " | 120,00 | 23,80 | 680,00 | 30,00 | CP | 3,86 | 2,00 | 3.9 |  | 5,46\% | PA | 11400 |  |
| EOC | 4.7"/45 Pattern $Y$ | 120,00 | 20,41 | 783,34 | 20,00 | AP | 3,02 | 2,00 | 4.11 | Steel Cast Iron | 4,44\% | BP | 9974 |  |
|  | " | 120,00 | 20,41 | 783,34 | 20,00 | AP | 3,02 | 2,00 | 4.11 | Palliser | 2,08\% | BP | 9974 |  |
|  | " | 120,00 | 20,41 | 783,34 | 20,00 | CP | 3,63 | 2,00 | 4.11 | Steel | 10,00\% | BP | 9974 |  |
| Skoda | $12 \mathrm{~cm} / 45 \mathrm{~K} / 14$ | 120,00 | 23,80 | 800,00 | 30,00 | CPC | 4,20 | 4,00 | 5.1 |  | 8,82\% | T | 13564 | planned large cruiser |
| Blakely | 4.5-in MLR |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Krupp | $10.5 \mathrm{~cm} \mathrm{SKL} / 40 \mathrm{C} /$ | 105,00 | 17,40 | 840,00 | 30,00 | SAP |  | 3,00 | 4.4 |  |  |  | 13578 | Hai Yung, Fei Ying |
| Armstrong | 4"/14.8 BLR | 101,60 | 11,34 | 359,66 | 15,00 | Common |  | 2,00 |  |  | 11,50\% | BP | 4141 |  |
| Canet | $100 \mathrm{~mm} / 45 \mathrm{M} 1896$ | 100,00 | 13,00 | 765,00 | 15,00 | CP | 3,60 | 2,00 | 3.6 |  |  |  | 8398 | Chien An |
| Skoda | $10 \mathrm{~cm} / 50 \mathrm{~K} / 11$ <br> 25-pdr QF Pattern | 100,00 | 13,75 | 900,00 | 30,00 | CP | 4,20 | 4,00 | 3.9 | K/09 | 12,36\% | T | 14451 | planned Scouts |
| Armstrong | (3.75"/40) | 95,25 | 11,34 | 612,65 | 20,00 | AP | 3,03 | 2,00 | 2.66 |  |  |  | 7614 | Fei Ting |
|  | (cordite) | 95,25 | 11,34 | 722,38 | 20,00 | CP | 3,79 | 2,00 | 2.66 |  |  |  | 8300 |  |
| Armstrong | 12-pdr BLR ( $3^{\text {" } / 28) ~}$ <br> 40 -cal Type $38-\mathrm{cm}$ | 76,20 | 5,67 | 487,68 | 12,00 | Common | 3,65 | 2,00 | 4.57 |  | 4,76\% | BP | 4398 | Lung Hsiang, Chen Tung, Chen Chung |
|  | gun | 76,20 | 5,99 | 680,00 | 75,00 | CP |  | 4,00 | 7.0 |  | 7,58\% | SH | 10688 | Ning Hai |
| Krupp | 7.5 cm RK L/25 C/80 | 75,00 | 4,30 | 473,00 | 15,00 | Common |  | 2,00 |  |  | 4,65\% | BP | 4507 |  |
| Krupp | $7.5 \mathrm{~cm} \mathrm{SKL} 30 \mathrm{C} / 12$ | 75,00 | 5,85 | 605,00 | 30,00 | SAP | 3,70 | 4,00 | 3.5 | M. 1911 |  |  | 9300 | Chang Feng |
|  | GREECE |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Bethlehem | 14"/45 | 355,60 | 635,04 | 762,00 | 15,00 | APC | 3,53 | 4,00 | 7.6 |  |  |  | 18237 | Salamis |
| Canet | $340 \mathrm{~mm} / 45 \mathrm{M} 1912$ | 340,00 | 540,00 | 795,00 | 13,00 | APC | 3,18 | 2,00 | 6.2 | M. 1912 | 4,07\% |  | 15384 | Basileus Konstantinos |
| USN | 12"/45 Mk. 5 | 304,80 | 394,63 | 822,96 | 15,00 | APC | 3,40 | 4,00 | 5.94 |  |  |  | 18726 | Kilkis |
| Canet | 274mm/34 M1884 | 274,40 | 216,00 | 657,00 | 12,00 | AP | 2,40 | 2,00 | 9.3 |  |  |  | 9349 | Psara |
|  | " | 274,40 | 180,00 | 720,00 | 12,00 | Common | 2,40 | 2,00 | 9.3 |  |  |  | 9608 |  |
| Canet | 274mm/28 M1881 | 274,40 | 216,00 | 550,00 | 12,00 | AP | 2,40 | 2,00 | 6.5 |  |  |  | 7525 | Psara |
|  | " | 274,40 | 180,00 | 607,00 | 12,00 | Common | 2,40 | 2,00 | 6.5 |  |  |  | 7923 |  |
| Krupp | $26 \mathrm{~cm} \mathrm{RKL} / 30 \mathrm{C} / 84$ | 263,00 | 275,00 | 520,00 | 13,00 | AP | 3,50 | 2,00 | 2.5 |  |  |  | 7975 | Ambrakia |
|  | " | 263,00 | 205,00 | 602,00 | 13,00 | Common | 3,20 | 2,00 | 2.5 |  | 5,61\% | BP | 8770 |  |



|  |  | 18052 | Vasileos Georgios |
| :---: | :---: | :---: | :---: |
|  |  | 18721 | Hydra |
|  |  | 13348 | Salamis，Helle，Aetos |
|  |  | 11278 |  |
| 5，65\％ | BP | 4841 | Basileos Georgios |
| 5，65\％ | BP | 5390 | Achelaos |
|  |  | 5187 | Psara |
|  |  | 8561 | Kilkis |
|  |  | 8561 |  |
|  |  | 4696 | Huascar |
|  |  | 4739 |  |
|  |  | 4661 | re－armed Independencia |
| 5，39\％ | BP | 4655 |  |
| 1，92\％ | BP | 5143 | Independencia |
| 7，55\％ | BP | 5185 |  |
|  |  | 5086 | Independencia |
|  |  | 6570 |  |
|  |  | 6570 |  |
| 1，25\％ | BP | 16217 | Almirante Grau |
| 4，87\％ | BP | 16217 |  |
| 9，81\％ | BP | 16217 |  |
|  |  | 4527 | Huascar |
|  |  | 4242 |  |
| 6，17\％ | BP | 4375 |  |
| 9，15\％ | BP | 7353 | Almirante Grau |



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$12.7 \mathrm{~cm} \mathrm{SKC} / 34$

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| Krupp | $26 \mathrm{~cm} \mathrm{RKL/20} \mathrm{C/74}$ |
| :---: | :---: |
|  | ＂ |
| EOC | 8＂／39．9 Pattern P |
|  | ＂ |
| Armstrong | 7＂／16 6．5－Ton MLR |
|  | ＂ |
| Armstrong | 70－pdr MLR |
| Armstrong | 6＂／26 Pattern B |
|  | ＂ |
| EOC | 6＂／45 Pattern |
|  | ＂ |
|  | ＂ |
|  | ＂ |
| Canet | 150mm／45 M． 1896 |
|  | ＂ |
| Krupp | 15 cm RKL／25 C／75 |
|  | ＂ |
| Krupp | 15 cm RKL／35 C／88 |
|  | ＂ |
| Krupp | $15 \mathrm{~cm} \mathrm{SKL} / 40 \mathrm{C} / 92$ |
|  | ＂ |
| Armstrong | 5＂／25 Pattern |
| Armstrong | 40－pdr 1．32－Ton MLR |
| EOC | 4．7＂／45 Pattern |
|  | ＂ |
|  | ＂ |
| Canet | 120mm／45 M． 1887 |


|  |  | $\begin{aligned} & \overline{0} \\ & \text { N } \\ & \stackrel{\pi}{\pi} \\ & \frac{\pi}{q} \end{aligned}$ |  |  |  |  |  |  |  | $\begin{aligned} & : \frac{\pi}{\bar{W}} \\ & \frac{\tilde{\pi}}{\tilde{\pi}} \\ & \hline 0 \end{aligned}$ | $\stackrel{\downarrow}{\vdash}$ | $\begin{aligned} & \text { 들 } \\ & \text { = } \\ & \underline{\underline{\underline{\sigma}}} \end{aligned}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Ğ } \\ & \text { or } \end{aligned}$ | $\begin{array}{ll} \stackrel{L}{0} & \underset{\sim}{\sim} \\ \underset{\sim}{7} & \sigma \end{array}$ | $\begin{aligned} & \text { M } \\ & \text { 웅 } \end{aligned}$ | $\begin{array}{ll} \stackrel{\rightharpoonup}{n} \\ \underset{\sim}{m} & \stackrel{\sim}{0} \\ \underset{\sim}{2} \end{array}$ | $\begin{array}{lll} m & \circ \\ \vdots & 0 \\ \infty & \infty \\ \infty & \infty \end{array}$ | $\begin{aligned} & \text { J } \\ & \text { in } \end{aligned}$ | $\underset{\sim}{\hat{\circ}}$ | - | - | $\begin{aligned} & \stackrel{7}{6} \\ & \underset{\sim}{7} \end{aligned}$ | $\begin{aligned} & 0 \\ & \text { O} \\ & \text { Aे } \end{aligned}$ | $\underset{\infty}{\underset{\infty}{\text { ® }}}$ | O - ¢ |  |  | O - or |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | $\vdash$ |
|  |  |  |  |  | © N | $\begin{gathered} \circ \stackrel{\circ}{\circ} \\ \stackrel{\rightharpoonup}{5} \\ \text { Non } \end{gathered}$ |  |  |  |  |  |  |  |  | $\begin{aligned} & \text { oे } \\ & \stackrel{\text { O}}{ } \end{aligned}$ |


|  | " | 120,00 | 22,00 | 850,00 | 15,00 | CP | 3,60 | 2,00 | 3.6 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vickers | 4.7"/50 Mk. G | 120,00 | 22,00 | 915,00 | 45,00 | SAPC |  | 5,00 | 3.66 |
| Krupp | $10.5 \mathrm{~cm} \mathrm{SKL} / 35 \mathrm{C} / 86$ | 105,00 | 18,00 | 580,00 | 25,00 | CP | 4,36 | 2,00 | 4.0 |
| Krupp | $10.5 \mathrm{~cm} \mathrm{SKL} 40 \mathrm{C} / 97$ | 105,00 | 17,40 | 840,00 | 20,00 | SAP | 3,30 | 3,00 | 4.4 |
| Coventry | 4"/50 | 101,60 | 14,06 | 914,40 | 30,00 | SAP |  | 3,00 | 4.42 |
| Canet | 100mm/27 M. 1881 | 100,00 | 14,00 | 560,00 | 15,00 | Common | 3,90 | 2,00 | 3.6 |
| Canet | 100mm/45 M. 1896 | 100,00 | 13,00 | 760,00 | 15,00 | CP | 3,60 | 2,00 | 3.6 |
| EOC | 3.5"/40 Pattern | 88,90 | 9,07 | 737,62 | 20,00 | CP | 3,73 | 2,00 | 2.66 |
| Krupp | 8.7 cm RKU $24 \mathrm{C} /$ <br> 12-pdr QF Pattern N | 87,00 | 6,80 | 444,00 | 20,00 | Common | 2,81 | 2,00 | 3.5 |
| EOC | (3"/40) | 76,20 | 5,67 | 673,61 | 20,00 | CP | 3,72 | 2,00 | 2.59 |
|  | Yugostavia |  |  |  |  |  |  |  |  |
| Skoda | $14 \mathrm{~cm} \mathrm{L/56} \mathrm{K/37}$ | 140,00 | 39,80 | 880,00 | 45,00 | SAPBC | 4,22 | 10,00 | 4.4 |
| Skoda | $12 \mathrm{~cm} \mathrm{~L} / 46 \mathrm{~K} / 37$ | 120,00 | 24,00 | 850,00 | 35,00 | SAPBC | 4,14 | 10,00 | 3.8 |
| Skoda | $9 \mathrm{~cm} \mathrm{L/45} \mathrm{K/12}$ | 90,00 | 10,20 | 770,00 | 30,00 | CPC | 4,20 | 3,00 | 4.4 |
| Skoda | $8.4 \mathrm{~cm} \mathrm{~L} / 55 \mathrm{~K} / 29$ | 83,50 | 10,00 | 800,00 | 85,00 | CPC | 4,90 | 10,00 | 4.4 |
| Skoda | $7.5 \mathrm{~cm} \mathrm{ப} 30 \mathrm{~K} /$ | 75,00 | 6,50 | 500,00 | 30,00 | CP | 4,71 | 4,00 | 3.1 |
|  | FINLAND |  |  |  |  |  |  |  |  |
| Bofors | 25 cm . K. $/ 45 \mathrm{M} / 32$ | 254,00 | 225,00 | 850,00 | 45,00 | APC | 3,84 | 5,00 | 5.0 |
|  | " | 254,00 | 225,00 | 850,00 | 45,00 | SAP | 4,36 | 5,00 | 5.0 |
| Bofors | 10 cm . K./50 M/32 | 105,00 | 16,00 | 800,00 | 85,00 | CPC |  | 10,00 | 5.2 |
| Obuchov | 102mm/60 M. 1908 | 101,60 | 17,50 | 823,00 | 30,00 | CP | 5,00 | 4,00 | 3.0 |
|  | " | 101,60 | 17,50 | 823,00 | 30,00 | CP | 5,00 | 4,00 | 3.0 |
| Obuchov | $75 \mathrm{~mm} / 50 \mathrm{M} .1891$ | 75,00 | 4,91 | 823,00 | 30,00 | CP | 3,36 | 2,00 | 3.0 |



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## Kent R and Crawford <br> Nicholas W italevich M itiukov

# Identification of the Parameters of Naval Artillery 

Scientific edition

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[^0]:    ${ }^{1}$ See Hogg and Bachelor, Naval Gun, p. 67 for the perfect example in point. Some of the description of the Cavalli gun is correct. Nothing mentioned of Wahrendorff is.

[^1]:    2 "Breech Loading Rifled Artillery," in www.globalsecurity.org/ military, and Baxter, The Introduction of the Ironclad Warship, pp. 56, 90, 91 and 198. For a very interesting discussion regarding a connection between C avalli and the CSS Virginia, see Greene and M assignani, Ironclads at War.

[^2]:    ${ }^{3}$ See "Chapter IV. Rifles" in Gibbon's Artillery M anual, in www. usregulars. com/ gibbons. N ote that this gun pre-dates A rmstrong by several years.

[^3]:    ${ }^{4}$ General Sir Howard Douglas. A Treatise on Naval Gunnery - 1855. London: J ohn M urray, 1855. pp. 213-14.
    ${ }^{5}$ Ibid., pp. 150-51.

[^4]:    ${ }^{6}$ Ibid., pp. 217-18. M V from Table 1 are calculated values working from the known data, using exterior ballistics software written by W. J. Jurens.
    ${ }^{7}$ Letter to the author, dated J anuary 11, 2007.

[^5]:    ${ }^{8}$ Gibbon's, op.cit.
    ${ }^{9}$ Engels, "On Rifled Cannon," New Y ork Daily Tribune. A pril 7, 1860.
    ${ }^{10}$ Gibbon's, op.cit.

[^6]:    ${ }^{11}$ Ibid. And "Ordnance," Classic Encyclopedia. A nd Spencer Tucker, Arming the Fleet, p. 226.

    12 "Ordance," op. cit. and Gibbon's, op.cit. and Whipple, "The Progress in Naval A rtillery From 1855 to 1880." Ordnance Notes, -- No. 203, Washington, June 19, 1882. A nd Baxter, op.cit. p. 209.

[^7]:    ${ }^{13}$ Lars Ahlberg. Documents e-mailed to the author on November 6 and 7, 2006. And "B reech-loaded Guns... used by the Swedish A rmed Forces," www.tfd.chalmers.se.
    ${ }^{14}$ Herbert Jager, German A rtillery of W orld War One, p. 7.
    ${ }^{15}$ Douglas, op.cit., p. 216. and A hlberg, op.cit.

[^8]:    ${ }^{16}$ Ibid., p. 212. and J ager, op.cit., p. 7.
    17 "Ordnance," op. cit. A nd "Breech Loading Rifled A rtillery," op. cit.
    ${ }^{18}$ Douglas, op.cit., p. 150.
    ${ }^{19}$ Ibid., pp. 218 \& 219. Douglas means the 'cylinder' rather than a 'wedge.' This is also confirmation that the breech of the Cavalli gun failed, as he comments further that, "If the latter, when it failed, had been on board a ship, the breech would have passed through, or have made a prodigious fracture in the opposite side; and consequently, besides the physical injury, it must have produced the worst moral effect on the crew."

[^9]:    ${ }^{20}$ Ibid., p. 219.
    ${ }^{21}$ A hlberg, op.cit. A nd "B reech-loaded Guns..." op.cit.

[^10]:    ${ }^{22}$ A hlberg, op.cit. A nd Gardiner, Conway's All the World's Fishting Ships, 1860-1905, p. 362.
    ${ }^{23}$ Jager, op.cit., pp. 7 \& 9.
    ${ }^{24}$ Conway's, op.cit., pp. 267-276. And Jack Greene and Alessandro M assignani, Ironclads at War, Conshohocken: Combined Publishing, 1998., pp. 196-241and p. 254. A nd Lars A hlberg, e-mail dated December 20, 2006. A nd Brassey, The Naval A nnual, 1886, p. 386.

[^11]:    ${ }^{25}$ A. Shirokorad, Encyclopedia [of] Fatherland [Russian] Artillery. [Russian Ianguage] M insk: K arvest, 2000, pp. 258-260.
    ${ }^{26}$ L awrence Sondhaus, Preparing for Weltpolitik, A nnapolis: Naval Institute Press, 1997, p. 59.
    ${ }^{27}$ Shirokorad, op.cit. pp. 259-260. A nd Hans M ehl, Naval Guns, op. cit. p. 47.A nd Thomas A llnutt B rassey, The Naval A nnual, 1886. Portsmouth: J. Griffin and C 0.: 1886, p. 386.

    28 "Baron M artin von W ahrendorff," op.cit.
    ${ }^{29}$ Jager, op.cit. p. 9. Jager says 6-pdr, but the C/64 and K rupp's own system referred to guns as 4-pdrs, and the corresponding gun in Russian service, based on a K rupp design, is al so a

[^12]:    4-pdr, though the caliber identical. See E. M onthaye, Krupp and De B ange, p. 208, and Shirokorad, op.cit. NOTE: The 'pounder' system for denoting gun calibers was very imprecise. B ore sizes for a 30 -pdr were $16.72 \mathrm{~cm}, 16.66 \mathrm{~cm}, 16.47 \mathrm{~cm} 16.3 \mathrm{~cm}$ and 16.18 cm . The 24 -pdr could be $15.53 \mathrm{~cm}, 15.32 \mathrm{~cm}, 15.24 \mathrm{~cm}$ or 14.91 cm . A nd 12 -pdrs could be 12.19 cm or 12 cm . To some degree, nationality was a factor, but not necessarily.
    ${ }^{30}$ B axter, op.cit. p. 259. A nd Jager, op.cit. p. 7.
    31 "B reech Loading Rifled A rtillery," op.cit. A nd "History of Rifled Cannon," op.cit.
    ${ }^{32}$ Sondhaus, op.cit. pp. $53 \& 73$.

[^13]:    ${ }^{33}$ Col. J. C. Benton. Ordnance and Gunnery. Ordnance Department, 1867. p. 138.
    34 "History of Rifled Cannon," op.cit. The author does not know if the order to K rupp was eventually filled, or if the French firm of Schneider was able to provide the steel castings.
    ${ }^{35}$ Benton, op.cit. pp. 138-9.
    ${ }^{36}$ Ibid., p. 143.

[^14]:    ${ }^{37}$ Ibid., 142. A nd King, The War-Ships and Navies of the World, 1880. A nnapolis: Naval Institute Press, 1982 edition, pp. 465-6. A nd Tucker, Arming the Fleet, A nnapolis: Naval Institute Press, 1989, p. 239.
    ${ }^{38}$ J ager, op.cit., p. 9.

[^15]:    ${ }^{39}$ J ager, op.cit. p. 11. A nd "B reech Loading Rifled A rtillery," op.cit.
    ${ }^{40}$ Jager, Ibid.

[^16]:    ${ }^{41}$ J ager, Ibid. A nd E. M onthaye, K rupp and De Bange, p. 208. A nd Geoffrey Wawro, The A ustro-Prussian War, p. 220. Dr. W awro errs in referring to the Prussian artillery as a whole as "outmoded." Indeed, the A ustrian M 1861 and the Prussian C/61 were virtually identical, coming as they did from the same W ahrendorff design. A lso, Nathan Okun, e-mail to the author, February $20,2007$.

[^17]:    ${ }^{42}$ Ibid.
    ${ }^{43}$ Ibid., p. 104. A nd Greene, Ironclads at W ar, p. 259.
    ${ }^{44}$ Greene, op.cit., p. 259. A nd Erich Groner, German Warships, 1815-1945, pp. 132 134.
    ${ }^{45}$ Brassey, The British Navy. P. 62. A nd "Ordnance," op.cit. A nd "Breech Loading Rifled A rtillery," op.cit.

[^18]:    ${ }^{46}$ M onthaye, op.cit. p. 208. A nd Shirokorad, op.cit., pp. 161, 274, 287, 303, 392, 410, 420, \& 424. The Russians experimented with the K reiner Breech, an interrupted screw breech, and one other, but the vast majority of the M 1867 guns were the K rupp cylindro-prismatic. The experiments were most likely using Russian produced guns.
    ${ }^{47}$ Sondhaus, The Habsburg Empire and the Sea. p. 243.A nd Gardiner, Conway's 1860 1905, pp. 268-276.
    ${ }^{48}$ Conway's 1860-1905, op.cit., pp. 372, 383, 392 and 416.

[^19]:    ${ }^{49}$ Ibid., pp. 219, 231, 235 and 413. A nd W atts and Gordon, The Imperial Japanese Navy, pp. 77-82. A nd Jentschura, Jung and M ickel, Warships of the Imperial Japanese Navy, 1869 1945, pp. 12, 89, and 113-4.
    ${ }^{50}$ Hovgaard, op.cit, p. 397.

[^20]:    ${ }^{51}$ Sondhaus, Weltpolitik, op.cit., p. 82. Jager, op.cit., p. 62. Hovgaard, op.cit. p. 398. A nd M onthaye, op.cit., p. 112. A nd Groner, op.cit., p. 134.
    ${ }^{52}$ Sondhaus, W eltpolitik, op.cit, pp. 90-91. A nd Greene, op.cit., p. 258. And M onthaye, op.cit., pp. 112-113.
    ${ }^{53}$ Hovgaard, op.cit., p. 398. A nd V ery, "Development of Armor for Naval Use,"pp. 441 442.

[^21]:    ${ }^{54}$ Sondhaus, Weltpolitik, op.cit, pp. 90-91. A nd Greene, op.cit., p. 258. And M onthaye, op.cit., pp. 112-113. A nd V ery, op.cit.

[^22]:    ${ }^{55}$ Gardiner, Comway's All the W orld's Fighting Ships, pp. 267-270.
    ${ }^{56} \mathrm{M}$ arshall Bastable, Arms and the State, pp. 135-142.

[^23]:    ${ }^{57}$ See Greene, Ironclads at W ar.
    ${ }^{58}$ M.L. Ruffell, "B reech M echanisms." A nd M ehl, Naval Guns, p. 183.

[^24]:    ${ }^{59}$ M onthaye, op.cit. p. 208.
    ${ }^{60}$ Ibid., p. 106.
    ${ }^{61}$ Brassey, The Naval A nnual 1886, pp. 386-391. The Trial 4 MV is a calculated value.

[^25]:    ${ }^{62}$ B rassey, The Naval A nnual 1886, pp. 386-391. The Trial 4 MV is a calculated value.

[^26]:    ${ }^{63}$ Ruffell, op.cit.

